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Using Turbidity Monitoring and LiDAR-Derived Imagery to Investigate Sources of Suspended Sediment in the Little North Santiam River Basin, Oregon, Winter 2009-2010

Steven Sobieszczyk
Portland State University

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Using Turbidity Monitoring and LiDAR-Derived Imagery to Investigate Sources of
Suspended Sediment in the Little North Santiam River Basin, Oregon,
Winter 2009–2010

by
Steven Sobieszczyk

A thesis submitted in partial fulfillment of the
requirements for the degree of

Master of Science
in
Geology

Thesis Committee:
Scott F. Burns, Chair
R. Benjamin Perkins
Jiunn-Der Duh

Portland State University
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Abstract

The Little North Santiam River Basin is a 111-square mile watershed located in the Cascade Range of western Oregon. The Little North Santiam River is a major tributary to the North Santiam River, which is the primary source of drinking water for Salem, Oregon and surrounding communities. Consequently, water quality conditions in the Little North Santiam River, such as high turbidity, affect treatment and delivery of the drinking water. Between 2001 and 2008, suspended-sediment loads from the Little North Santiam River accounted for 69% of the total suspended-sediment load that passed the treatment plant. Recent studies suggest that much of this sediment originates from landslide activity in the basin.

Using airborne Light Detection and Ranging (LiDAR)-derived imagery, 401 landslides were mapped in the Little North Santiam River Basin. Landslide types vary by location, with deep-seated earth flows and earth slumps common in the lower half of the basin and channelized debris flows prominent in the upper basin. Over 37% of the lower basin shows evidence of landslide activity compared to just 4% of the upper basin. Instream turbidity monitoring and suspended-sediment load estimates during the winter of 2009–2010 demonstrate a similar distribution of sediment transport in the basin. During a 3-month study period, from December 2009 through February 2010, the lower basin supplied 2,990 tons, or 91% of the suspended-sediment load to the Little North Santiam River, whereas the upper basin supplied only 310 tons of sediment. One small 23-acre earth flow in the lower basin, the Evans Creek Landslide, supplied 28% of the total suspended-sediment load, even though it only comprises 0.0004% of the basin.

The Evans Creek Landslide is an active earth flow that has been moving episodically since at least 1945, with surges occurring between 1945 and 1955, 1970 and 1977, in February 1996, and in January 2004. Recent erosion of the landslide toe by Evans Creek continues to destabilize the slope, supplying much of the sediment measured in the Little North Santiam River. Over the last 64 years, the average landslide movement rate has been between 5 and 12 feet per year.

Dedication

For my little girl, Maggie

and

for Mac, stay strong.

Acknowledgements

I would like to thank all those who motivated me and supported me, for those who corrected my errors, and for those who sacrificed their time and energy to help me complete this study. This research could have not been completed without you.

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Lastly, I need to offer a special thanks to those two individuals who made my world a whole lot easier and with which this project could not have been completed:

- Sheri Schneider (U.S. Geological Survey) and Ian Madin (Oregon Department of Geology and Mineral Industries). One word: “LiDAR.”

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Chapter 1: Introduction

Landslides are a common landscape feature in the Cascade Range of western Oregon. The combination of heavy rainfall, deeply-weathered soils, and steep slopes in the region make hillsides highly susceptible to slope failure. Along high elevations with steep slopes debris flows tend to be most common, while in the lower Western Cascades and Willamette Valley foothills earth flows and rotational earth slumps become more prevalent (Swanston, 1981; Swanson and others, 1987; Pearch, 2001; Hofmeister and others, 2002). Landslide activity poses many risks to people and the environment, including concerns from sediment transport in streams, damage to infrastructure, and even loss of life. Therefore, the identification of landslide locations or landslide-prone areas is vital for reducing these potential risks. Recently, landslide identification and visualization has improved greatly due to the availability of high-resolution aerial Light Detection and Ranging (LiDAR)-derived imagery (Haugerud and others, 2003; Burns, 2007). Since LiDAR is effective at penetrating the dense tree canopy cover of Pacific Northwest forests, new landslide inventories have become much more detailed than those completed previously using a combination of aerial photographic interpretation and field reconnaissance (Burns, 2007).

Identifying and cataloguing landslides is a high priority for state and federal land managers following periods of intense rainfall and flooding, such as during the 100-year flood event that occurred in February 1996 (Burns and others, 1998; Hofmeister and others, 2002; Oregon Department of Geology and Mineral Industries, 2009a). In early 1996, heavy rainfall mobilized thousands of debris flows (Hofmeister, 2000), as well as numerous rotational slumps and earth flows, across much of the western Oregon. One

watershed where hundreds of these rapidly-moving landslides were observed was the North Santiam River Basin (Bates and others, 1998; Hofmeister, 2000). The landslides damaged a number of homes and roads, as well as supplied 100,000s of tons of sediment into rivers and streams, greatly reducing water quality in the North Santiam River (Bates and others, 1998; U.S. General Accounting Office, 1998; Hulse and others, 2002).

Because the North Santiam River serves as the primary source of drinking water for Salem, Oregon, and the surrounding communities, highly turbid (or “dirty”) water was problematic for treatment and consumption. In response, the City of Salem joined with the U.S. Geological Survey (USGS) to investigate sediment sources and establish a near real-time continuous water-quality monitoring network in the basin. The monitoring network became operational in the fall of 1998 and remained an essential tool for regulators and land managers through the winter of 2009–2010.

Between 1998 and 2010, storms did not produce any runoff events as large as the flood observed in February 1996. Although recent storms were smaller, major turbidity events did continue to occur throughout much of the North Santiam River Basin (Sobieszczyk and others, 2007). However, few of these turbidity events affected treatment plant operations. For example, major turbidity events in the upper North Santiam River Basin, such as the November 6, 2006, Mount Jefferson debris flow (Sobieszczyk and others, 2008) were large and dramatic, but rarely supplied significant amounts of sediment into the lower basin below Detroit Lake (Bragg and Uhrich, 2010). Suspended sediment from the upper basin often settled and remained trapped behind Detroit Dam, effectively reducing the amount of material that reached the City of Salem’s drinking-water treatment plant. Therefore, most suspended sediment that passed the treatment plant originated in the lower North Santiam River Basin. According to a recent

study (Bragg and Uhrich, 2010), 69% of the suspended-sediment load that passed the treatment plant between October 2001 and September 2008 came from the Little North Santiam River.

Since most of the suspended-sediment load measured in the lower North Santiam River comes from the Little North Santiam River, much of the new research in sediment transport focuses on the Little North Santiam River Basin. For example, this study investigates potential source areas where sediment originates within the basin, what factors likely influence sediment erosion and transport, and if there are possible mitigation solutions that can be implemented to reduce erosion and suspended-sediment transport. Since landslides appear to contribute much of the suspended sediment found in streams of Cascadian watersheds (Fredriksen, 1971; Ambers, 2001; Pearch, 2001; Sobieszczyk and others, 2007), slope stabilization techniques are also discussed.

Chapter 2: Aims and Objectives

The purpose of this study is to examine potential source areas where sediment production is responsible for increased turbidity in the Little North Santiam River.

Previous work in the Little North Santiam River Basin (Bureau of Land Management, 1997; Sobieszczyk and others, 2007; Bragg and Uhrich, 2010) and elsewhere in the Cascade Range (Fredriksen, 1971; Bates and others, 1998; Pearch, 2001; Hulse and others, 2002) suggests that high turbidity in streams is often associated with a specific landslide or mass-wasting event. Therefore, this study investigates landslide source areas in the Little North Santiam River Basin and examines their influence on sediment input to rivers and streams. This assessment was completed using a combination of remote sensing techniques, including LiDAR-based mapping, aerial photographic interpretation, and instream turbidity monitoring. Specific goals for this project included:

- Use high-resolution LiDAR-derived imagery, aerial photographs, and field reconnaissance to map landslide deposits in the Little North Santiam River Basin;
- Monitor continuous instream turbidity and estimate suspended-sediment loads at five locations in the Little North Santiam River Basin for the winter of 2009–2010;
- Examine how sediment input varied, by reach, in the Little North Santiam River;
- Where possible, relate suspended-sediment loads to specific landscape features, such as the Evans Creek Landslide;
- Examine how the Evans Creek Landslide has changed over time;
- Discuss how geology, hydrology, and land management practices influence erosion potential and sediment transport in the basin; and
- Assess possible alternatives for reducing erosion risk and improving slope stability in the basin.

Chapter 3: Background

3.1: Study Area

Located in the heart of the Cascade Range of western Oregon, the Little North Santiam River drains 111 square miles (mi^2) [287 square kilometers (km^2)] and traverses over 22 miles (mi) [35 kilometers (km)] before entering the North Santiam River at the town of Mehama, Oregon (Figure 1). Since the Little North Santiam River is the largest tributary with the greatest amount of sediment input of any stream entering the North Santiam River below Detroit and Big Cliff Reservoirs (Bragg and Uhrich, 2010), it has a significant effect on water quality and streamflow conditions in the North Santiam River.

As is characteristic with Cascadian rivers, the headwaters of the Little North Santiam River are located high in the mountains, discharging mostly from groundwater seeps. Seasonal snowmelt from high elevation snowfields also contribute to higher streamflow conditions during the winter and spring. The Little North Santiam River Basin is considered part of the Western Cascade ecoregion (Omernik, 1987) and physiographic province (Forest Ecosystem Management Assessment Team, 1993), which when combined with the High Cascades to the east, comprises the Cascade Range. The Western Cascades typically have lower average elevations and are composed of older and more weathered bedrock than the High Cascades. Surface elevations in the basin range from 660 to 5,560 feet above sea level.

Access through the basin is relatively limited with residents mostly dependent on North Fork and Gates Hill Roads, both of which are Marion County Public Works-maintained roadways. The Little North Santiam River Basin covers much of north-central Marion County, with a small portion of the basin overlapping into Clackamas County.

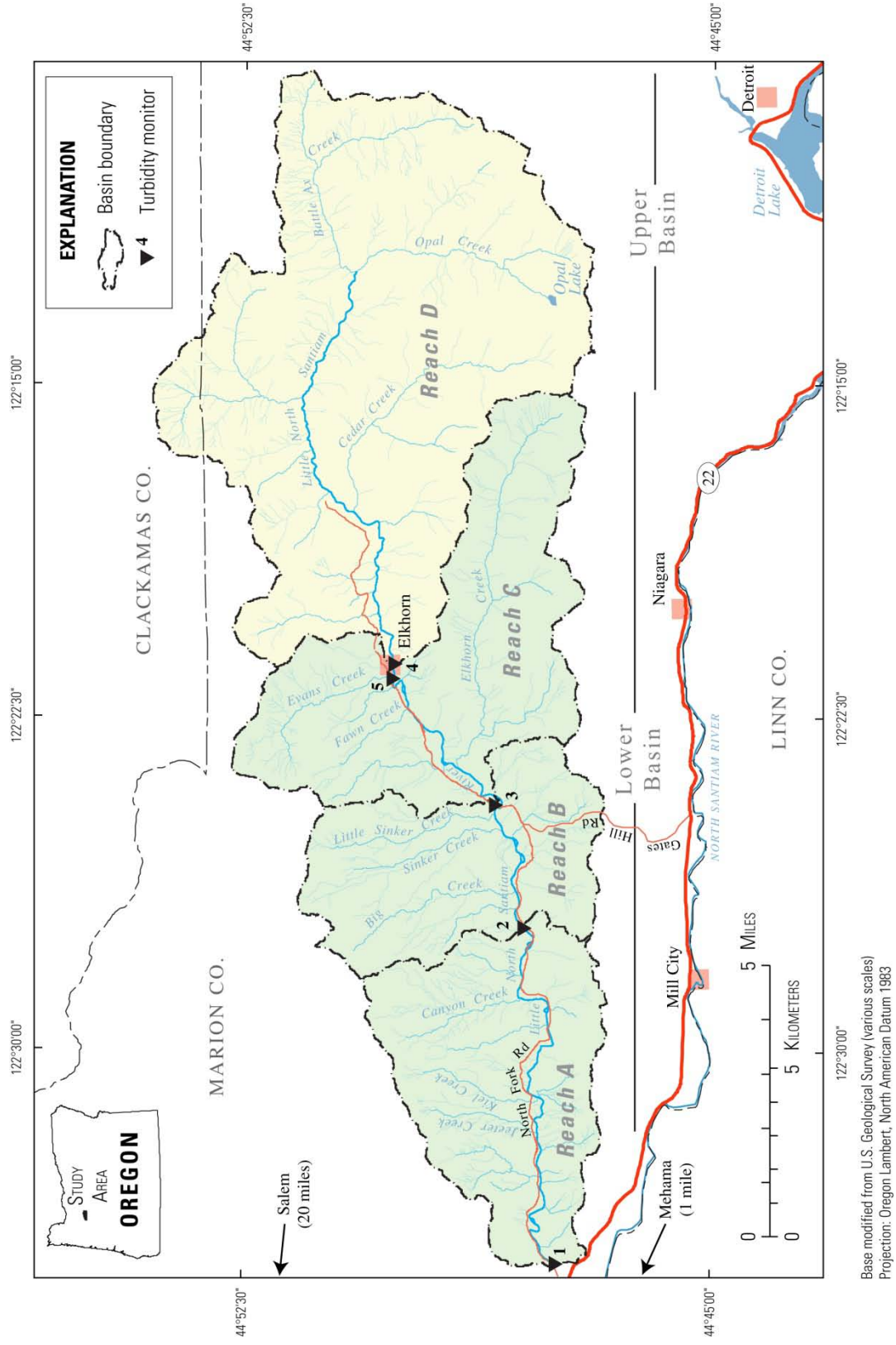


Figure 1. Location of the Little North Santiam River Basin, Oregon.

3.2: Basin Setting

3.2.1: Climate and Precipitation

The climate of the Little North Santiam River Basin is characteristic of the Western Cascades physiographic province, represented by warm, dry summers and cool, rainy winters (PRISM Climate Group, 2006). It is common for mountain peaks in the basin to receive 10s of inches (in.) [10s to 100s of centimeters (cm)] of winter snowfall, while much of the valley floor receives less than a few inches of snow a year (Oregon Climate Service, 2006). Most precipitation occurs as rainfall, with highlands receiving nearly a third more rain than the valley floor (Figure 2). Although the estimated 30-year mean annual precipitation in the basin varies between 70 and 103 in. [178 and 262 cm], nearby rain gages in Salem and Detroit, typically record between 40 and 50 in. [102 and 127 cm] of rain per year (Oregon Climate Service, 2006).

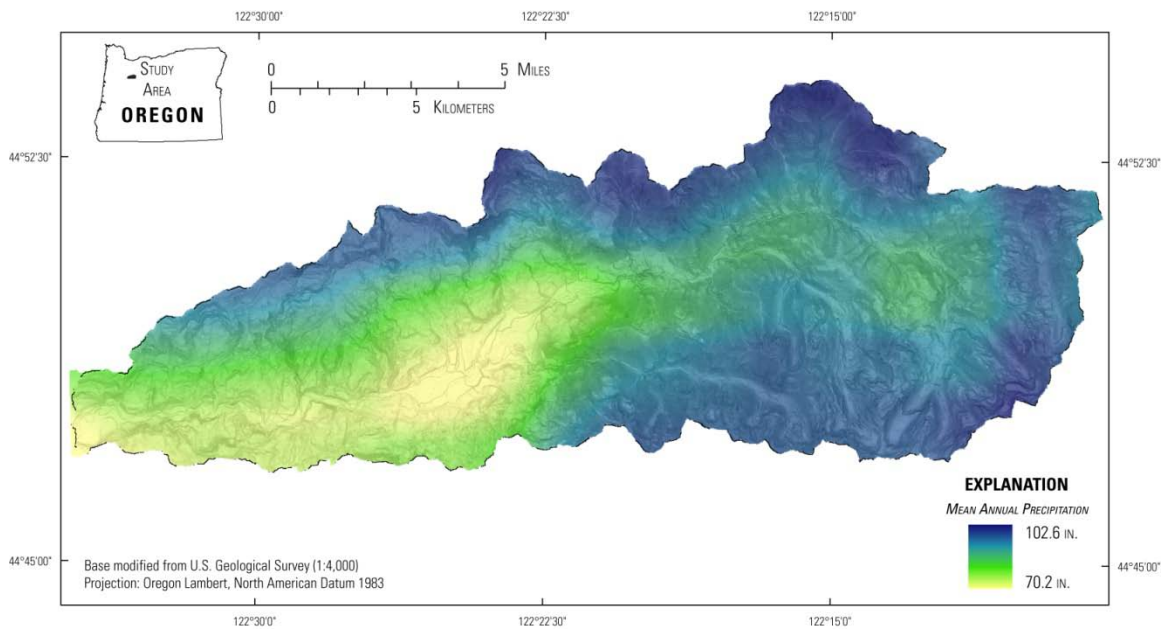


Figure 2. Mean annual precipitation (1971-2000), in inches, for the Little North Santiam River Basin, Oregon (modified from PRISM Climate Group, 2006).

3.2.2: Geologic Maps and Soil Surveys

3.2.2.a: Geology

The bedrock geology of the Little North Santiam River Basin is comprised predominantly of Little Butte and Late Western Cascade Volcanics (Walker and McLeod, 1991; Bureau of Land Management, 1997; Sherrod and Smith, 2000; Oregon Department of Geology and Mineral Industries, 2009b). These terranes consist of mixed rock types, including volcanoclastic sedimentary rocks, tuffs, and lava flows and flow breccias (Table 1). Rocks are generally Oligocene (32 to 17 million years old) to Miocene (17 to 10 million years old) age. The upper basin, as defined by Reach D (Figure 1), is primarily younger (Miocene-age) and less eroded basaltic andesite. This basalt “cap” has eroded and receded in much of the lower basin, thereby exposing older Oligocene-aged undifferentiated tuffaceous, volcanoclastic, and sedimentary rocks (Figure 3; Oregon Department of Geology and Mineral Industries, 2009b). Similar basalt flows cover both the northern and southern ridge top margins of the lower basin. Along with expansive lava flows and other pyroclastic deposits, a number of northwest-trending basaltic and andesitic dikes and intrusions are also exposed at different locations in the basin.

Surficial geology along the valley floor includes alluvial, colluvial, and lacustrine deposits, as well as some Quaternary glacio-fluvial deposits. Pleistocene glaciers scoured parts of the upper basin, leaving cirques and at least one glacial lake (Opal Lake). Ancient subduction zone earthquakes (Scott Burns, Portland State University, oral commun., 2009) likely triggered massive landslides in the central and lower valley that dammed the Little North Santiam River, creating prehistoric lakes and subsequent terrace deposits near present day Elkhorn and Elkhorn Valley (Sherrod and Smith, 2000).

Table 1. Geologic unit descriptions (Oregon Department of Geology and Mineral Industries, 2009b) and related landslide frequency per unit in the Little North Santiam River Basin, Oregon.

[Shading represents geologic units with landslide activity]

Unit	Description	Age	Terrane	Rock Type	General Geology	Landslide Frequency
Dike	Dike	Oligocene/Miocene	Little Butte Volcanics	mixed lithologies	intrusive rocks	0
Dike1	Dike	Oligocene/Miocene	Late Western Cascade Volcanics	mixed lithologies	intrusive rocks	0
QTg	Weathered terrace gravel	Pliocene/Pleistocene	Willamette Group	mixed grained sediments	sediments	0
QTi	Quaternary-Tertiary intrusions	Pliocene/Pleistocene	Late High Cascade Volcanics	mafic composition lithologies	intrusive rocks	0
Qal	Alluvium	Quaternary	Quaternary surficial deposits	mixed grained sediments	sediments	1
Qau	Alluvium, undifferentiated	Quaternary	Quaternary surficial deposits	mixed grained sediments	sediments	3
Qba	Basalt of Battle Ax	Quaternary	Late High Cascade Volcanics	basaltic andesite	volcanic rocks	0
Qgf	Glacio-fluvial deposits	Quaternary	Quaternary surficial deposits	mixed grained sediments	sediments	15
Qls	Landslide deposits and colluvium	Quaternary	Quaternary surficial deposits	mixed grained sediments	sediments	38
Qt	Terrace and fan deposits	Quaternary	Quaternary surficial deposits	mixed grained sediments	sediments	40
Qyt	Younger till	Quaternary	Quaternary surficial deposits	mixed grained sediments	sediments	6
Tad	Andesite, porphyritic feeder dikes of the lower member	Oligocene/Miocene	Little Butte Volcanics	andesite	intrusive rocks	0
Tb	Ridge-capping basalt and basaltic andesite	Miocene	Early High Cascade Volcanics	basalt	volcanic rocks	1
Tba	Basaltic andesite	Miocene	Late Western Cascade Volcanics	basaltic andesite	volcanic rocks	18
Tbp	Tourmaline bearing breccia pipes	Oligocene/Miocene	Little Butte Volcanics	breccia	intrusive rocks	0
Tc	Columbia River Basalt Group and related flows	Miocene	Columbia River Basalt Group	basalt	volcanic rocks	4
Td	Beds at Detroit	Oligocene/Miocene	Little Butte Volcanics	mixed lithologies	volcaniclastic rocks	0
Tdg	Diorite and gabbro	Miocene	Late Western Cascade Volcanics	intermediate composition lithologies	intrusive rocks	0
Tds	Dacite	Oligocene/Miocene	Little Butte Volcanics	dacite	volcanic rocks	0
Tfc	Flows and clastic rocks, undivided	Miocene	Late Western Cascade Volcanics	intermediate composition lithologies	volcanic rocks	44
Thg	Hewitt Granodiorite	Oligocene/Miocene	Little Butte Volcanics	intermediate composition lithologies	intrusive rocks	0
Ti	Undifferentiated Tertiary intrusions	Miocene	Late Western Cascade Volcanics	mixed lithologies	intrusive rocks	0
Tib	Intrusive basalt and andesite intrusions	Miocene/Pliocene	Late Western Cascade Volcanics	mixed lithologies	intrusive rocks	0
Tib1	Intrusive basalt and andesite intrusions	Oligocene/Miocene	Little Butte Volcanics	mixed lithologies	intrusive rocks	0
Tiha	Hornblende Andesite/Diorite	Miocene	Late Western Cascade Volcanics	andesite	intrusive rocks	5
Tipa	Pyroxene Andesite/Diorite	Oligocene/Miocene	Little Butte Volcanics	mixed lithologies	intrusive rocks	0
Tis	Silicic intrusive rocks	Oligocene/Miocene	Little Butte Volcanics	felsic composition lithologies	intrusive rocks	0
Tlm	Sardine Formation, lower member	Oligocene/Miocene	Little Butte Volcanics	mixed lithologies	volcaniclastic rocks	11
Tmd	Microdiorite	Oligocene/Miocene	Little Butte Volcanics	intermediate composition lithologies	intrusive rocks	0
Tmv	Mafic vent complexes	Miocene	Late Western Cascade Volcanics	mafic composition lithologies	vent and pyroclastic rocks	0
Tn	Andesite of Nohorn Creek	Miocene	Late Western Cascade Volcanics	andesite	volcanic rocks	0
Tql	Quartz latite/rhyodacite	Oligocene/Miocene	Little Butte Volcanics	felsic composition lithologies	intrusive rocks	0
Tr	Rhododendron Formation	Miocene	Late Western Cascade Volcanics	andesite	volcanic rocks	6
Trd	Ruth diorite	Oligocene/Miocene	Little Butte Volcanics	intermediate composition lithologies	intrusive rocks	0
Tsa1	Sardine Formation, Tuff of Pansy Basin	Oligocene/Miocene	Little Butte Volcanics	ashflow tuff	volcaniclastic rocks	1
Tsa4	Sardine Formation, Hornblende Andesite flow of Silver King Mountain	Miocene	Late Western Cascade Volcanics	andesite	volcanic rocks	0
Tu	Tuffaceous sedimentary rocks, basalt flows, and tuffs, undivided	Oligocene/Miocene	Little Butte Volcanics	mixed lithologies	volcaniclastic rocks	195
Tum	Sardine Formation, upper member	Miocene	Late Western Cascade Volcanics	basaltic andesite	volcanic rocks	10
Tus	Clastic sedimentary rocks	Oligocene/Miocene	Little Butte Volcanics	mixed lithologies	volcaniclastic rocks	3

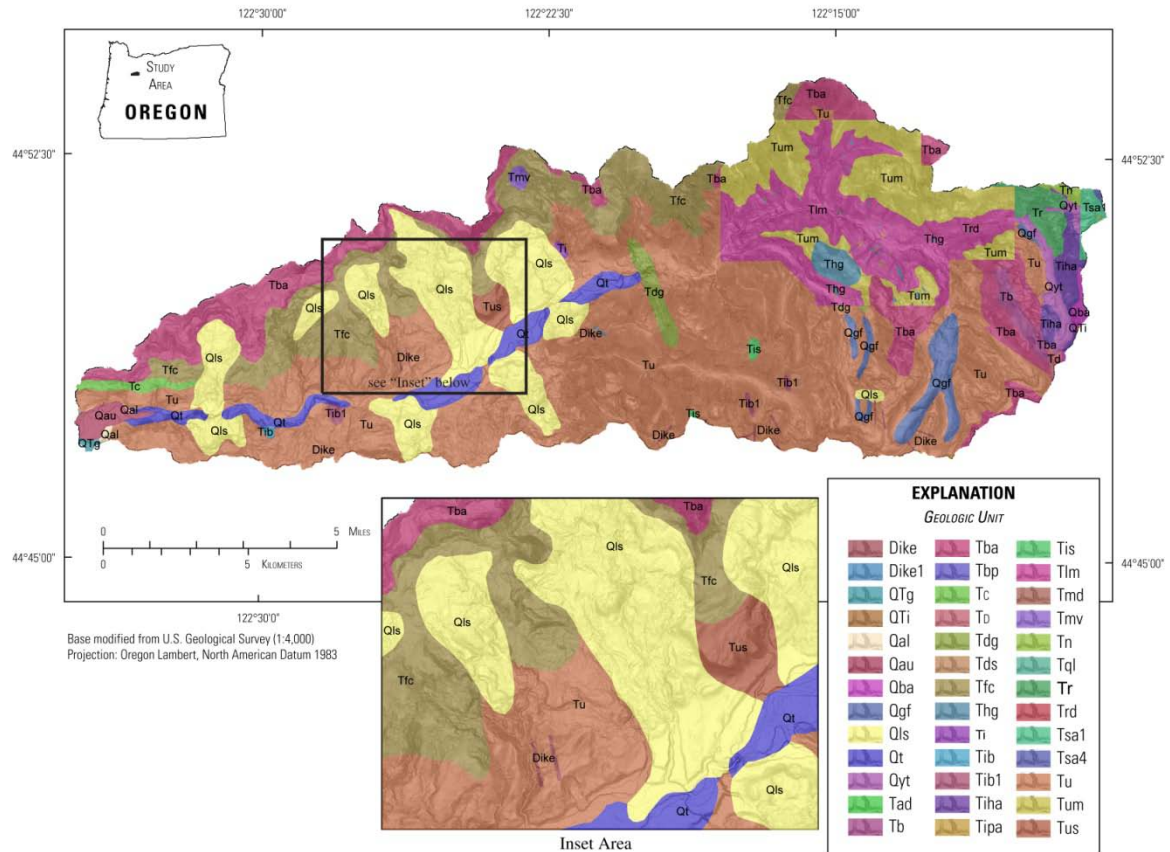


Figure 3. Geology of the Little North Santiam River Basin, Oregon (Oregon Department of Geology and Mineral Industries, 2009b).

3.2.2.b: Pedology (Soils)

Due to mixed private, state, and federal land ownership within the Little North Santiam River Basin (see “Land Management and Land Use Activities” below) there is not a high-quality continuous, comprehensive soil survey across the entire basin. Instead, the Natural Resources Conservation Service (NRCS) has compiled a countywide soil survey geographic (SSURGO) database (Natural Resources Conservation Service, 2007) for non-federal land, while the U.S. Forest Service (USFS) compiled a soil resources inventory (SRI) survey for land in the Willamette National Forest (U.S. Forest Service,

1992). Each survey mapped and characterized different soil-related factors, with little to no overlap between the two inventories. However, the Bureau of Land Management (BLM) conducted a broad watershed assessment (1997) following the 1996 flood that examined the general pedology (Table 2) of the whole basin based on the available soil inventories, including the coarse-scale state soil geographic (STATSGO) database (Natural Resources Conservation Service, 1994).

Table 2. Soils of the Little North Santiam River Basin, Oregon (Bureau of Land Management, 1997).

[**Abbreviations:** mi², square miles; km², square kilometers]

Soil Groups	Area (mi ²) [km ²]	Percent of basin	Description
Keel, Hummington, Highcamp	59 [153]	53%	Cryic cold soils
Winopee, Dinzer, Talapus	13 [34]	12%	Cryic cold soils
Peavine, Honeygrove, Orford	16 [42]	14%	Silty clay loams, Clay loams
Klickatat, Kinney, McCully	21 [55]	19%	Gravelly, cobbly loams
Malabon, Coburg, Salem	1 [3]	1%	Silt loams

Soil development in the Little North Santiam River Basin is controlled by the underlying geology, past glaciations, regional climate, vegetation, and periodic disturbances such as fire, flood, and landsliding (Bureau of Land Management, 1997). Soil type and development also varies based on basin location. For example, the upper half of the basin (primarily Reach D) consists of shallow-soiled highlands with sharp bedrock ridges. Due to steep slopes in these high elevations, only shallow, poorly-sorted soil accumulation is possible. The relatively young soils have undergone limited soil horizon development and are composed of moderately to well-drained cobbly or stony loams (Bureau of Land Management, 1997).

In the western, low-elevation portion of basin, soils are thicker and more developed. These soils consist of well-drained clay loams covering intermixed cobbly loams, as well as a mixture of glacial till, colluvium, and weathered tuffaceous igneous rock. Much of tuffaceous, volcaniclastic rock has weathered into chlorite, illite, and smectite-rich clays (Glasmann, 1997; Ambers, 2001). These thick, clay-rich soils form unstable, deep-seated earth flows and rotational earth slumps found in the lower basin. Smectite clays are a major source of persistent turbidity (Sobieszczyk and others, 2007) since they are easily eroded and can remain in colloidal suspension for months following major storm events (Bates and others, 1998; Hulse and others, 2002; Uhrich and Bragg, 2003). Due to the expandable nature of these smectite clays, their presence in earth flow soils is evident by their x-ray diffraction clay mineralogy after samples are treated with ethylene glycol (Figure 4), a process that causes the clay layers to hydrate and expand.

3.2.3: Land Management and Land Use Activities

Land management in the Little North Santiam River Basin is divided into private, state, and federal lands (Table 3). Most of the upper basin, and nearly half of the entire basin, is covered by the Bull of the Woods Wilderness, a component of the USFS Willamette National Forest. The wilderness area extends from near the town of Elkhorn east through the remainder of the highlands (Figure 5). Much of the federally-protected old growth forest is accessible by trail, including natural and historical sites, such as the scenic Opal Creek Wilderness area and the historic mining town Jawbone Flats. The lower basin consists of a checkerboard of mixed landowners, including Oregon Department of Forestry, BLM, private timber, and private residential (Figure 5).

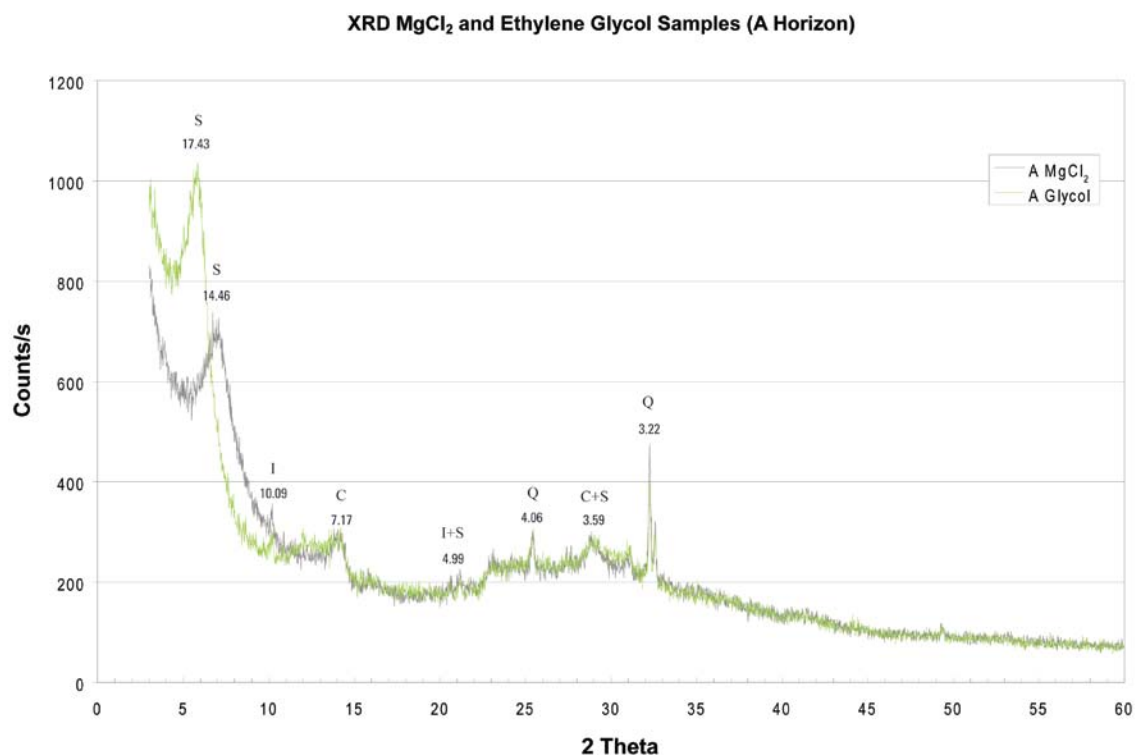


Figure 4. X-ray diffractogram (XRD) for soil sample collected from the Bear Trap Slide (earth flow) in the lower Little North Santiam River Basin, Oregon. Clay mineralogy includes smectite (S), illite (I), chlorite (C), quartz (Q), and expansive intermixed layers (C+S). Labels represent d-spacing distances (Å) of clay minerals. Clay mineralogy sample was processed twice, first with MgCl_2 (gray line) only, then with MgCl_2 and ethylene glycol (green line). XRD work completed previously by author (unpublished) using methods defined in Glasmann (1997) and Ambers (2001).

Table 3. Summary of land ownership in the Little North Santiam River Basin, Oregon (Oregon Department of Forestry, 2003).

[Abbreviations: mi^2 ; square miles; km^2 , square kilometers]

Owner	Area	Percent of basin
	(mi^2) [km^2]	
Bureau of Land Management	20 [54]	19%
Forest Service	54 [140]	48%
Oregon Department of Forestry	3 [8]	3%
Private	33 [85]	30%
Total	111 [287]	100%

Land use activities in the basin include: recreation, such as golfing, camping, hiking, fishing, and kayaking; resource extraction, such as timber harvesting and mining; agricultural farming; and urban development and domestic use. The Little North Santiam River is considered a pristine river (Bureau of Land Management, 1997) and is designated as one of Oregon's Scenic State Rivers (Oregon Parks and Recreation Department, 2010). Large developments and points of interest in the basin include the Elkhorn Valley Golf Course, North Fork and Salmon Falls County Parks, and Bear Creek and Elkhorn Valley Campgrounds.

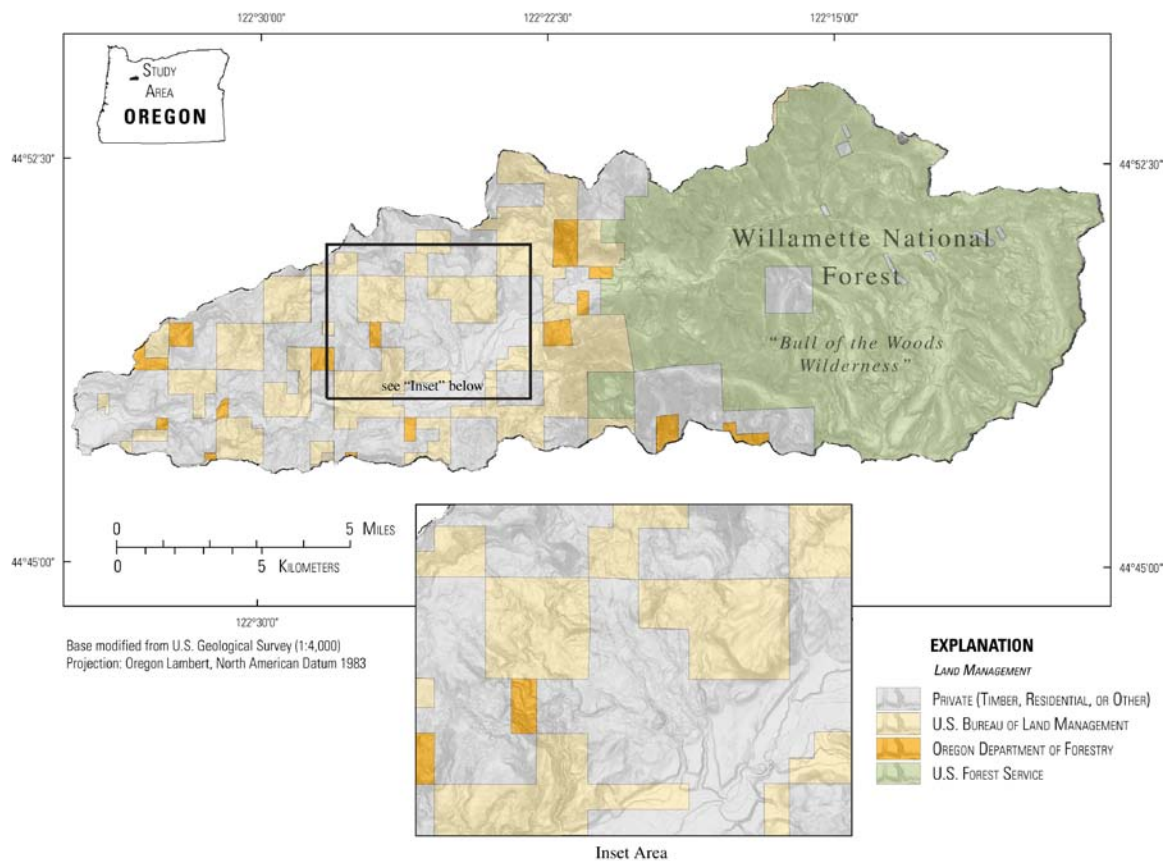


Figure 5. Distribution of land ownership or management in the Little North Santiam River Basin, Oregon (Oregon Department of Forestry, 2003).

3.2.4: Roadways, Logging Roads, and Trail Network

Road construction and maintenance is a common necessity in the Little North Santiam River Basin. Timber companies that actively harvest must continually develop new logging roads while either maintaining or decommissioning older ones. In addition, large roadways, such as the North Fork Road, also require continued maintenance and repairs. For example, active landsliding beneath the North Fork Road has required a series of engineered solutions over the past few years to stabilize and repair segments of the roadway (Landslide Technology, 1997; GeoDesign, 2009). At the time of this publication, a section of road atop an active landslide (“Bear Trap Slide”) near Mile Post 4 was still progressively failing and causing major transportation problems (Rod Bray, Marion County Public Works, oral commun., 2009). North Fork Road and Gates Hill Road are the two primary roadways that traverse in and out of the basin and are both maintained by the county.

Similar to previously mentioned basin characteristics, the road network in the Little North Santiam River Basin is highly variable (Figure 6). The upper basin has few active roads and a limited number of remnant logging roads, most of which have been converted into network of hiking trails. Conversely, the lower basin has a dense network of logging roads and road right-of-ways, two county-maintained roadways, and other residential roads, driveways, and trails.

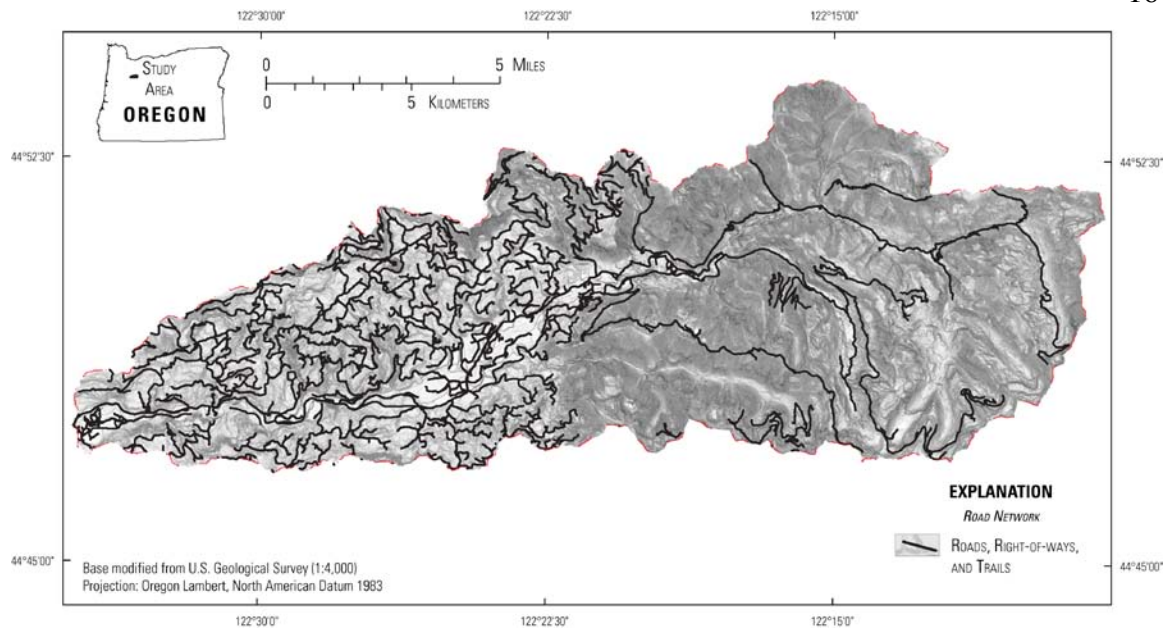


Figure 6. Roads, right-of-ways, and trails in the Little North Santiam River Basin, Oregon.

3.3: Historical Water-Quality Issues

3.3.1: Little North Santiam River Turbidity

Although the pristine waters of the Little North Santiam River allow for low maintenance, affordable drinking water through primarily slow-sand filtration, sometimes water-quality issues arise that require more costly treatment. Examples of water-quality issues include point source pollution, algal blooms, and high turbidity events. This study focuses on issues with turbidity and related suspended-sediment transport. Turbidity issues relate to any event where enough sediment enters a stream that there is a concern about maintaining a safe public water supply or protecting against damage to the drinking-water treatment plant (Economic and Engineering Services and HDR Engineering, 2003). Recent high turbidity events that were a concern in the Little North Santiam River occurred during the 1996 flood (Bureau of Land Management, 1997;

Bates and others, 1998; U.S. General Accounting Office, 1998), in November 1999, in January 2004 (Sobieszczyk and others, 2007; Bragg and others, 2007), and November 2006 (Bragg and Uhrich, 2010).

In 1996, a number of water samples were collected by the City of Salem at tributaries along the Little North Santiam River and measured in their laboratory for turbidity (Bureau of Land Management, 1997). Samples were collected during individual storm periods over the winter months from streams with visibly elevated turbidities. During the sampling Canyon Creek produced six high turbidity events, Sinker Creek produced four, Kiel and Evans Creeks produced two each, and Fawn Creek produced one (Bureau of Land Management, 1997). The highest measured turbidity during that study was from Evans Creek with a reading of 130 Nephelometric Turbidity Units* (NTU).

In November 1999, heavy rainfall initiated one of the highest monthly suspended-sediment loads recorded for the Little North Santiam River (Bragg and others, 2007). The river transported roughly 46,000 short tons (T) [42,000,000 kilograms (kg)] of sediment in November (Heather Bragg, U.S. Geological Survey, written commun., 2009). That single month comprised 78% of the entire yearly suspended-sediment load for water year 2000 (October 1, 1999 through September 30, 2000). The major turbidity event that occurred in January 2004 was much smaller than both the 1996 flood and November 1999 storm periods, yet poor water-quality conditions still prompted a brief closure of the water treatment plant (Sobieszczyk and others, 2007). Turbidity rose above 250 Formazin Nephelometric Units* (FNU) and estimates indicated over 11,000 T [10,000,000 kg] of suspended sediment flowed through the Little North Santiam River in only four days. The sediment transported over that 4-day period equated to 62% of the annual suspended-sediment load for water year 2004 (Bragg and others, 2007). Lastly, in November 2006 a

major storm passed over much of the Pacific Northwest, triggering landslides across much of the region (National Park Service, 2007; Pirot and others, 2007; Sobieszczyk and others, 2008). During that winter, due mostly to a single storm event on November 6 and 7, the second highest monthly suspended-sediment load, 39,000 T [35,000,000 kg], occurred in the Little North Santiam River (Bragg and Uhrich, 2010).

**Note for Measuring Turbidity*

Turbidity sensors that measure Nephelometric Turbidity Units (NTU) use a white or broadband light source (400-680 nanometers), whereas sensors measuring in Formazin Nephelometric Units (FNU) use an infrared or monochrome light source (780-900 nanometers). Both instruments detect scattered light at near 90° to the incident light source. FNU are one of the most common measurements for in situ turbidity readings. Laboratory instruments commonly measure in NTU. Units are not interchangeable (Anderson, 2005).

3.3.2: Evans Creek Turbidity

Field investigations during these high turbidity events in the Little North Santiam River, as well as during other storms from subsequent years, determined that much of the suspended sediment observed in the river came from Evans Creek (Figure 7). Evans Creek is a small tributary that enters the Little North Santiam River downstream of the town of Elkhorn (Figure 1). The creek drains a 3.4 mi² [9 km²] watershed. Since at least 2004 (Sobieszczyk and others, 2007), Evans Creek has been consistently more turbid than the Little North Santiam River (Figure 7). Turbidity is high in Evans Creek

regardless of rainfall or river stage conditions, with elevated turbidity observed both in wet winter and dry summer months.



Figure 7. Multiple instances of turbid water from Evans Creek entering the Little North Santiam River, Oregon (Photos: Mark Uhrich and Steven Sobieszcyk, U.S. Geological Survey, various dates).

3.4: Local Slope Stability Concerns and Landslide History

Previous landslide inventories (Oregon Department of Geology and Mineral Industries, 2009a) and an examination of geologic maps in the area (Walker and McLeod, 1991; Sherrod and Smith, 2000; Oregon Department of Geology and Mineral Industries, 2009b) identify between seven and ten discrete Quaternary landslide deposits (“Qls”) in the Little North Santiam River Basin (Figure 3), depending on the source material (see “Landslide Inventory Compared to Previous Studies” in Results section, or Table 10). The landslide deposits in these inventories are concentrated in the lower basin and cover about 12 mi² [31 km²] (Figure 8). Following the 1996 flood, the Oregon Department of Geology and Mineral Industries (DOGAMI) completed a new inventory of recent landslides from that winter and discovered 35 additional rapidly-moving landslides, or debris flows, in the basin (Figure 8; Hofmeister, 2000). The Bureau of Land Management (1997) also inventoried landslides for their land in the Little North Santiam River Basin and determined that most failures were small, none greater than 10,000 cubic feet (ft³) [300 cubic meters (m³)].

Previous work completed by Sobieszczyk and others (2007) examined sediment contribution from a small earth flow adjacent to Evans Creek, a tributary to the Little North Santiam River. Located on BLM land, the Evans Creek Landslide supplied much of the 10,000 T [9,000,000 kg] of sediment measured during the January 2004 turbidity event (Sobieszczyk and others, 2007). The landslide has continued to move and supply a large amount of sediment into Evans Creek and the Little North Santiam River through the winter of 2009–2010 (see “Evans Creek Landslide” in Results section). Remediation

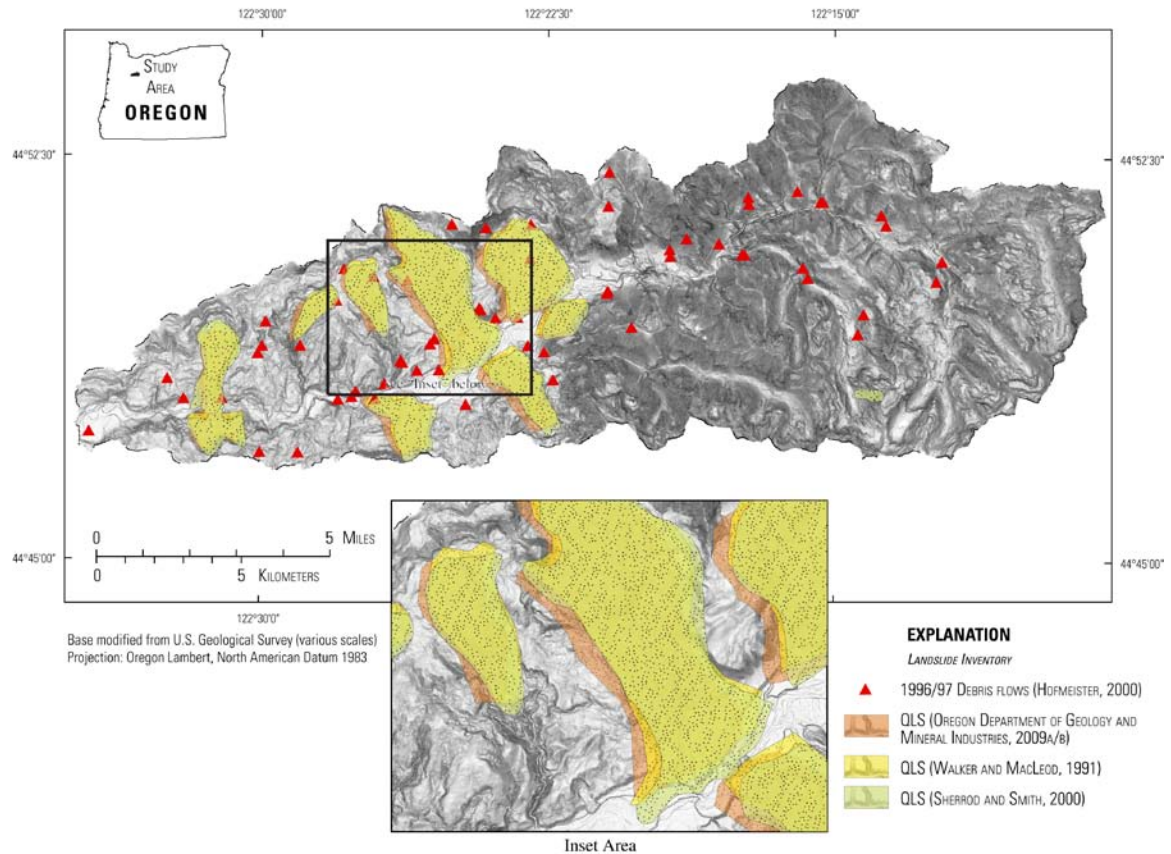


Figure 8. Previous landslide inventories completed for the Little North Santiam River Basin, Oregon (Walker and McLeod, 1991; Sherrod and Smith, 2000; Hofmeister, 2000; Oregon Department of Geology and Mineral Industries, 2009a; Oregon Department of Geology and Mineral Industries, 2009b).

work was completed by the BLM in 2009 in an attempt to stabilize the slope and reduce erosion from the landslide surface (Patrick Hawe, Bureau of Land Management, written commun., 2009).

The Evans Creek Landslide flows into Evans Creek and has its toe continuously incised by the high gradient stream (Figure 9A). Surface fractures, sag ponds, bent “pistol-butt” trees, and downed timber (Figure 9B; Figure 9C) all indicate movement of the earth flow. A centralized, scoured debris flow channel atop the landslide transports eroded material as turbid “wash” regardless of season or rainfall conditions (Figure 9D).

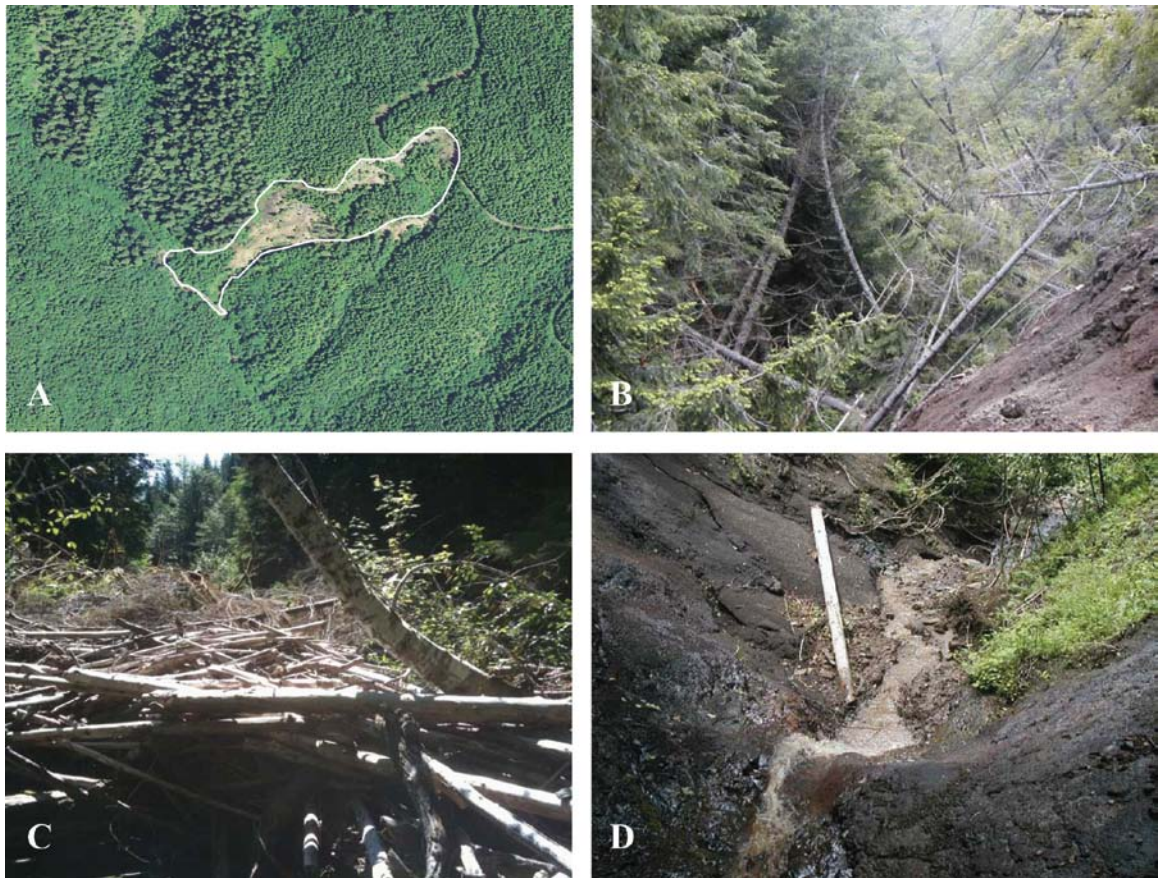


Figure 9. Photographs from the Evans Creek Landslide: A) aerial view of landslide deposit, B) Slope movement and pistol-butt trees, C) downed trees at toe of landslide along Evans Creek, and D) turbid water flowing across face of landslide (Photos: A, Oregon Geospatial Enterprise Office, 2010; B, C, D: Steven Sobieszczyk, U.S. Geological Survey, various dates).

Landslide activity and slope stability concerns also affect transportation in the basin. The greatest concern relates to a road failure of the North Fork Road near Mile Post 4 (Figure 10). Termed the “Bear Trap Slide” (GeoDesign, 2009), the earth flow continues to move and damage the roadway. The failure is part of a much larger landslide complex, one that has previously damaged parts of the road a few hundred feet west of the current damage (Landslide Technology, 1997). Marion County Public Works is currently working on a long-term solution to the Bear Trap Slide road failure.



Figure 10. Road damage near Mile Post 4 on North Fork Road caused by Bear Trap Slide (Photos: Anthony Bartuff, Portland State University, 2007; and Steven Sobieszczyk, Portland State University, 2010).

Chapter 4. Review of Literature

4.1: North Santiam River Basin Suspended Sediment and Turbidity Study

Following the flood of 1996, the City of Salem joined into a cooperative agreement with the USGS to establish a near real-time streamflow and water-quality monitoring network for the North Santiam River Basin. Beginning in 1998, the USGS began to “investigate the sources and dynamics of suspended sediment in the North Santiam River” (Uhrich and Bragg, 2003). By 2009, 11 different monitoring stations had been established across the basin, although not all sites were operational over the same period (<http://or.water.usgs.gov/santiam>). Included in the monitoring network were three stations located along the Little North Santiam River (Table 4). Two of these monitors, Stations 14182500 and 14181900, were still operational during the winter of 2009–2010 and are referenced later in this report as Station 1 and Station 4, respectively.

Table 4. Historic streamflow-gaging and water-quality monitoring stations, Little North Santiam River Basin, Oregon.

Station Reference	USGS Station No.	Period of record (water year)	Water-quality parameter				
			Water temperature	Specific conductance	pH	Turbidity	Dissolved oxygen
Little North Santiam River near Mehama, Oregon	14182500	2001 - present	X	X	X	X	X
Little North Santiam River above Evans Creek at Elkhorn, Oregon	14181900	2008 - 2010	X	X	X	X	X
Little North Santiam River below Canyon Creek near Mehama, Oregon	14182400	2008	X	X	X	X	X

The USGS suspended sediment and turbidity study changed focus in December 2009 to investigate other aspects of water quality besides turbidity, primarily algae and nutrients. Research presented in this study concludes the final sediment-related component of the near 10-year turbidity study (1998–2009). Findings from the USGS

study showed that isolated events, such as road failures and debris flows (Bragg and others, 2007; Sobieszczyk and others, 2007; Sobieszczyk and others 2008), are responsible for the largest spikes in turbidity observed in the basin; that only 14% of sediment from the North Santiam River Basin above Detroit Lake passes Detroit and Big Cliff Dams (Bragg and Uhrich, 2010); that nearly 70% of sediment that passes the drinking water treatment plant originates in the Little North Santiam River Basin (Bragg and Uhrich, 2010); and that winter storms during November, December, and January account for 80% of the sediment transported in the North Santiam River Basin (Uhrich and Bragg, 2003; Bragg and others, 2007; Bragg and Uhrich, 2010).

4.2: Similar Research in the Pacific Northwest and Elsewhere

Since this study not only examines turbidity and suspended-sediment loads, but also sediment contribution from landscape features, such as landslides, previous studies that investigated the interrelation or correlation among landslides, hydrology, land-use practices, and road construction were also reviewed. Included in this literature review are studies that addressed: how road development and timber harvesting influence erosion (Fredriksen, 1971; Mersereau and Dyrness, 1972; Swanston and Swanson, 1976; Grant and Wolff, 1991); how roads and timber harvesting affect slope stability (Morrison, 1975; Swanson and Dyrness, 1975; Swanston, 1981; Hicks, 1982; Jakob, 2000; Sidle, 2005; Bathurst and others, 2009); how land use practices affect sediment transport (Swanston and Swanson, 1976; Nolan and Janda, 1981; Amaranthus and others, 1985); and how landslides contribute to suspended sediment in streams (Swanson and others, 1987;

Burton and Bathurst, 1998; Ambers, 2001; Pearch, 2001; Korup and others, 2004; Sobieszczyk and others, 2007).

In order to put these previous studies in context with this study, first the term “sediment source” must be defined. A sediment source area refers to “any location or activity that retains, distributes, or generates sediment and has sufficient likelihood of releasing sediment into a stream or river” (Economic and Engineering Services and HDR Engineering, 2003). This means any natural landscape feature, such as a landslide, or anthropogenic landscape activity, including timber harvesting and road building, which promotes or contributes sediment to a river or stream may be considered a potential sediment source.

Historically, dominant sediment sources in the Western Cascades include debris flows, earth flows, and rotational earth slumps, as well as surface erosion caused by gully incision or stream bank erosion (Russell, 1994). Fredriksen (1971) and Sobieszczyk and others (2007) suggest that active earth flows contribute between 60% and 90% of suspended sediment observed in some Western Cascade streams, while other erosion processes, such as bank erosion, supply less than 3% of the load (Pearch, 2001).

Sediment production from landslides can be further augmented based on the type of land-use activity atop the landscape feature. Field investigations into steep forested terrains around the world show that erosion rates increase 2x to 10x within the first 3 to 15 years after an area has been recently clearcut (Wu and Sidle, 1995, Jakob, 2000; Sidle, 2005). Erosion rates are even higher (Table 5) for areas with active road building, with some studies in the Western Cascades showing erosion rates 50x to 300x higher than that of naturally-forested landscapes (Swanson and Dyrness, 1975; Hicks, 1982; Morrison, 1975).

Table 5. Landslide frequencies, volumes, and erosion rates estimated in other similar Cascades studies (modified from Amaranthus and others, 1985).

[Abbreviations: yd³, cubic yards; m³, cubic meters; ac, acre; km², square kilometers; yr, year; na, no data available]

Environment	Study Length	Average slide volume	Erosion Rate Volume	Source
	(yr)	(yd ³) [m ³]	(yd ³ /ac-yr) [m ³ /km ² *yr]	
Natural Forest				
Cascades	25	1,908 [1,468]	0.19 [36]	Swanson and Dymess (1975)
Cascades	15	2,601 [2,001]	0.24 [46]	Morrison (1975)
Middle Santiam	26	na	0.05 [9.3]	Hicks (1982)
Harvest/Clearcut				
Cascades	25	1,751 [1,347]	0.70 [133]	Swanson and Dymess (1975)
Cascades	15	575 [442]	0.62 [118]	Morrison (1975)
Middle Santiam	26	na	0.17 [31.9]	Hicks (1982)
Cascades	na	na	0.25 [48]	Elliot (2006)
Roads				
Cascades	25	1,804 [1,388]	9.36 [1,780]	Swanson and Dymess (1975)
Cascades	15	2,444 [1,880]	82.53 [15,690]	Morrison (1975)
Middle Santiam	26	na	4.69 [886]	Hicks (1982)

In addition to sediment production from the natural landscape, anthropogenic activities, such as timber harvesting, road building, mineral extraction, farming, and industrial, urban, and residential development all increase the amount of sediment transported to streams during large storms (U.S. General Accounting Office, 1998). The most abundant of these activities in the Little North Santiam River Basin is probably timber harvesting (logging). Not only does logging contribute to suspended sediment in streams (Nolan and Janda, 1981), it also increases erosion rates up to 4x more (Grant and Wolff, 1991), and increases landslide movement rates 2x to 4x faster than prior to clearcutting (Swanston, 1981). The combination of clearcutting with intense rainfall, steep slopes, and vulnerable lithologies greatly accelerates mass wasting; therefore,

increasing the amount of sediment input into streams and greatly altering the channel morphology and instream water quality (Sidle, 2005).

In addition to logging, the amount of road development and even the road network, itself, supply sediment to streams. Roads are important because they affect slope stability (Sidle and others, 1985) and increase runoff by expanding the surface flow network of a basin (Wemple and others, 1996). Roads affect hillslope stability by: 1) changing the flow characteristics and drainage of a slope; 2) concentrating water onto unstable areas; 3) undercutting slopes; 4) actively transporting sediment; and 5) possibly overburdening susceptible surfaces with fill (Sidle and others, 1985; Sidle, 2005).

Previous studies (O'Loughlin and Pearce, 1976; Gray and Megahan, 1981; Amaranthus and others, 1985; Allison and others, 2004; Sidle, 2005) indicate that roads are up to 100x more likely to initiate landslides on hillslopes than undisturbed forested terrain (Table 5). Lastly, a review of other watershed assessments indicate that up to 90% of sediment produced in a basin can originate from road–stream crossings (Gregersen and others, 2007).

Chapter 5. Methods

The methods used for this study focus on Geographic Information System (GIS) data set acquisition and processing, instream turbidity monitoring, streamflow estimation, and suspended-sediment load calculations. Methods presented here are used to characterize the basin morphology and relate how landscape features contribute sediment to streams in the Little North Santiam River Basin.

5.1: LiDAR Mapping and Other Digital Data Processing

Airborne-based LiDAR data for the Little North Santiam River Basin were collected as part of the 2008 Oregon LiDAR Consortium (OLC) Willamette Valley Phase I Acquisition. Information about data collection, processing, and quality-assurance of the LiDAR data are available through the DOGAMI OLC website (<http://www.oregongeology.org/sub/projects/olc/default.htm>). LiDAR data within the Little North Santiam River Basin boundary were collected between September 17, 2008, and July 1, 2009, with final deliverables received in December 2009. LiDAR deliverables included: 3 foot (ft)-resolution [1 meter (m)] bare earth digital elevation model (DEM) rasters; 3 ft-resolution [1 m] highest hit (first return) DEM rasters; point cloud LAS files; intensity rasters; plus, associated reports and metadata. Horizontal accuracy for the LiDAR data set was ± 1 ft [0.3 m], while vertical accuracy was ± 6 in [15 cm].

5.1.1: Landslide Inventory

5.1.1.a: Landslide Delineation

High-resolution LiDAR data were used as background imagery to aid in mapping landslide deposits, scarp flanks, and internal scarps across the Little North Santiam River Basin. Digital data sets produced, including the slopeshaded-DEM and landslide inventory geodatabase, were processed using ESRI ArcGIS 9.3 software. The landslide mapping protocol used for this study was based on standards presented in DOGAMI's Special Paper 42 (Burns and Madin, 2009). To briefly summarize, landslide deposits were viewed at 1:10,000 scale and mapped at a 1:4,000 scale, with a minimum mapping unit size of 0.5 acres [2,000 square meters (m^2)]. Landslide features outside the Little North Santiam River Basin boundary were clipped to the basin extent. Landslide features visible in LiDAR-derived imagery, such as arcuate scarps, hummocky terrain, sag ponds, terraces, or offset drainage, were all used to help identify landslide boundaries (Dikau and others, 1996). In addition, 2009 aerial photographs (Oregon Geospatial Enterprise Office, 2010) were used to aid in mapping questionable features, such as debris flow deposits, disturbed vegetative change (alder versus evergreen), and indiscernible anthropogenic features. Identification guidelines for mapping denuded slopes and creep-flow movement were influenced by previous LiDAR-based landslide inventory studies (Madin and Burns, 2006; Schulz, 2007). Figure 11 shows an example of how both aerial photographs and LiDAR imagery were used for mapping head scarp and landslide deposits. Where possible, landslides were field verified.

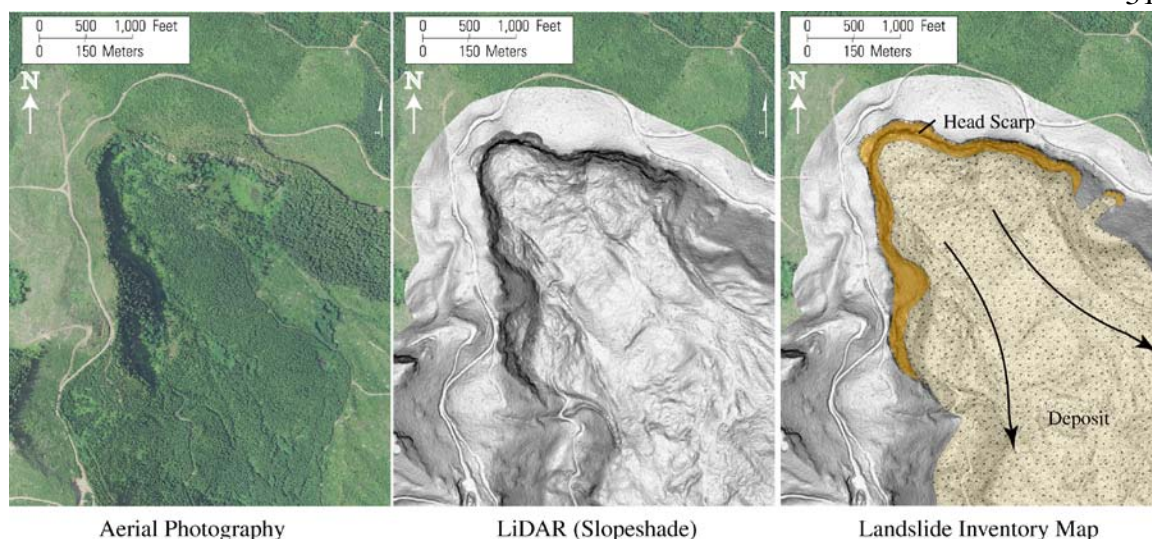


Figure 11. Landslide delineation based on aerial photographs and LiDAR mapping techniques (Burns and Madin, 2009). Landslide inventory included: landslide deposits (polygon), landslide head scarp (polygon), internal scarps (line), and photographs from site visits (points).

5.1.1.b: Landslide Classification

Landslide classification, as presented in Special Paper 42 (Burns and Madin, 2009), followed the naming conventions first presented by Varnes (1978) and later revised by Cruden and Varnes (1996) and summarized in Highland (2004). Landslide descriptions were classified based on both the type of movement and the type of failed material (Table 6). Slope failures were characterized as complex landslides when: 1) multiple, different landslide types were nested within one feature (Figure 12); or 2) where broad expanses of hillsides were denuded, hummocky, or apparently flowing (Figure 13). These expansive, complex slope failures were formed by erosion and mass wasting along rivers, yet lacked easily discernable deposits similar to those of individual landslides (Figure 13). Also, due to their size and location, complex landslides likely had material removed or modified by anthropogenic or natural processes (Schulz, 2007).

Table 6. Landslide classification based on type of movement and type of material (modified from Varnes, 1978).

TYPE OF MOVEMENT		TYPE OF MATERIAL	
		BEDROCK	ENGINEERING SOILS
			Predominantly coarse Predominantly fine
FALLS		Rock fall	Debris fall Earth fall
TOPPLES		Rock topple	Debris topple Earth topple
SLIDES	ROTATIONAL	Rock slump	Debris slump Earth slump
	TRANSLATIONAL	Rock slide	Debris slide Earth slide
LATERAL SPREADS		Rock spread	Debris spread Earth spread
FLOWS		Rock flow (deep creep)	Debris flow Earth flow (soil creep)
COMPLEX		Combination of two or more principal types of movement	

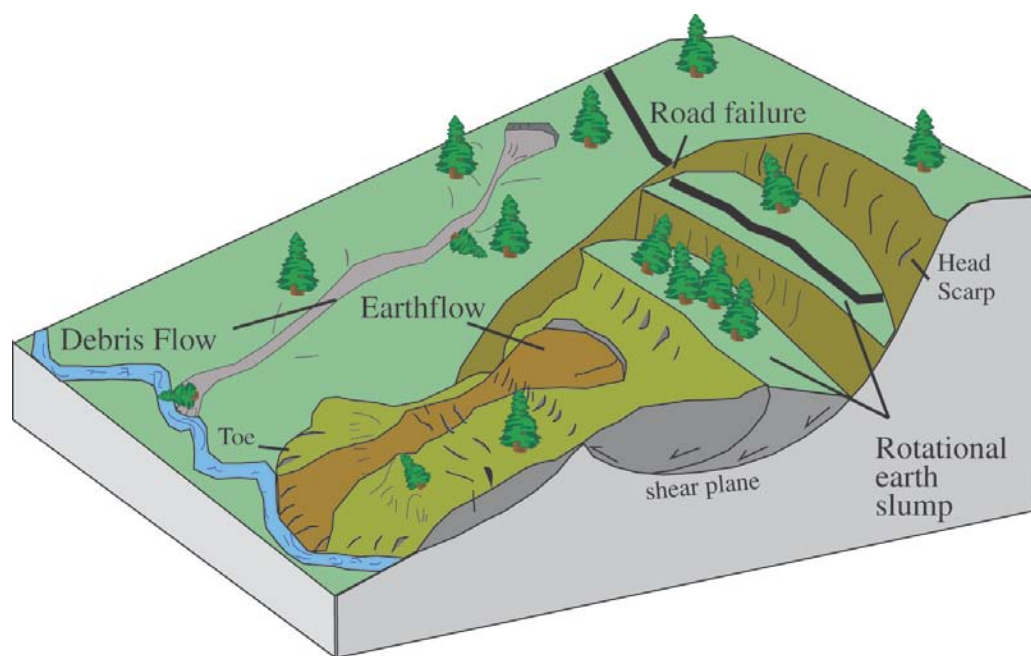


Figure 12. Illustration of landslide complex, including: earth slump, debris flow, and earth flow (modified Cruden and Varnes, 1996).

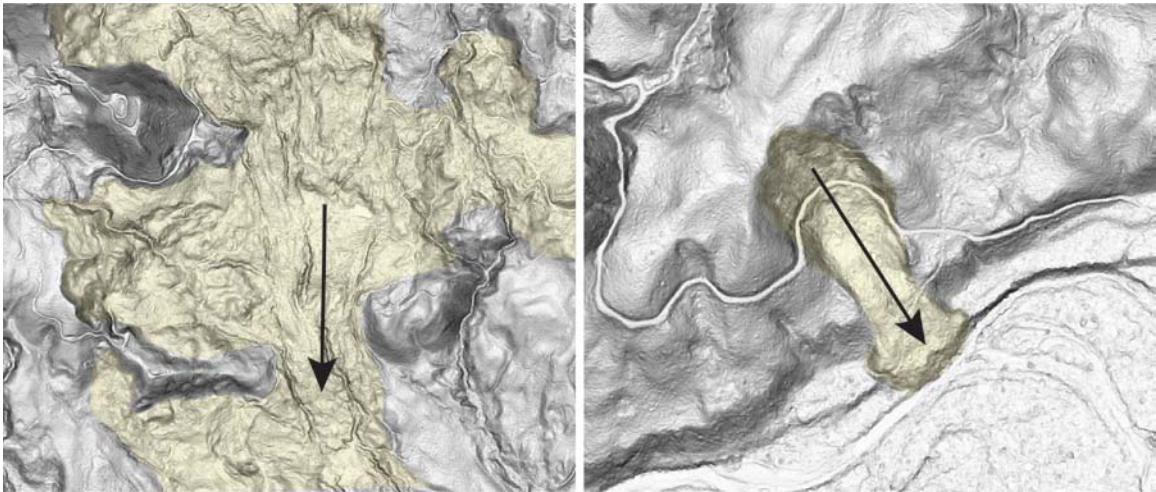


Figure 13. Comparison between complex landslide (left) and earth flow (right).

5.1.1.c: Field Verification of Mapped Landslide Deposits

The landslide inventory received limited field verification. Due to time and access constraints, only 28 of the 401 mapped landslides were visited (Appendix A.2: Landslide Inventory). Photographs were taken at each of the field-checked locations and are included in the landslide inventory geodatabase (Appendix B.1: Landslide Inventory). No field measurements or calculations were completed onsite; all information presented in this report was derived from the LiDAR-derived data sets only. The final landslide inventory for this study was quality-assurance reviewed by both the USGS and DOGAMI.

5.1.1.d: Landslide Movement Rate Analysis for the Evans Creek Landslide

Due to significant sediment contribution from the Evans Creek Landslide (see “Evans Creek Landslide” in Results section), additional landslide movement analyses

were completed for this particular earth flow. Historical aerial photographs obtained from the University of Oregon Aerial Photography Research Service (University of Oregon Library, written commun., 2010) and BLM (Patrick Hawe, Bureau of Land Management, written commun., 2010) for 1945, 1955, 1962, 1970, 1977, and 1988 were combined with recent digital orthophotographs from 1995, 2000, 2005, and 2009 (Oregon Geospatial Enterprise Office, 2010) to determine landslide movement rates over time.

Since the historic aerial photographs were not referenced to a spatial coordinate system, they were georectified using the ESRI ArcGIS 9.3 Georeference tool. Georectification error varied for each photograph, improving from ± 100 ft [30 m] in 1945 to about ± 30 ft [9 m] in 1988. The uncertainty for rectification was due to a lack of identifiable reference features, such as roads, buildings, bedrock outcrops, or even isolated trees in some of the photographs. A substantial change in vegetative cover following clearcutting prior to the 1962 photograph further reduced visual reference points between 1945, 1955, and 1962. After 1962 roads and other recognizable features were built, making rectification easier and more accurate. Recent orthophotographs were already georeferenced and no further action was required. Once the series of photographs were projected into the same reference frame, changes to landslide morphology were assessed. Where possible, three to five identical objects (trees, rocks, or roads) were identified in each photograph and measured for distance displaced. The mean distance moved for each of the objects was then divided by the time period between photographs to determine relative movement rate of the landslide. This movement rate only applies to the observed surface movement of the landslide. It does not equate to the rate of sediment input into Evans Creek.

5.1.2: Timber Harvest Change (1995-2009)

Along with mapped landslide deposits, another element inventoried for this study was recent timber harvest change. As mentioned earlier, studies have shown a strong correlation between logging with slope instability and increased erosion (Morrison, 1975; Swanson and Dyrness, 1975; Swanston, 1981; Hicks, 1982; Amaranthus and others, 1985; Grant and Wolff, 1991; DeRoo and others, 1998; Elliot, 2006). This relation exists because forest vegetation improves slope stability by controlling soil moisture through evapotranspiration and root cohesion (Sidle, 2005). This cohesion and vegetative cover also protects against soil erosion. Therefore, this timber harvest inventory was created for use as a comparative analysis tool between land management practices, landslide activity, and suspended-sediment transport.

5.1.2.a: Aerial Photographic Interpretation of Timber Harvests

Since a considerable amount of research in the Little North Santiam River Basin began after the 1996 flood, any changes to the landscape during that event, or the years after, is essential for understanding the development of the landscape. This type of chronological analysis is especially useful for comparing concurrent projects. For example, any logging completed between 2000 and 2009 corresponded to a similar time period as the USGS continuous water-quality monitoring in the Little North Santiam River; therefore, any sediment input resulting from the logging may be evident in changes in turbidity and suspended-sediment load.

Timber harvesting in the basin was inventoried for four separate time periods (Figure 14), including prior to 1995, between 1995 and 2000, between 2000 and 2005,

and between 2005 and 2009 (Oregon Geospatial Enterprise Office, 2010). Similar to the mapping protocol used in the landslide inventory, logging features were initially viewed at a 1:10,000 scale but mapped at a 1:4,000 scale. Timber plots where trees were harvested or removed were digitized and identified as clearcut, thinned, or developed (replaced with homes, campgrounds, or other infrastructure) depending on what type of land use occurred after the trees were removed. Naturally barren areas, such as rock outcrops and landslide deposits, were not included in the inventory. It is worth noting that the 1995 imagery was used solely to establish a baseline from which to map recent change; no mapped features representing the 1995 period, or earlier, were included in the final analyses.

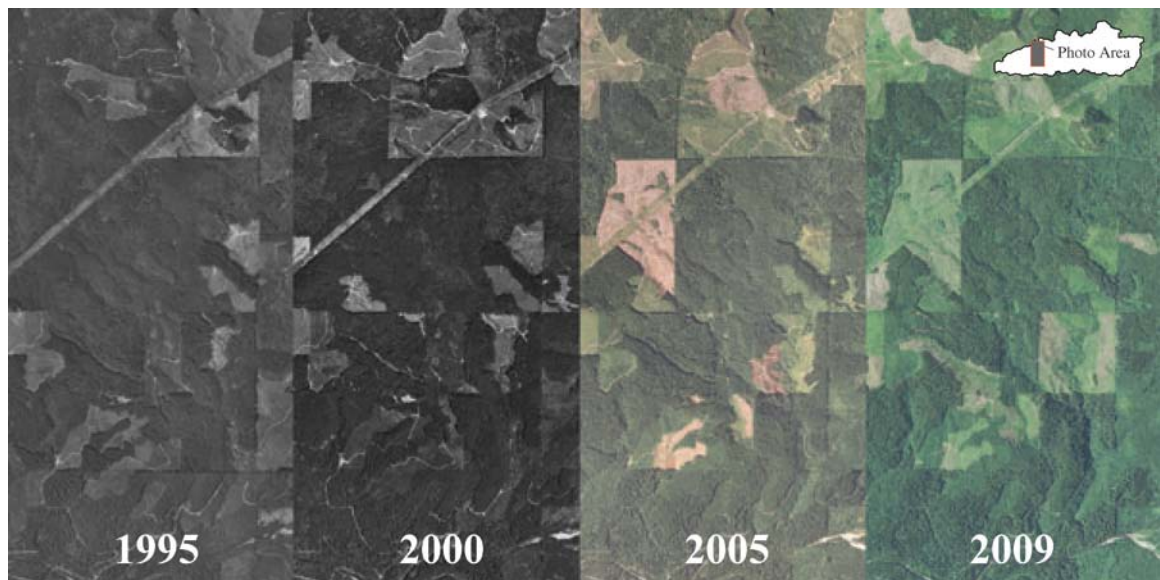


Figure 14. Example of landscape change due to timber harvesting in the Little North Santiam River Basin, Oregon, from 1995 through 2009 (Oregon Geospatial Enterprise Office, 2010).

5.1.2.b: LiDAR Rectification Techniques

Although the aerial photographs were georeferenced, there were still inherent geometric distortions present in the imagery, especially in the 1995 and 2000 photographs. Therefore, the aerial photographic interpretation exhibited a certain amount of acquisition and rectification error, such as the relief displacement was not corrected. To improve the quality of the timber harvest change data set and reduce displacement error caused by geometric distortions, the final inventory was compared to the higher-resolution LiDAR-derived imagery. The 3 ft-resolution [1 m] LiDAR data (± 1 ft [0.3 m] horizontal error) were more accurate than the georectified aerial photographs (± 18 to ± 23 ft [± 5 to ± 7 m] error; U.S. Geological Survey, 2002; U.S. Department of Agriculture, 2010), therefore, it was used to improve the accuracy of the photographic-derived data.

Using differential analysis (subtract highest hit DEM raster from bare earth DEM raster), tree canopy heights were shown for the entire Little North Santiam River Basin. Tree stands of equal age and height, as well as recently clearcut or barren areas, were easily visible in the differential raster. The final timber harvest inventory was superimposed over the differential DEM and boundaries were modified to match those represented by the differential raster. This adjustment of the timber harvest change data set allowed the inventory to match the detail and projection accuracy of the LiDAR-derived landslide inventory.

5.1.3: Hydrography (Rivers, Streams, and Gullies)

Another digital data set derived from the LiDAR-based imagery was the hydrography of the Little North Santiam River Basin. The hydrography, or river network, was mapped manually and compared against previous hydrographic data sets (U.S. Geological Survey, 1999; Horizon Systems Corporation, 2005), USGS topographic maps (U.S. Geological Survey, 2010), and other Oregon maps (Oregon Atlas & Gazetteer, 2004) to verify stream names and locations. Due to the detail of the LiDAR-derived imagery, digitization of the rivers, streams, and gullies were completed manually rather than by automated methods, which would have produced questionable results. This type of mapping allowed for a cleaner product of equal or higher quality than the computer generated stream network. Similar to both the landslide and timber harvest inventories, features were located at a 1:10,000 scale and digitized at a 1:4,000.

5.2: Continuous Turbidity Monitoring

5.2.1: Site Selection and Installation of Monitoring Equipment

Prior to this study, the USGS had been actively monitoring turbidity in the Little North Santiam River at two locations (Table 4), the USGS streamflow-gaging station “Little North Santiam River near Mehama, Oregon (14182500),” and the “Little North Santiam River above Evans Creek at Elkhorn, Oregon (14181900).” Turbidity and suspended-sediment loads from those two locations had been used previously to help quantify sediment transport in the upper and lower parts of basin (Mark Uhrich, U.S. Geological Survey, oral commun., 2008). However, due to a large disparity in measured

turbidity between the sites, for this study it was decided that additional monitoring was needed in the lower basin to help isolate potential sediment source areas between the previously established stations. Three temporary turbidity monitors were installed in the basin. Two of the turbidity monitors (Station 2 and Station 3) were placed roughly equidistant between the two preexisting stations in the Little North Santiam River, while the third monitor (Station 5) was placed at the mouth of Evans Creek (Figure 1). The new locations were chosen based on: 1) ease of access; 2) safety from theft or vandalism; and 3) likelihood for secure positioning during extreme flows. The lowest downstream monitor on the Little North Santiam River was installed at the BLM Elkhorn Valley Campground (Figure 15). The second mainstem monitor required additional scouting and communication with local residents. Eventually, a suitable location was found near the Elkhorn Valley Golf Course at a private residence (Figure 15). The turbidity monitor at Evans Creek was installed on the upstream side of the Evans Creek Bridge along North Fork Road (Figure 16). The turbidity monitors were installed in late-November 2009 and were operated at Station 2 and 3 into early-March 2010 and at Evans Creek until early-June 2010. Table 7 lists the final stations for the Little North Santiam River monitoring network deployed during this study for the winter 2009–2010.

Table 7. Turbidity monitoring stations in the Little North Santiam River Basin, Oregon, winter 2009–2010

[Abbreviations: mi^2 , square miles; km^2 , square kilometers]

Station No.	Station Reference	USGS Station No.	Drainage Area (mi^2) [km^2]
1	Little North Santiam River near Mehama, Oregon	14182500	111 [287]
2	Little North Santiam River at Elkhorn Valley Campground, Oregon	444802122271400	92 [238]
3	Little North Santiam River below Elkhorn Creek, Elkhorn Valley, Oregon	444827122242700	76 [197]
4	Little North Santiam River above Evans Creek at Elkhorn, Oregon	14181900	52 [135]
5	Evans Creek at Elkhorn, Oregon	14182000	3.4 [8.8]



Figure 15. Streamside locations of temporary turbidity monitoring stations on the Little North Santiam River: Station 2 at Elkhorn Valley Campground and Station 3 at private residence below Elkhorn Creek (Photos: Steven Sobieszczyk, Portland State University, 2010).



Figure 16. Streamside location of Evans Creek turbidity monitor [Station 5] (Photos: Steven Sobieszczyk, Portland State University, 2010).

5.2.2: Data Collection and Calibration of Field Instrumentation

YSI multiparameter 6920 datasondes with 6026 turbidity probes that were encased in a segment of PVC pipe and weighted with roughly five pounds (lbs) of linked chain were used at Stations 2 and 3 (Figure 17). Due to a higher risk of damage, a PVC pipe mounting was used at Evans Creek rather than a weighted pipe segment (Figure 16). Turbidity readings, in FNU, were recorded every 30 minutes. To ensure data quality, sites were visited every four weeks for calibration and data download. Data collection and final records were processed according to USGS water-quality record protocols (Wagner and others, 2006). The official period of record for the winter 2009–2010 monitoring was December 1, 2009 through February 28, 2010.



Figure 17. YSI 6920 datasonde with 6026 turbidity probe and deployment casing for temporary monitoring stations along the Little North Santiam River Basin, Oregon (Photos: Steven Sobieszczyk, Portland State University, 2009).

5.3: Methods Used for Data Processing

5.3.1: Streamflow Estimates for Monitoring Locations

5.3.1.a: Estimating Streamflow Based on Drainage Area

Continuous streamflow data was required to estimate suspended-sediment loads for each station. Continuous streamflow values were only available for the two previously established stations (Station 1 and 4, respectively); therefore, streamflow needed to be estimated for Stations 2 and 3. Streamflow can be estimated at unknown locations using a drainage-area ratio combined with streamflow measurements from a nearby known station (Emerson and others, 2005). The equation used to estimate streamflow is:

$$Q_x = \left(\frac{A_x}{A} \right) * Q \quad \text{(EQUATION 1)}$$

where Q_x is the estimated streamflow (cubic feet per second; ft^3/s) for the unknown station; A_x is area (mi^2) upstream of the unknown station; A is the area (mi^2) upstream of a nearby known streamflow-gaging station; and Q is streamflow (ft^3/s) from nearby known streamflow-gaging station. This equation was modified for use with two known gaging stations along a single river, one station located upstream and one located downstream of unknown station, by altering it as follows:

$$Q_x = \left[\left(\frac{A_a - A_x}{A_a - A_b} \right) * (Q_a - Q_b) \right] + Q_b \quad \text{(EQUATION 2)}$$

where Q_x is the estimated streamflow (ft^3/s) for the unknown station; A_x is area (mi^2) upstream of the unknown station; Q_a is streamflow (ft^3/s) at downstream station (Station 1); A_a is area (mi^2) upstream of downstream station (Station 1); Q_b is streamflow (ft^3/s) at upstream station (Station 4); and A_b is area (mi^2) at upstream station (Station 4). For this method the known streamflow from the upstream station (Station 4) is removed, and then streamflow is estimated for the unknown station before the subtracted upstream streamflow is reincorporated. This method eliminates overestimation of streamflow at the unknown station while retaining known upstream conditions. This is not the first time that the drainage area equation has been modified to improve streamflow estimates. Other studies have altered the equation to estimate low-flow statistics in rivers and streams (Ries and Friesz, 2000) and to estimate streamflow at a known gaging station that had missing continuous stage data (Rantz and others, 1982).

The modified streamflow estimation technique was tested and verified by using 12 months (October 2007 to September 2008) of known streamflow data measured at the former USGS streamflow-gaging station “Little North Santiam River below Canyon

Creek near Mehama, Oregon (14182400)” (Figure 18). Streamflow data estimated using equation 2 was within 5% of actual measured streamflow at the station. Using the original Equation 1 underestimated the streamflow by over 10% (Figure 18).

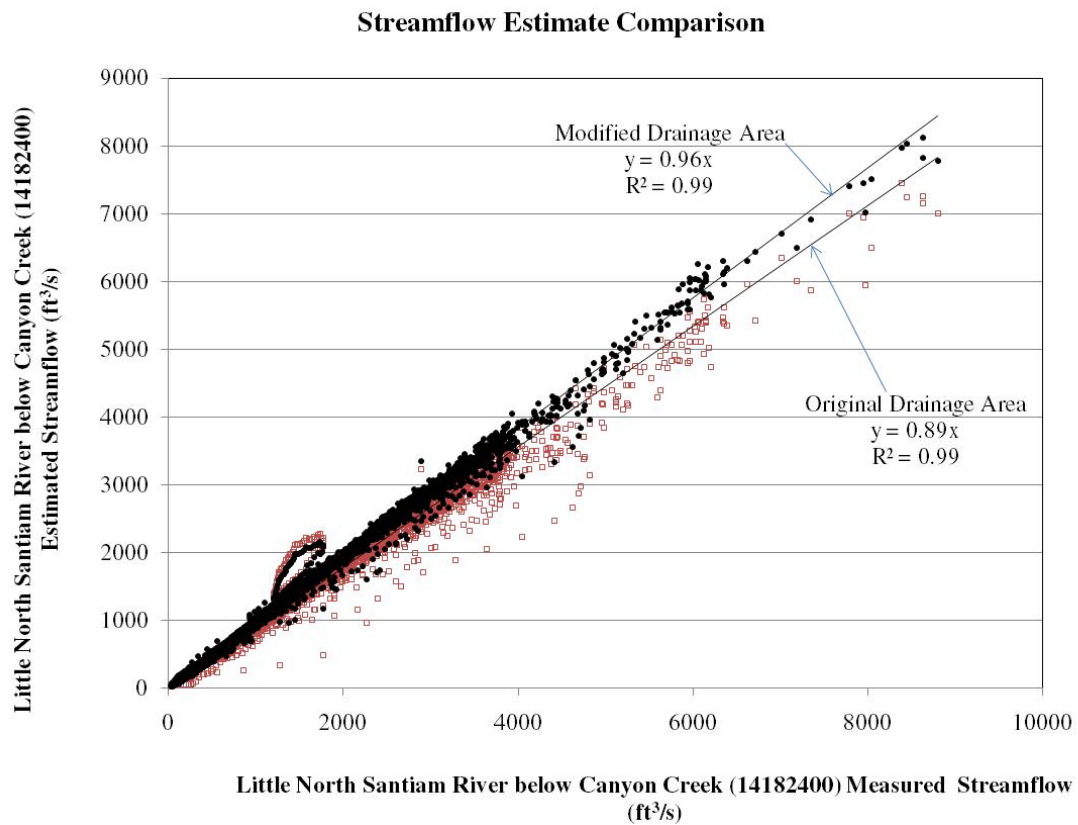


Figure 18. Streamflow comparison between known streamflow and estimated streamflow for USGS stream-gaging station Little North Santiam River below Canyon Creek near Mehama, Oregon (14182400).

5.3.1.b: Estimating Streamflow Based on Discharge Measurements

In some instances continuous streamflow data is not available upstream or downstream of the desired unknown location. For these cases streamflow can be estimated from discharge measurements that are collected onsite. Using a regression model (Figure 19), discrete discharge measurements (Station 5) can be compared with

known streamflow from a nearby station (Station 4). If the two stations share a strong correlation, the continuous streamflow from the nearby station can then be used as a surrogate to estimate streamflow at the unknown station. This method is similar to the approach commonly used by the USGS to estimate streamflow for periods of missing data within an established streamflow record (Rantz and others, 1982).

For the Evans Creek station (Station 5) six discharge measurements (n=6) were collected between November 2009 and April 2010 and compared against streamflow readings recorded at the same time at Station 4 (Figure 19). This regression model and associated equation were then used to estimate streamflow for Station 5.

$$Q_x = 0.07 * Q^{0.94} \quad \text{(EQUATION 3)}$$

where Q_x is the estimated streamflow (ft^3/s) for the unknown station (Station 5); and Q is the continuous streamflow (ft^3/s) at a nearby known station (Station 4).

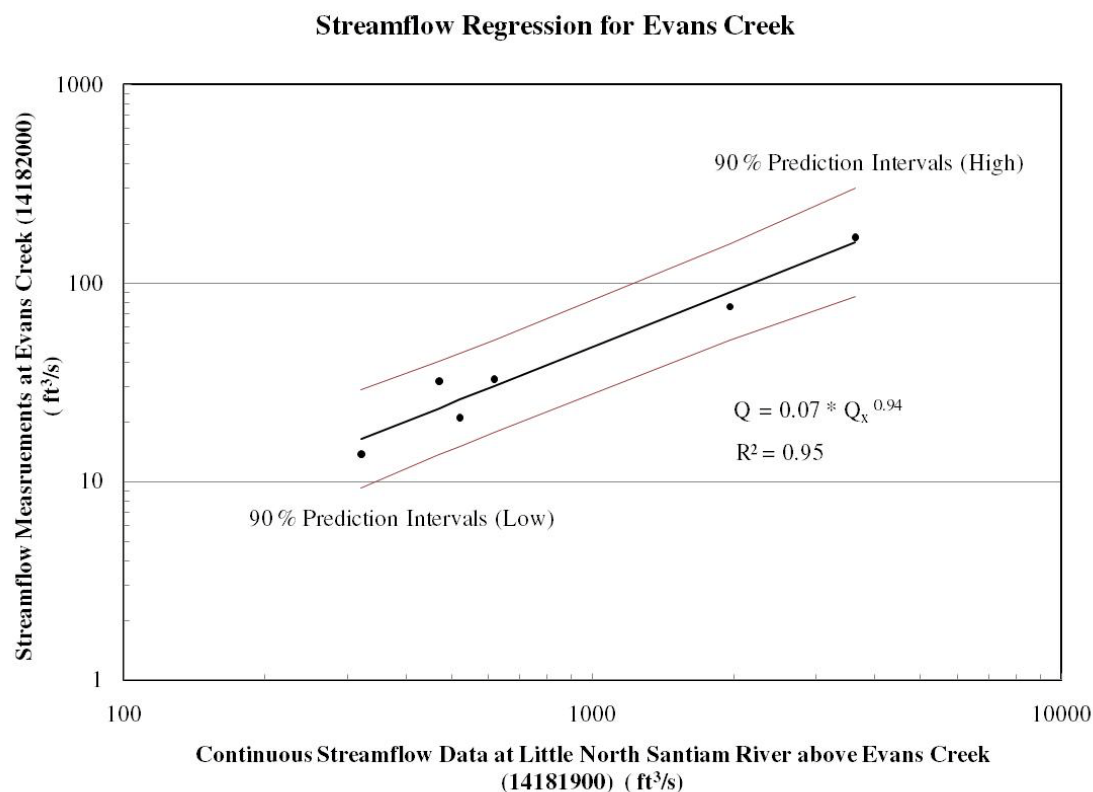


Figure 19. Regression model representing the relation of discharge measurements at Evans Creek (Station 5) and continuous streamflow data at Little North Santiam River above Evans Creek (Station 4), winter 2009–2010.

5.3.2: Estimating Suspended-Sediment Loads

5.3.2.a: Little North Santiam River (Stations 1 through 4)

Suspended-sediment load calculations for this study are based on methods developed by the USGS and used previously in the North Santiam River Basin (Uhrich and Bragg, 2003; Bragg and others, 2007; Bragg and Uhrich, 2010). Using a regression equation that relates instream turbidity to sampled suspended-sediment concentrations (Figure 20), continuous turbidity measurements can be used to estimate continuous

suspended-sediment loads. These concentrations are multiplied by continuous streamflow data to estimate suspended-sediment loads (Equation 4).

Starting in 2001, the USGS collected nearly 10 years of monitoring data and 131 suspended-sediment samples (n=131) at Station 1 (Appendix A.1: Suspended-Sediment Samples at Station 1 near Mouth of Little North Santiam River). The correlation between sediment concentration and turbidity (Figure 20) creates a regression model such that continuous instream turbidity can be used to estimate instantaneous suspended-sediment concentrations. Also, the samples collected at this location had turbidity readings between 0 and 410 FNU, well above the range of 0 to 90 FNU observed in the Little North Santiam River during this study. The regression equation established for Station 1 was applied to each of the four mainstem stations (Bragg and Uhrich, 2010):

$$SSL = (1.81 * T^{1.02}) * Q \quad \text{(EQUATION 4)}$$

where SSL is the suspended-sediment load (short tons, T) for a station; T is the turbidity (in FNU) for each station; and Q is 30-minute continuous streamflow (ft³/s) data for the station.

Although a turbidity–suspended-sediment concentration regression existed for Station 4, the short period of record (from 2008 to 2010), limited number of samples collected (n=6), and a regression similar to Station 1 (Figure 20) signify that the Station 1 regression can be used for the four Little North Santiam River stations.

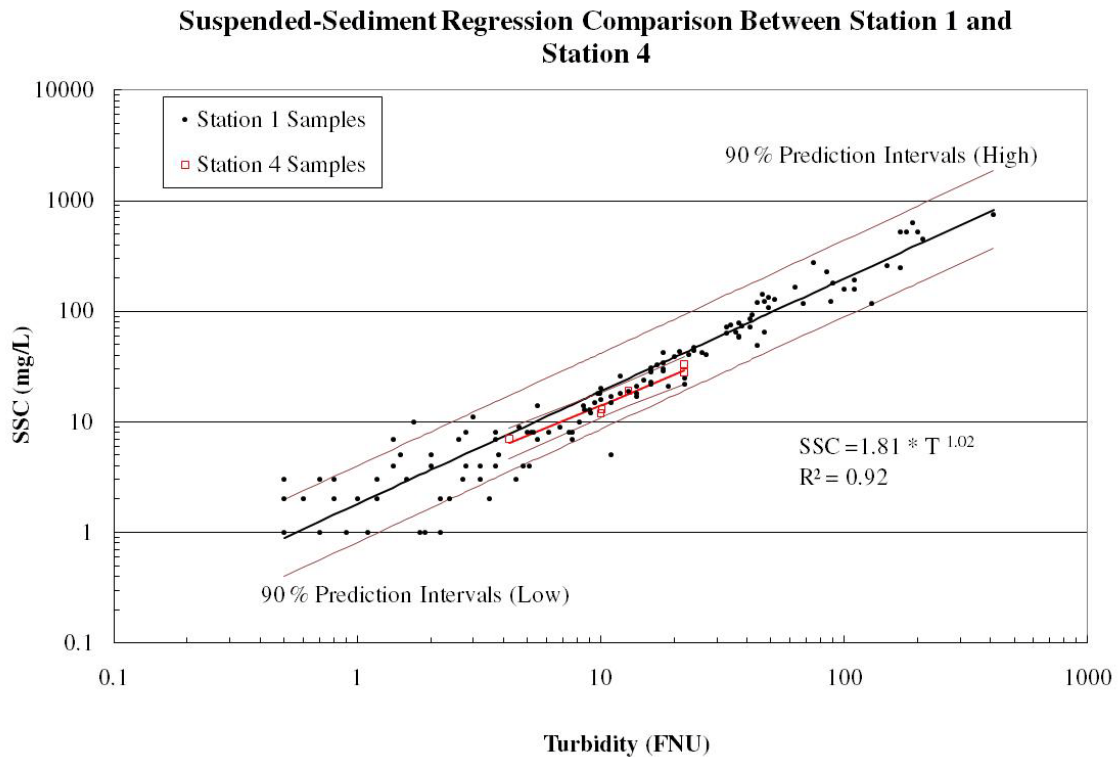


Figure 20. Regression model comparison between turbidity and suspended-sediment concentration for Little North Santiam River at Station 1 and Station 4.

5.3.2.b: Evans Creek (Station 5)

Since the sediment production history is different for Evans Creek compared to the mainstem stations, a new regression was created (Figure 21). Suspended-sediment load calculations for Evans Creek were based on a sample set of 13 suspended-sediment samples (n=13) collected onsite from December 2009 to April 2010. Samples had suspended-sediment concentrations that ranged between 0 and 120 FNU (Table 8). This range of turbidity values was low compared to instream turbidity monitoring (Figure 30), which increases the potential for underestimating suspended-sediment loads at high

turbidities. However, with there being the data available, it was the only suitable option.

The regression equation for Evans Creek is as follows:

$$SSL = (1.19 * T^{1.06}) * Q \quad \text{(EQUATION 5)}$$

where SSL is the suspended-sediment load (T) for a station; T is the turbidity (in FNU)

for each station; and Q is 30-minute continuous streamflow (ft³/s) data for the station.

Due to the limited number of samples and the short sample history (winter 2009–2010), the error associated with this regression (Figure 21) is much greater than that of the Little North Santiam River regression.

Table 8. Suspended-sediment samples collected for Evans Creek.

[**Abbreviations:** FNU, Formazin Nephelometric Units; ft³/s, cubic feet per second; m³/s, cubic meters per second; SSC, suspended-sediment concentrations; mg/L, milligrams per liter; na, no data available]

Date & Time	Sample Type	Turbidity (FNU)	Streamflow (ft ³ /s) [m ³ /s]	SSC (mg/L)	% Fines
12/16/09 15:56	Equal Width Integrated	50	205 [5.8]	78	na
12/17/09 8:59	Equal Width Integrated	75	225 [6.4]	54	na
12/22/09 13:15	Equal Width Integrated	40	177 [5.0]	33	na
1/16/10 14:10	Equal Width Integrated	99	70 [2.0]	74	na
2/26/10 10:30	Equal Width Integrated	27	36 [1.0]	26	na
3/29/10 9:36	Equal Width Integrated	450	147 [4.2]	871	na
3/29/10 11:30	Equal Width Integrated	320	166 [4.7]	867	na
3/30/10 12:55	Equal Width Integrated	140	164 [4.6]	226	69%
3/30/10 13:30	Equal Width Integrated	91	158 [4.5]	183	68%
4/7/10 11:19	Equal Width Integrated	10	149 [4.2]	13	64%
4/9/10 11:49	Equal Width Integrated	15	30 [0.8]	23	79%
4/9/10 12:00	Equal Width Integrated	15	30 [0.8]	21	80%
4/22/10 12:45	Equal Width Integrated	12	14 [0.4]	30	48%

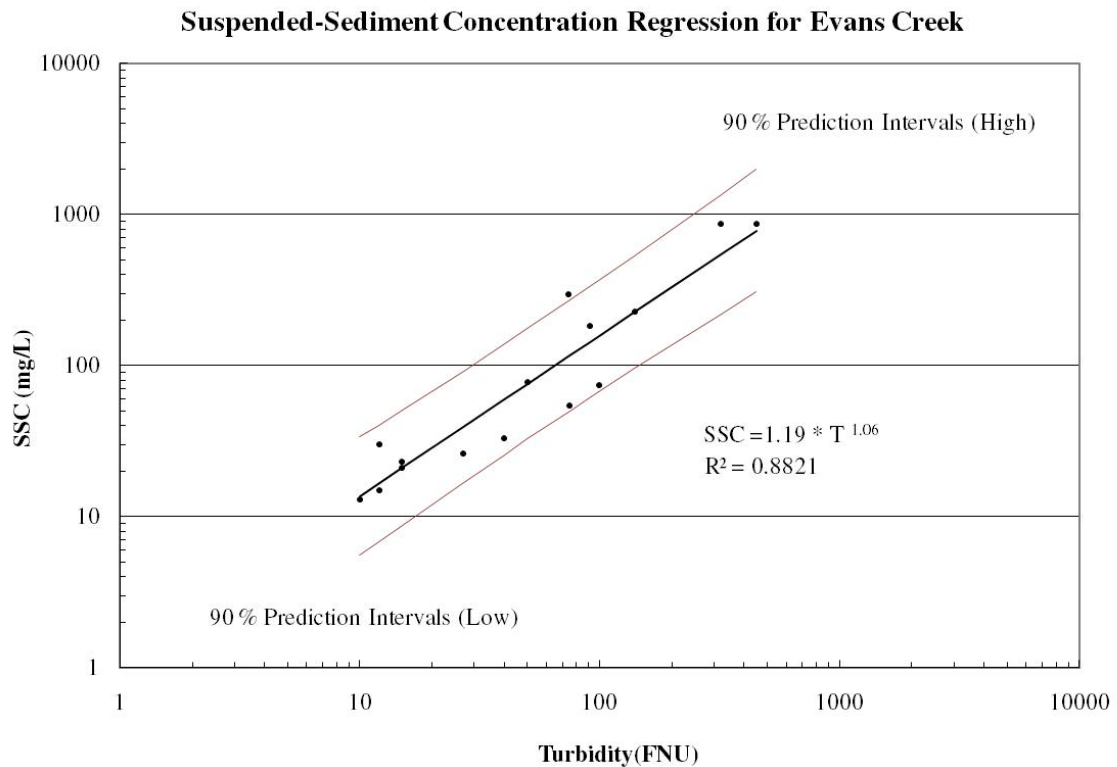


Figure 21. Regression model for the relation of turbidity and suspended-sediment concentration at Evans Creek (Station 5), winter 2009–2010.

5.3.3: Calculating a Sediment Delivery Ratio

One aspect of sedimentation that is often discussed in sediment transport studies is how to quantify the transport efficiency of a river since not all soil eroded from the watershed surface is carried out of the watershed (Walling, 1983). Numerous studies (U.S. Department of Agriculture, 1972; Boyce, 1975; Ferro and Minacapilli, 1995; Julien, 1995; Ouyang and Bartholic, 1997; Lu and others, 2006; Vanoni, 2006) have presented a variety of models or calculations that can be used to estimate a sediment delivery ratio for a watershed. The sediment delivery ratio should equal the percent of

surface material eroded that is actually transported downstream. Or, in mathematical terms:

$$SDR = \frac{S_y}{S_e} \quad (\text{EQUATION 6})$$

where SDR is the sediment deliver ratio (unitless value); S_y is the sediment yield (short tons per square mile; T/mi^2); and S_e is the gross erosion (T/mi^2) of the upstream watershed (Julien, 1995; Ouyang and Bartholic, 1997). Depending on the size of the study area and the data available, different techniques are used to determine the sediment delivery. There are three basic options: 1) the Universal Soil Loss Equation (USLE; Wischmeier and Smith, 1978); 2) empirical modeling; or 3) single parameter-derived equations. The USLE is the most popular method for estimating erosion and has been “modified” (MUSLE; Williams, 1975) and “revised” (RUSLE; Renard and others, 1997) to improve its functionality. It was originally designed for flat, uniform, agricultural regions and does not necessarily perform as well on steep, forested terrains (as tested in this study).

Other complex models (GeoWEPP; Renschler, 2008; SHETRAN; Ewen and others, 2000) simulate expected erosion and sediment production based on various processes that control sediment delivery, including rainfall, soil erodibility factor (k-factor), slope-length factor, land cover and land use, erosion-control practice factor, and stream incision (slope-steepness factor). However, these models require a variety of input parameters based on field measurements that are used to calibrate and verify model effectiveness. Without available erosion data, it is not possible to accurately run these models.

Lastly, models based on single-parameter equations, such as a slope–erosion or drainage area–erosion relation, are simple but effective because “sediment yield rates will decrease as the average slope decreases, reflecting a decrease in the efficiency of overland sediment transport” (Boyce, 1975). Due to the large drainage area, lack of site-specific erosion measurements, and presence of landslides as sediment sources, the sediment delivery ratio used in this study is based on two single-parameter equations that use a predefined drainage area–erosion relation (U.S. Department of Agriculture, 1972; Boyce, 1975; Julien, 1995; Vanoni, 2006). The first equation for the sediment delivery ratio is from Vanoni (2006) and it states:

$$SDR = 0.42 * A^{-0.13} \quad \text{(EQUATION 7)}$$

where SDR is the sediment delivery ratio; and A is basin area (mi²). Equation 7 differs from a similar drainage area–erosion relation equation described in Julien (1995) based on work completed by Boyce (1975), which states:

$$SDR = 0.31 * A^{-0.30} \quad \text{(EQUATION 8)}$$

where SDR is the sediment delivery ratio; and A is basin area (mi²).

Since the description of error analysis for these models was limited and because there are different sediment delivery ratios calculated by each, the gross sediment erosion results discussed in this report will represent a range between these two methods.

Chapter 6. Results

6.1: Landslide Inventory

6.1.1: Landslide Variability and Distribution

The size, variability, and distribution of landslides in the Little North Santiam River Basin are similar to what was mapped in other Western Cascade watersheds (Oregon Department of Geology and Mineral Industries, 2009a). However, few other studies have compiled as detailed of a landslide inventory as presented here. In total, there are 401 unique landslide deposits mapped in the basin, with hundreds more smaller landslides left unmapped that are below the predefined 0.5-acre minimum mapping unit for this study (Table 9). Included in the inventory are 143 “nested” landslides that are self-contained within larger landslide deposits. Of the 401 landslide deposits, 268 are classified as prehistoric (>150 years old). Conversely, 133 landslides display recent movement characteristics and have likely failed within the last 150 years. The most abundant landslide type is earth flow, with 190 discrete failures. Earth flow deposits comprise over a quarter (26%) of all mapped landslide deposits in the basin. When combined with earth flow-dominated complex landslides, these deep-seated failures constitute 90% of the total extent of landslide deposits in the Little North Santiam River Basin. Earth flows have relatively moderate gradient failure planes (mean slope of 24°) but are seen on slopes as shallow as 8°.

The second most common landslide classification is debris flow. Individual debris flow deposits are much smaller than earth flow deposits and populate nearly every upper basin catchment (Figure 22). Although there are nearly as many debris flows as earth flows, 164 and 190, respectively, their depositional area is 1/5th as large. Debris flows

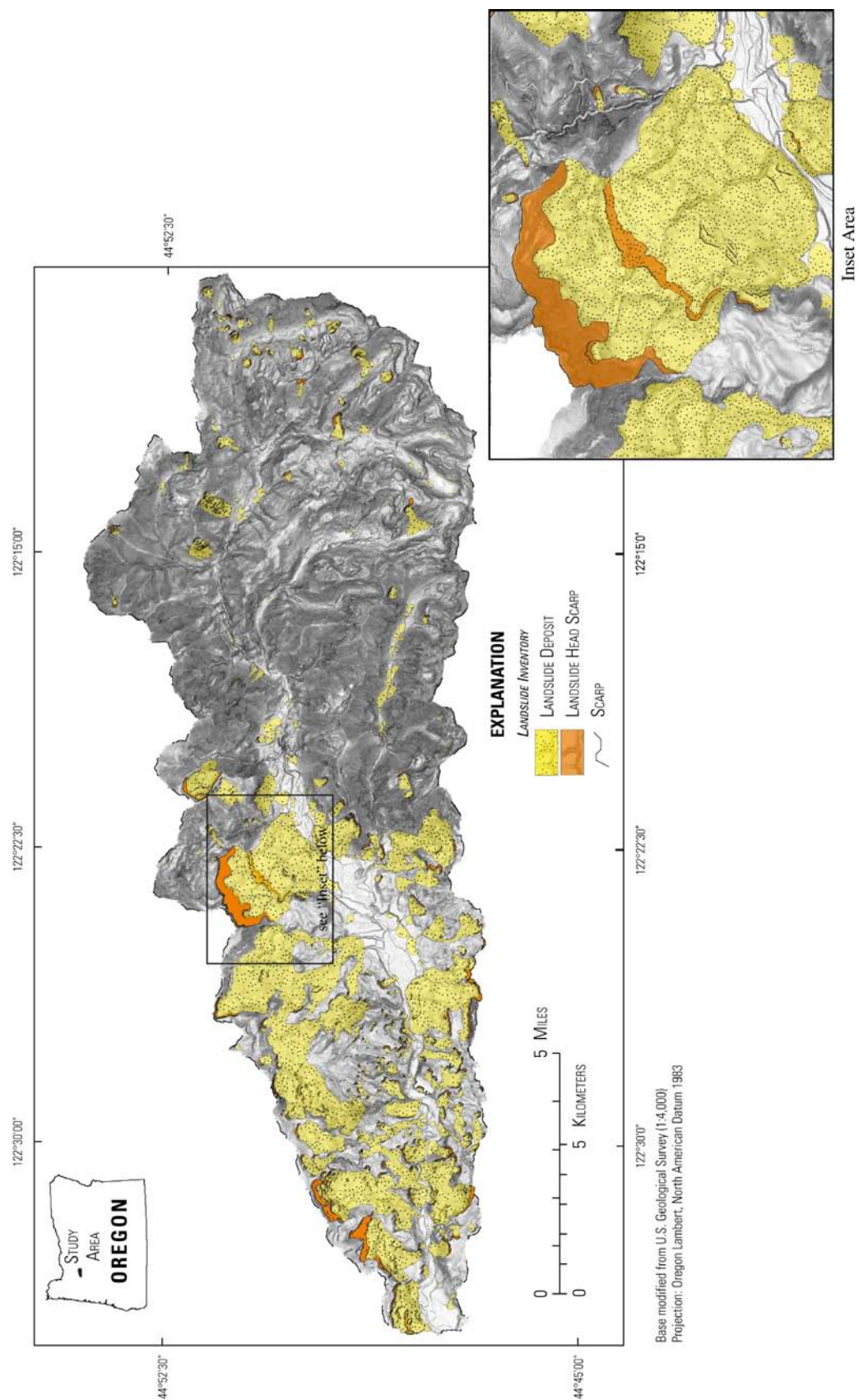


Figure 22. LiDAR-based landslide inventory for the Little North Santiam River Basin, Oregon, with inset of the Fawn Creek Landslide.

occur on much more variable slopes, with slopes ranging between 3° to 40° (mean slope of 18°). This variability is likely due to a greater potential for mapping error with these deposits compared to other landslide types. Debris flow deposits are found on both steep-sloped valleys and gradual-sloped valley floors.

Table 9. Number and extent of individual landslide deposits by movement type (including nested landslide deposits).

[Abbreviations: mi², square miles; km², square kilometers]

Type	Count	Area (mi ²) [km ²]	% of Area (Landslide Deposits)	% of Area (Basin)
Earth Flow	190	7 [19]	26%	4%
Debris Flow	164	2 [5]	5%	1%
Complex	21	18 [46]	64%	16%
Rock Fall	13	0.4 [1.1]	2%	0.4%
Earth Slide-Rotational	9	0.5 [1.2]	2%	0.4%
Earth Slide-Translational	4	0.4 [1.1]	2%	0.4%
Total	401	28 [73]	100%	22%

Individual landslide deposits cover 28 mi² [73 km²] (Table 9), however, since some landslides are nested within others, there is actually closer to 24 mi² [62 km²] of deposits spread across the Little North Santiam River Basin (Figure 22). This equates to roughly 22% of the total basin extent. The distribution of deposits is uneven, with 37% of lower basin (Reach A, B, and C) underlain by landslides compared to only 4% of the upper basin (Reach D). Generally, each reach decreases in landslide density going upstream compared to the adjacent downstream reach. For example, 45% of Reach A is covered with landslide deposits, followed by 46% of Reach B, 25% of Reach C, and 4% of Reach D. Of the top 12 largest landslide deposits ten are classified as complex landslides, each located in the lower basin. The largest of these complexes covers over 6

mi², including most of Sinker Creek, Little Sinker Creek, and Big Creek watersheds.

Most landslides are in the northern half of the basin on south-facing slopes.

Discrete landslide deposits have a wide range in size. The biggest individual landslide feature, the Fawn Creek Landslide (Figure 22, inset), is so large (2.8 mi² [7 km²]) that it failed along a nearly 800 ft [240 m] head scarp on Lookout Mountain. The original landslide failure was mapped as prehistoric (> 150 years old), yet there have been periods of recent movement at the toe (Figure 23), as well as multiple, historic nested failures within the landslide. The original landslide likely failed in response to a large subduction zone earthquake (Scott Burns, Portland State University, oral commun., 2009). During that same seismic event a smaller earth flow across the river failed, as well, joining the Fawn Creek Landslide to dam the Little North Santiam River. Detailed information on each landslide is found in Appendix A.2: Landslide Inventory, while directions for downloading the entire landslide inventory geodatabase are found in Appendix B.1: Landslide Inventory.



Figure 23. Trail along toe of Fawn Creek Landslide at Salmon Falls State Park (Photo: Steven Sobieszczyk, Portland State University, 2009).

6.1.2: Landslide Inventory Compared to Previous Studies

The accuracy of the LiDAR-derived imagery produces a landslide inventory map (Figure 22) that exceeds the detail of those produced from previous surveys (Figure 8). This improvement is demonstrated by comparing the landslide statistics between the surveys (Table 10). The inventory completed for this study documents 50x more landslides, as well as over 2x more depositional extent than previous studies (Table 10). The locations of the largest deposits are similar between the inventories; however, the margins of the landslides vary considerably. DeRoo and others (1998) suggest that older

landslide inventories that use aerial photographic analysis and some field verification underestimate the number of deposits because dense vegetation obscures many of the deep, expansive complex landslide deposits seen in the Western Cascades. In addition, the coarseness of previous mapping scales (1:500,000) means that smaller features, such as debris flow scars and deposits, were not included in the previous inventories. The Little North Santiam River Basin has over 400 landslide deposits, which equates to nearly 1 every 3.5 mi² [9 km²].

Table 10. Comparison between number of landslides from current and previous landslide inventories in the Little North Santiam River Basin, Oregon.

[Abbreviations: mi², square miles; km², square kilometers]

Landslide Deposit Statistics									
Reach A		Reach B		Reach C		Reach D		Total	
# of Landslides	Area (mi ²) [km ²]	# of Landslides	Area (mi ²) [km ²]	# of Landslides	Area (mi ²) [km ²]	# of Landslides	Area (mi ²) [km ²]	# of Landslides	Area (mi ²) [km ²]
2	1.9 [4.9]	3	5.5 [14]	2	4.1 [11]	0	0.0 [0.0]	7	12 [30]
2	2.1 [5.5]	3	5.3 [14]	3	4.3 [11]	0	0.0 [0.0]	8	12 [31]
4	2.5 [6.4]	2	4.5 [12]	3	4.6 [12]	1	0.1 [0.3]	10	12 [30]
140	8.5 [22]	59	7.3 [19]	93	5.9 [15]	109	2.3 [5.9]	401	24 [62]
									Source
									Walker and MacLeod (1991)
									Sherrod and Smith (2000)
									Oregon Department of Geology and Mineral Industries (2009a)
									Sobieszczyk - this study

6.1.3: Bedrock Geology and Landslide Deposits

A correlation between landslide occurrence and geologic units is shown in Figure 24. Since most of the basin is mapped as undifferentiated tuff (Tu), most of the landslide deposit extent (primarily complex landslides and earth flows) is contained within this unit. Although the abundance of landslides is high for this geologic unit (195 of the 401 deposits), due to its extent, the areal percentage of landsliding for the unit is relatively low (15% of the undifferentiated tuff area). The two most extensive landslide lithologies are Quaternary landslide deposits (Qls) at 74% and Tertiary Columbia River Basalts (Tc) at 86%. The “Qls–mapped landslide deposit” relation is appropriate given that mapped

landslide deposits should occur within mapped Quaternary landslide deposits; however, the “Tc–mapped landslide deposit” requires some clarification. There is a very small area of Tc located along the northern extent of the lower basin (Figure 3). This unit is almost completely contained within the mapped extent of two of the massive landslide complexes. Similar to how the large extent of the tuffaceous unit (Tu) deemphasizes the importance of the abundant landslide deposits, the limited extent of the Columbia River Basalt (Tc) overemphasizes its importance for the frequency of landsliding. The fact that the mapped landslide deposits (Qls) and LiDAR-based landslide inventory is not 100% is likely caused by the difference in resolution between mapping techniques between the different studies.

There are three units that have a sufficient abundance ($n > 10$) and extent ($> 15\%$ of the lithologic unit area) to indicate a possible causal relation between the underlying geology and the presence of landslides: Qt, Tfc, and Tba. These units represent the undifferentiated flows, clastic rocks, and tuffs (Tu and Tfc) that interact with the recessional overlying basalt cap (Tb and Tba). In addition, there are isolated failures within weakly-consolidated Quaternary terrace deposits (Qt) that are undercut by streams and rivers, as well as abundant debris flow deposits atop valley floor terrace deposits.

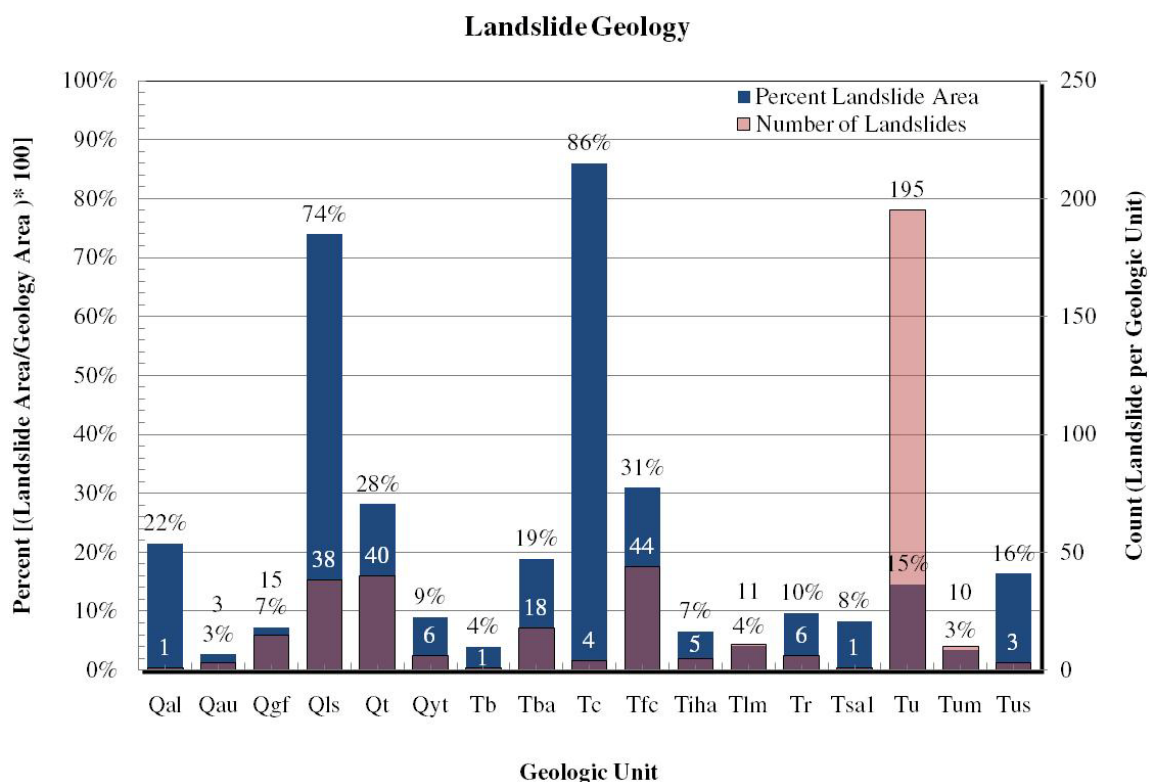


Figure 24. Number and size of landslide deposits, by geologic unit (Oregon Department of Geology and Mineral Industries, 2009b), in the Little North Santiam River, Oregon.

6.2: Evans Creek Landslide

Due to the influence Evans Creek has on suspended-sediment loads in the Little North Santiam River, special emphasis has been placed on its primary sediment supply source, the Evans Creek Landslide.

6.2.1: Earth Flow Description

The Evans Creek Landslide is a 23-acre [0.09 km²] active earth flow. The landslide measures from head scarp to toe at 1950 ft [600 m] long, 500 ft [150 m] wide, and between 10 and 30 ft [3 and 9 m] deep (Figure 25). The landslide has at least three

primary flow zones or regions of “nested” failures. The Evans Creek Landslide is located on the western flank of Evans Mountain and flows nearly due west at an aspect of 247.5° . The earth flow rests on a 30° to 35° slope.

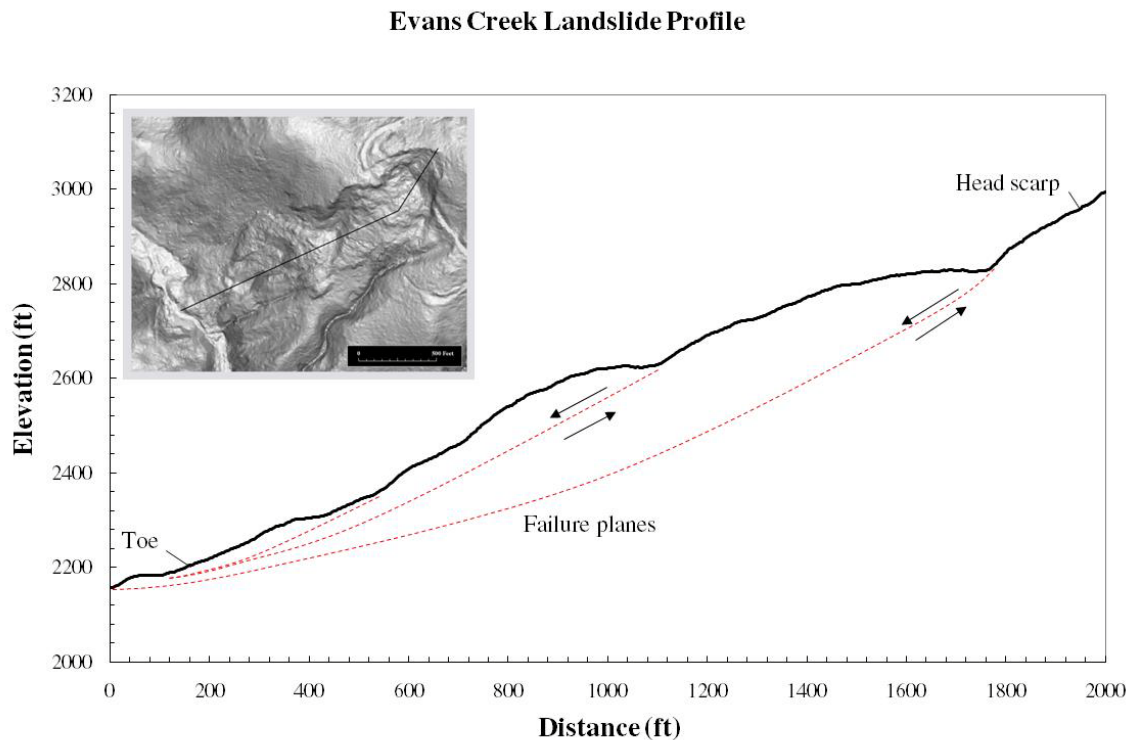


Figure 25. LiDAR-based cross-sectional profile of Evans Creek Landslide.

6.2.2: Landslide Movement History

Historical aerial photographs (Figure 26) for the Evans Creek Landslide area date back to 1945 and are available for as recently as 2009 (Patrick Hawe, Bureau of Land Management, written commun., 2010; Oregon Geospatial Enterprise Office, 2010; University of Oregon Library, written commun., 2010). In the earliest photograph (1945) visible changes to the canopy cover and surface exposures indicate that some minor slope

movement was present; however, due to dense vegetation, much of the earth flow is obscured. By 1955, a fresh landslide deposit and downed timber indicate that a massive failure had occurred. The period 1945-1955 shows the first evidence of the earth flow entering Evans Creek and likely marks the beginning of landslide-related turbidity problems in the stream. By 1962, much of the area had been harvested and developed with a network of logging roads. Before 1977 a second massive failure occurred, eliminating much of the young coniferous regrowth atop the landslide surface. The hillside appears to have stabilized for much of the 1980s and early 1990s, as very little movement is visible in photographs between 1988 and 1995. During this period much of the forest was able to regrow on the hillside, restabilizing parts of the slope. However, by the time of the 2000 imagery a third massive failure occurred. This remobilization occurred during the flood of February 1996 and washed out parts of the Evans Mountain Road (Jerry Pierce, Upward Bound Camp, oral commun., 2006). The 1996 failure released a large fluid component from the lower landslide, as well as extended the head scarp above the washed-out road (Figure 26). By 2005 another lobe of material mobilized from the landslide and flowed into Evans Creek. Previous research (Sobieszczyk and others, 2007) suggested this failure likely occurred in January 2004. By 2009, parts of the Evans Creek Landslide were frequently failing, supplying large pulses of sediment downstream.

Using aerial photographic interpretation, the movement rates were determined for the Evans Creek Landslide (Table 11). Over the last 64 years the landslide moved an average of 5 to 12 feet per year (ft/yr) [2 to 4 meters per year (m/yr)]. The movement rates between photographs varied depending on antecedent ground conditions, as well as variable image rectification error. There were periods of rapid movement with failure

rates approaching 21 and 29 ft/yr [6 and 9 m/yr], including the time periods between 1945 and 1955, between 1970 and 1977, and between 1995 and 2000. In addition, there were periods of nearly imperceptible movement, such as between 1955 and 1970 and between 1977 and 1995. The average Evans Creek Landslide movement rates were similar to the 7 to 23 ft/yr [2 to 7 m/yr] rates observed in other earth flow studies (Swanson and others, 1987; Pearch, 2001; Mackey and Roering, 2010).

The increased landslide movement rates observed every 20 years correspond very well with the Pacific Decadal Oscillation (PDO) weather pattern observed in the Pacific Northwest (Joint Institute for the Study of Atmosphere and Ocean, 2000). Pacific Decadal Oscillation brings similar amounts of rainfall to Oregon as the better known El Niño weather pattern; however, unlike El Niño which starts in the south Pacific along southern California, the PDO originates in the northern Pacific off the Pacific Northwest coast (Joint Institute for the Study of Atmosphere and Ocean, 2000).

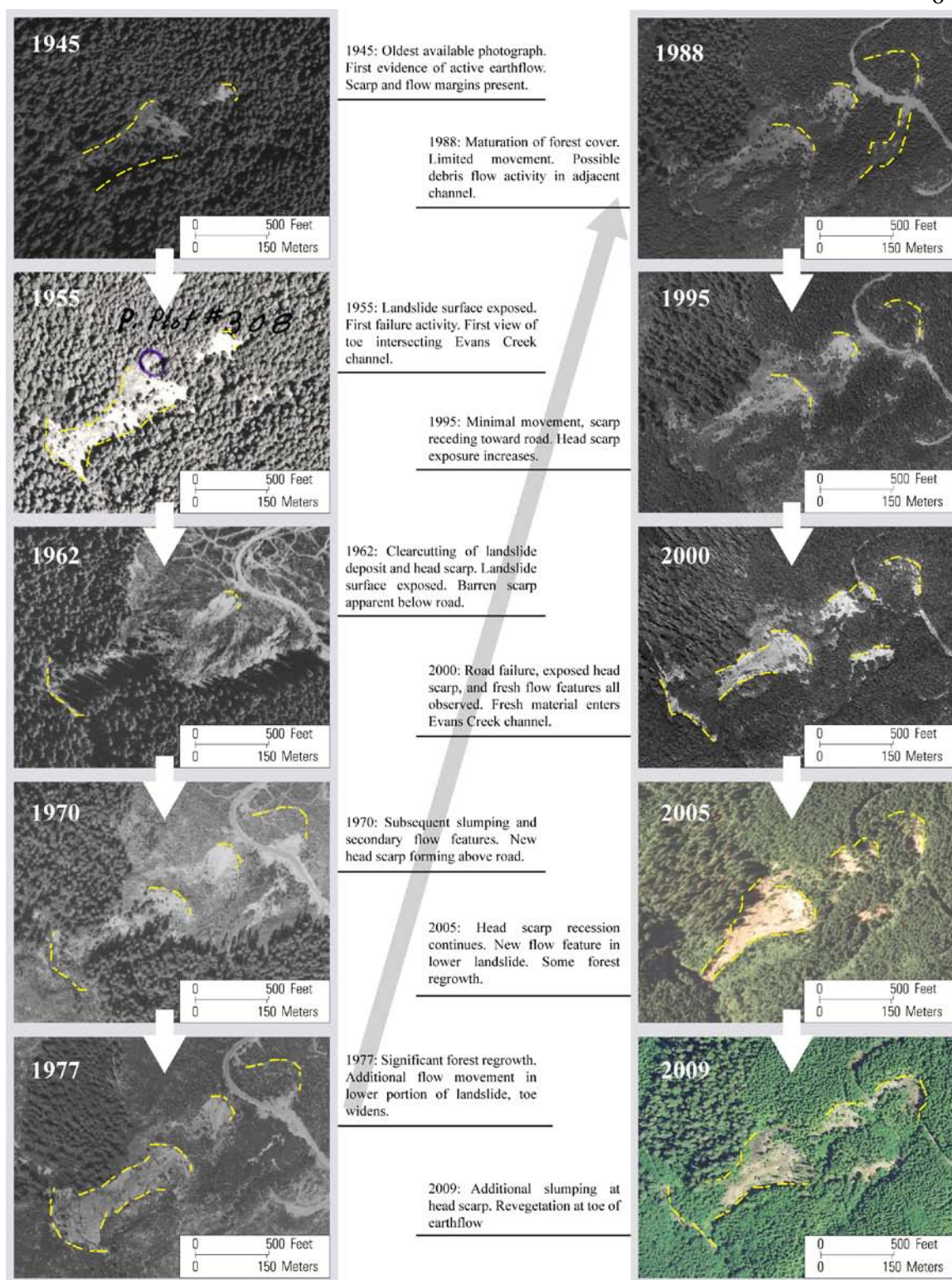


Figure 26. Historical aerial photographs (courtesy of University of Oregon Library, written commun., 2010; Patrick Hawe, Bureau of Land Management, written commun., 2010) and LiDAR imagery for the Evans Creek Landslide. Yellow dashed lines represent landslide features referenced in image description.

Table 11. Evans Creek Landslide movement rates between 1945 and 2009.

[Abbreviations: ft, feet; m, meters; yr, year; na, no data available]

Year	Average Movement Distance (ft) [m]	Rectification Error (+/-) (ft) [m]	Average Movement Rate (ft/yr) [m/yr]
pre-1945	na	100 [30]	na
1945-1955	125 [38]	100 [30]	3-23 [1-7]
1955-1962	23 [7]	50 [15]	0-10 [0-3]
1962-1970	10 [3]	30 [9]	0-5 [0-2]
1970-1977	175 [53]	30 [9]	21-29 [6-9]
1977-1988	18 [5]	30 [9]	0-4 [0-1]
1988-1995	15 [5]	23 [7]	0-5 [0-2]
1995-2000	100 [30]	23 [7]	15-25 [5-7]
2000-2005	22 [7]	18 [5]	1-8 [0-2]
2005-2009	28 [9]	18 [5]	3-12 [1-4]
		Mean	5-12 [2-4]

6.3: Identifying Sediment Sources

Sediment sources investigated in this study focus primarily on the interaction of landslide deposits with streams. However, due to the well-documented interrelation of landslides with other anthropogenic activities, such as timber harvesting, the spatial relation of these other landscape features with the stream network and landslide deposits are also examined.

6.3.1: Interaction of Landslide Deposits and Stream Incision

Based on the LiDAR-derived hydrography data set there are 212 miles [65 km] of perennial streams in the Little North Santiam River Basin. This stream network nearly doubles when the 195 miles [59 km] of gullies and ephemeral streams are added. Since these gullies and streams are seasonal, their erosion potential increases from “negligible”

to “high” once rainfall or snowmelt is introduced and stream conditions rise. The combination of: 1) gully and stream erosion of landslide deposits, and 2) isolated landslide failures into streams make landslides a potentially large and frequent source of sediment in the Little North Santiam River Basin. For example, a study by Chen and others (2006) in China showed that the Chinshui River removed up to 22% of a landslide deposit in just over two years. With 24 mi² [62 km²] of landslide deposits and over 400 miles [122 km] of rivers, streams, and gullies present in the Little North Santiam River Basin, there are significant amounts of sediment and ample modes for transport. However, not all landslides are incised by streams nor do all landslides contribute directly into stream drainages.

There are 53 miles [16 km] of stream that intersect mapped landslide deposits, plus an additional 62 miles [19 km] of gullies atop these deposits. That indicates that 28% of the total drainage network length in the basin has the potential to erode weakly-consolidated landslide deposits. Of the 401 landslide deposits in the basin, over half (51%) are incised by rivers, streams, or gullies (Figure 27). The risk for erosion and sediment removal further increases for the landslide deposits that have been recently clearcut. Five percent of the rivers, streams, or gullies flow across landslide deposits that have been recently timber-harvested, the most highly susceptible sediment producing landscape setting.

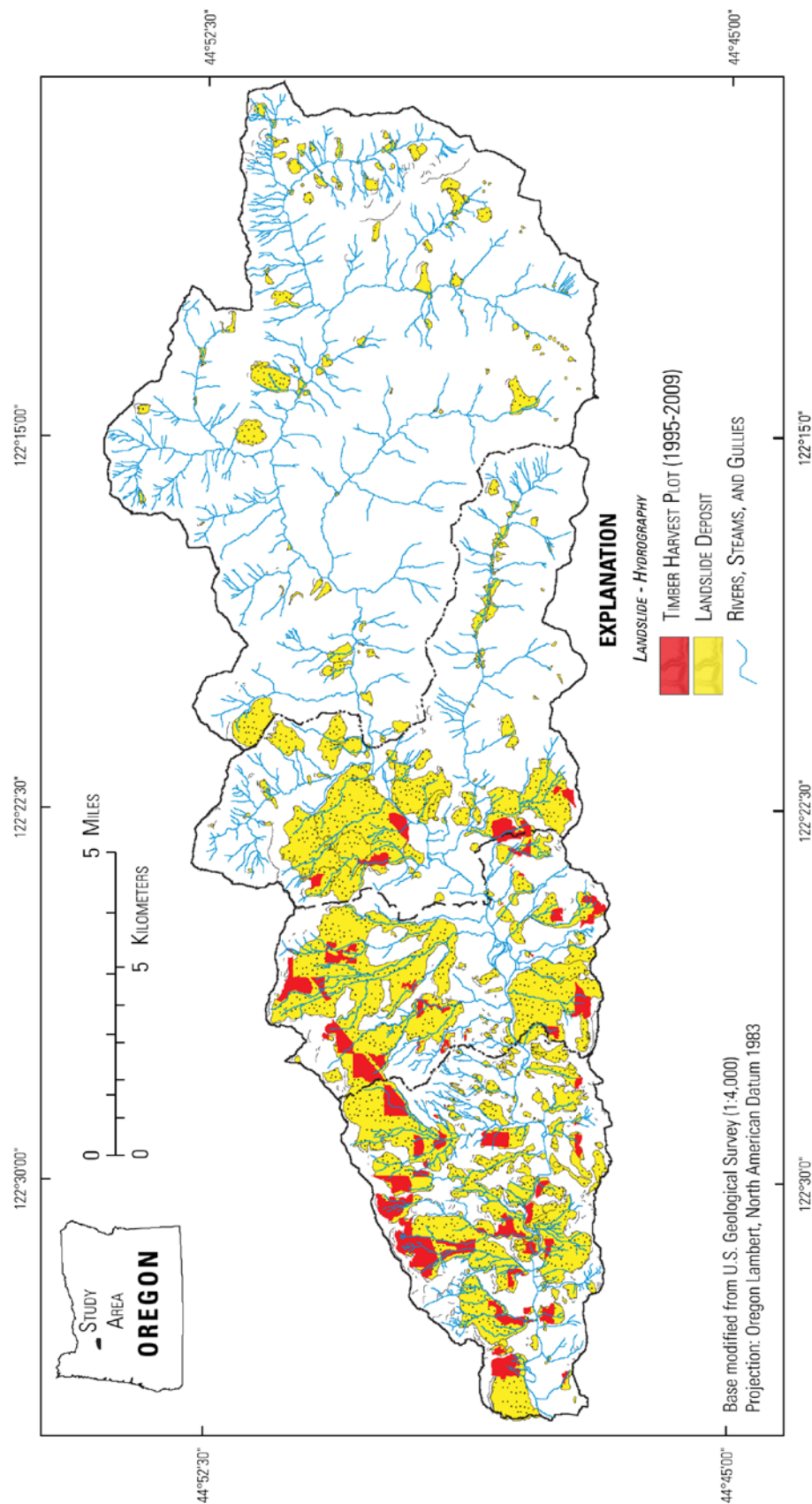


Figure 27. Spatial distribution of landslide deposits in relation to recent timber harvest plots and rivers, streams, and gullies in the Little North Santiam River Basin, Oregon.

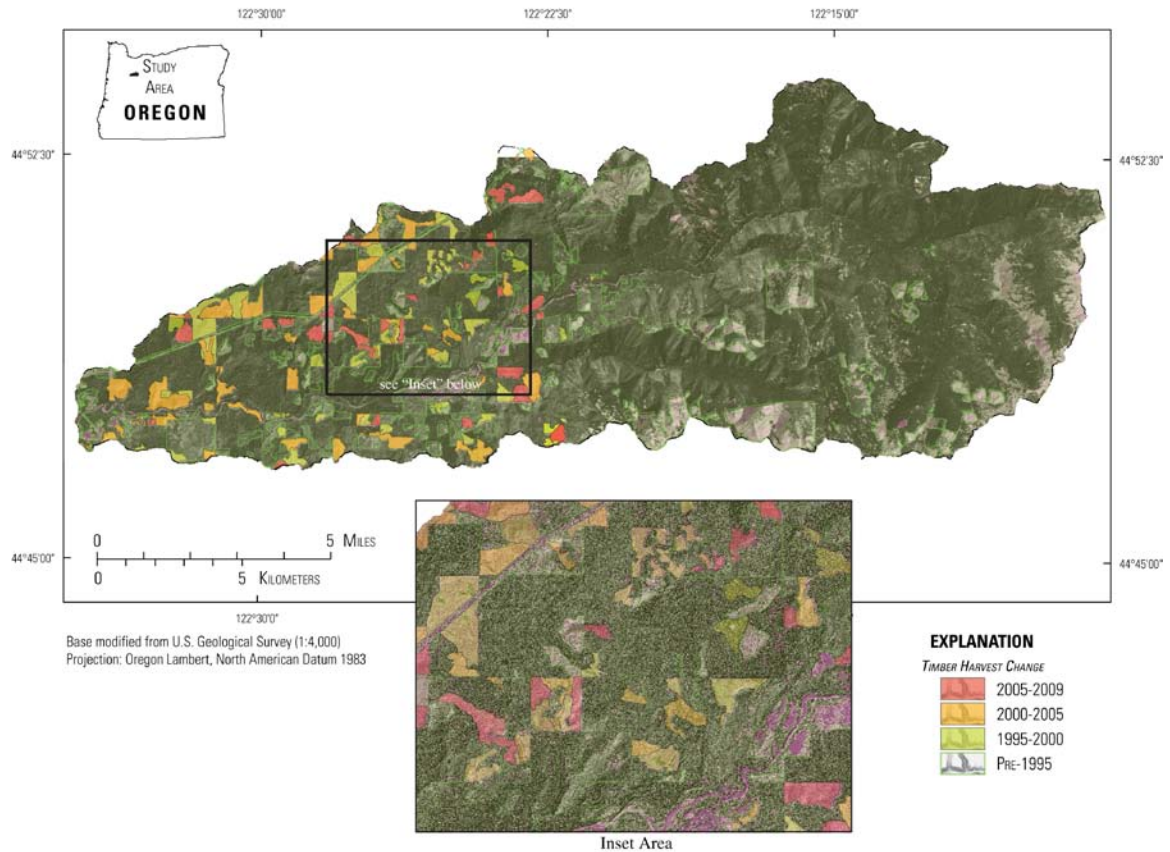


Figure 28. Mapped timber harvest change inventory from 1995 through 2009 for the Little North Santiam River Basin, Oregon.

6.3.3: Spatial Relation between Landslides and Timber Harvest Plots

Due to the large extent of landslide deposits, most timber harvest plots in the lower Little North Santiam River Basin fell entirely within the mapped landslide areas. Conversely, since logging was prohibited in the upper basin, there are no clearcut landslide deposits in Reach D. In the lower basin the lowest percentage of logging area atop landslide deposits was 55% between 2001 and 2005 in Reach C. For every other time period and reach at least 76% to 98% of all timber harvest plots fell on landslides. This indicates that most of the recent logging in the Little North Santiam River Basin

since 1995 has occurred predominately on landslide prone slopes. The correlation between landslides and timber harvest plots is shown in Table 13.

Table 13. Percentage of timber plot boundaries atop landslide deposits, as defined in this study, in the Little North Santiam River Basin, Oregon.

Percent of Timber Harvest Plots on Landslide Deposits				
Years	Reach A (%)	Reach B (%)	Reach C (%)	Reach D (%)
1996-2000	93%	82%	98%	0%
2001-2005	84%	76%	55%	0%
2006-2009	89%	86%	89%	0%

6.4: Instream Turbidity and Suspended-Sediment Load Results

6.4.1: Continuous Turbidity Monitoring

The most efficient way to determine if potential sediment sources contributed material to the Little North Santiam River was by deploying a turbidity monitoring network. Using five continuous instream turbidity monitors, the Little North Santiam River was separated into four separate reaches (Reach A, Reach B, Reach C, and Reach D) and Evans Creek (Figure 1). Turbidity monitors were installed in November 2009 and removed in March 2010. The official period of record for this study was December 1, 2009 through February 28, 2010 (Appendix A.3: Continuous Turbidity, Estimated Streamflow, and Suspended-Sediment Loads).

Turbidity in the Little North Santiam River for the winter 2009–2010 was variable and matched a similar disparity between the upper and lower basins as demonstrated by previously discussed basin characteristics. In the upper basin (Reach D) water passing the

monitor at Station 4 was clear with no turbidity measurements exceeding 10 FNU for any 30-minute reading for the entire 3-month period (Figure 29). Water clarity was significantly less at Station 3 (Reach C) where turbidity routinely reached 20 to 30 FNU, with one spike over 90 FNU (Figure 29). Turbidity levels remained relatively consistent along the remainder of the Little North Santiam River as represented by readings at Stations 1 and 2 downstream (Figure 29).

Two key interpretations can be inferred from observations of the continuous turbidity monitoring. First, most of the sediment that entered the river to increase turbidity entered the river between Stations 3 and 4. Second, although streamflow increased downstream at Stations 1, 2, and 3, turbidity levels remained consistent. This indicates that additional sediment was supplied in conjunction with increased streamflow to keep turbidity values elevated rather than allowing for dilution or settling of sediment. For most of the 3-month study period, the sediment entering the river upstream from Station 3 controlled the turbidity in the river. However, there was a brief period starting January 29, 2010, when something occurred between Station 2 and 3 that raised the baseline turbidity and kept it elevated for nearly 10 days. This increase in turbidity was likely due to material supplied by a reactivation of the Bear Trap Slide near Mile Post 4.

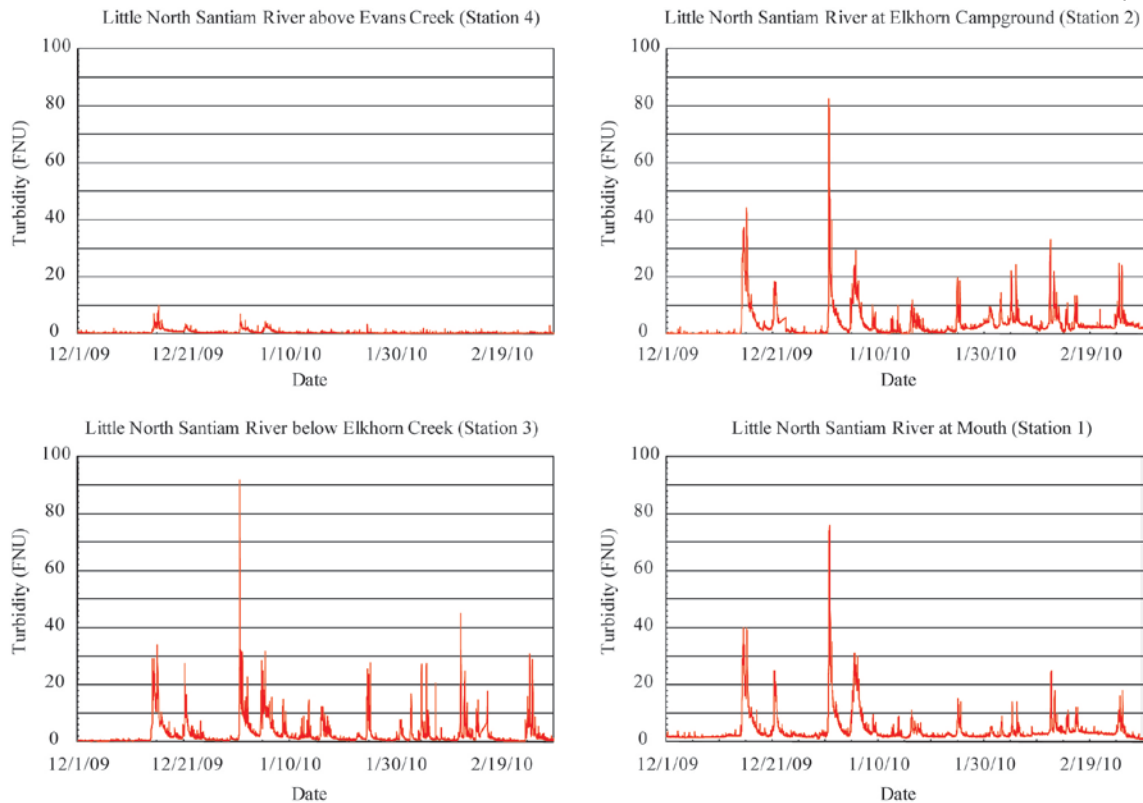


Figure 29. Continuous turbidity readings for December 2009 through February 2010 at four stations along the Little North Santiam River, Oregon.

Unlike the turbidity monitors along the Little North Santiam River, the monitor on Evans Creek routinely recorded above 100 FNU (Figure 30), with readings exceeding the maximum threshold of the equipment (~ 1000 FNU). Turbidity during storm periods was often an order of magnitude greater than what was recorded in the Little North Santiam River at Elkhorn (Station 4), just upstream (inset; Figure 30).

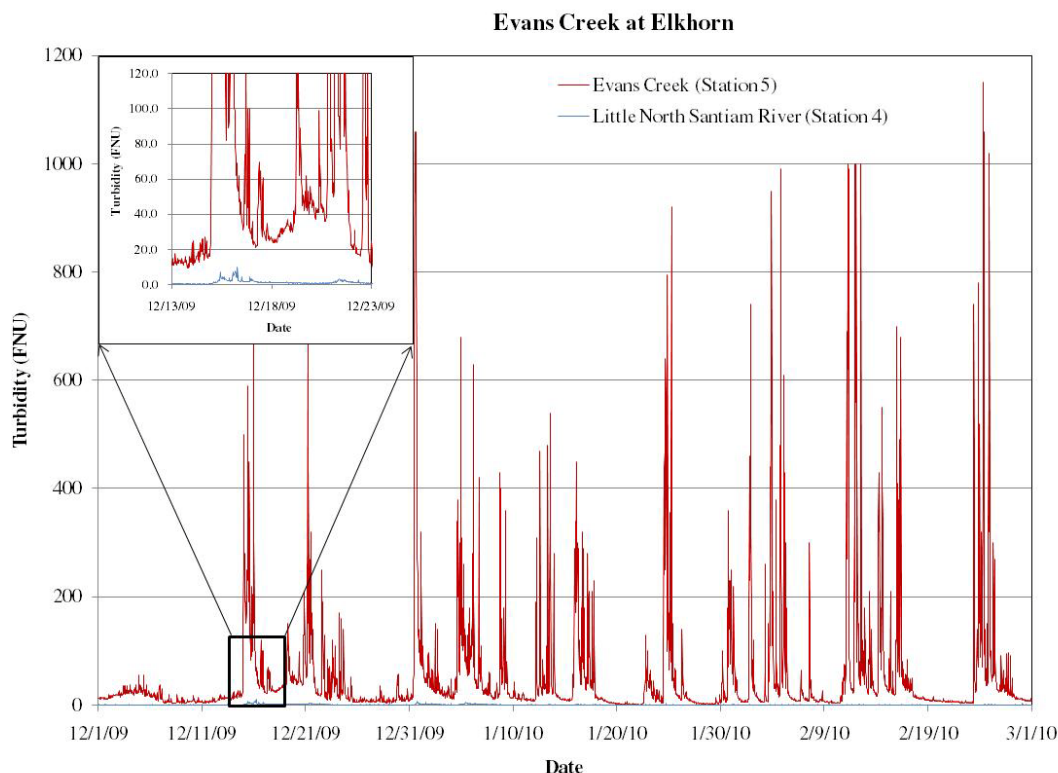


Figure 30. Continuous turbidity readings for December 2009 through February 2010 at Evans Creek at Elkhorn, Oregon (Station 5), and Little North Santiam River above Evans Creek at Elkhorn, Oregon (Station 4).

6.4.2: Suspended-Sediment Loads

6.4.2.a: Long-Term Suspended-Sediment Loads (1999–2008)

Water quality in the Little North Santiam River has been monitored by the USGS since April 2000 with streamflow-gaging and other observations dating back to 1998 (as Site ID 14182500). Therefore, there are about 10 years of water-quality data present for Station 1 at the mouth of the Little North Santiam River. Suspended-sediment load estimates are published for most of the decade, from October 1999 to September 2008 (Bragg and others, 2007; Bragg and Uhrich, 2010), and show an expected seasonal

variability in sediment transport in the river (Table 14). Historically, the periods of greatest rainfall and greatest sediment transport are November through January. Typically, that 3-month period accounts for 84% of the annual sediment transported by the Little North Santiam River. Monthly maxima match a similar timeline, as in most years the greatest monthly totals occur in either December or January. Therefore, although this study focused on the 3-month period from December through February, it still represents 52% of the expected historic annual suspended-sediment load for the basin.

Table 14. Historical suspended-sediment loads, by month, for Station 1 at mouth of Little North Santiam River (Heather Bragg, U.S. Geological Survey, written commun., 2010).

[Shading represents 3-month period corresponding to temporary monitor deployment. Bold values are greatest monthly total for particular year. **Abbreviations:** T, short tons]

MONTH	Suspended-Sediment Load (T)										SUM	%
	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008		
October	50	3	160	260	0	30	60	470	10	780	1,800	1%
November	4,100	46,000	60	2,600	50	640	180	1,100	39,000	1,300	95,000	37%
December	26,000	5,400	420	6,000	670	3,300	4,400	8,700	16,000	4,300	75,000	29%
January	2,200	1,400	40	1,100	6,800	13,000	2,300	12,000	4,900	960	45,000	17%
February	3,000	3,300	40	300	1,200	420	10	630	3,400	230	13,000	5%
March	620	530	410	1,100	4,900	170	2,200	90	540	990	12,000	5%
April	280	260	700	5,900	330	70	280	190	100	460	8,600	3%
May	980	630	490	70	120	210	220	90	30	1,200	4,000	2%
June	130	1,400	20	30	7	60	110	90	15	360	2,200	1%
July	0	0	1	0	0	0	2	10	5	17	40	0%
August	0	0	0	0	4	160	1	2	2	25	190	0%
September	0	0	1	0	1	70	1	1	2	2	80	0%
Annual	37,000	59,000	2,300	17,000	14,000	18,000	9,800	23,000	64,000	11,000	260,000	100%

6.4.2.b: Short-Term Suspended-Sediment Loads (Winter 2009–2010)

Suspended-sediment loads were calculated for the 3-month study period for each station on the Little North Santiam River and Evans Creek (Table 15). Roughly 3,300 T [3,000,000 kg] of sediment left the Little North Santiam Basin during the winter 2009–2010. Based on a proposed range of sediment delivery ratios between 8% and 26%

(Table 15), the instream suspended-sediment load translated to a total gross surface erosion of between 14,000 T [12,700,000 kg] and 41,000 T [37,000,000 kg]. Hence, 10,700 T [9,700,000 kg] to 37,700 T [34,000,000 kg] of sediment that was dislodged from the landscape settled before reaching the confluence with the North Santiam River. Generally, sediment input increased downstream as streamflow increased and more sediment sources were encountered.

Based on the instream monitoring and sediment calculations, little of the sediment measured in the Little North Santiam River was supplied by the upper basin. Reach D yielded only 6 T/mi² [2,100 kg/km²], almost an order of magnitude less than each of the other three reaches (Table 15). Reach C had the highest sediment input of any reach with 1,590 T [1,440 kg], or about 66 T/mi² [23,000 kg/km²]. Most of the sediment that entered the Little North Santiam River in Reach C was attributed to Evans Creek, a tributary that enters a few hundred feet downstream of Station 4. Although the 3-month period of record was short, it did offer enough information to accumulate tangible results; however, the suspended-sediment loads during this period were much lower than what was measured during average flow years (Table 14). Final results were not extrapolated to an annual sediment load because of insufficient data for November 2009 and unseasonable, prolonged rainfall for the months of April, May, June, and July 2010.

Table 15. Suspended sediment and gross erosion loads for December 2009 through February 2010 in the Little North Santiam River Basin, Oregon. Basin values represent entire area upstream, while reach values only quantify values between stations.

[**Abbreviations:** SSL, suspended-sediment load; SSY, suspend-sediment yield; SDR, sediment delivery ratio; mi², square miles; km², square kilometers; T, short tons]

Location			SSL		SSY (S _y)		SDR	Gross Erosion (S _e)
	Basin Drainage	Reach Drainage	3-month		3-month			3-month Basin
			Basin	Reach	Basin	Reach		
	(mi ²) [km ²]		(T)		(T/mi ²) [T/km ²]		(T)	
Reach A (Station 1)	111 [287]	19 [49]	3300	800	30 [11]	42 [16]	0.08 - 0.23	14,000 - 41,000
Reach B (Station 2)	92 [238]	16 [41]	2500	600	27 [11]	38 [15]	0.08 - 0.24	10,000 - 31,000
Reach C (Station 3)	76 [197]	24 [62]	1900	1590	25 [10]	66 [26]	0.08 - 0.24	8,000 - 24,000
Reach D (Station 4)	52 [135]	52 [135]	310	310	6 [2]	6 [2]	0.09 - 0.26	1,100 - 3,900
Evans Creek (Station 5)	3.4 [8.8]	-	910	-	270 [103]	-	0.21 - 0.36	2,500 - 11,000

6.4.2.c: Turbidity and Suspended Sediment Loads at Evans Creek

Based on field observations, turbidity measurements (Figure 30), and suspended-sediment samples, 910 T [830,000 kg] of sediment exited Evans Creek (Table 15). This is a conservative estimate because of the limited sample set and short period of record.

Examining results within the margin of error actually puts the amount of sediment from Evans Creek between 380 and 2200 T [340,000 to 2,000,000 kg]. Therefore, at least a third, if not more, of the total suspended-sediment load for the Little North Santiam River Basin, during winter 2009–2010, came from this one tributary. Most of this sediment in Evans Creek is attributed to material from the Evans Creek Landslide (see “Evans Creek Landslide” in Results section).

Chapter 7. Discussion

7.1: Factors Controlling Landslide Distribution

The most important controlling factor of landslide activity in the Little North Santiam River Basin is the underlying geology. There are two particular bedrock types that appear to dictate landslide failure potential: basalt and tuff. The young, minimally-weathered basaltic bedrock that comprises much of the upper basin supplies a resistant cap that limits erosion and weathering, therefore, restricting the formation of deep-seated landslides. Conversely, the lower basin is underlain by older, highly-weathered tuffaceous bedrock. These volcaniclastic tuffs and breccias are highly susceptible to deep-seated failures. The stark contrast between weathering is evident by the disparate landslide type and distribution when comparing the upper and lower basin, as well as the variability by reach.

The presence of thick soils in the lower basin further increase the likelihood of deep-seated landslides, such as rotational slumps, earth flows, and complex landslides. The lower basin bedrock has not always been as exposed as current conditions indicate. Incision of the younger basalt cap by the Little North Santiam River drainage system has removed the basalt from the valley, while leaving deposits along the high elevation basin margins. Since the basalt cap has persisted in the upper basin, slopes remain much steeper and soil accumulation is much shallower. Therefore, channelized debris flows become the most common landslide type. In most cases the debris flows contain abundant downed timber, rock, and water, but limited dirt and soil. These types of debris flows are referred to as debris torrents (Easterbrook, 1993). Since debris torrents in this basin are

not laden with mud, they do not contribute large suspended-sediment loads to the Little North Santiam River system.

7.2: Problems with Landslide Deposit-Timber Harvest Comparisons

Previous studies (Lyons, 1981; DeRoo and others, 1998) in the Cascade Range have indicated that the landslide frequency in clearcut areas, especially associated with logging roads, was 20x to 25x more frequent than landslide activity in undisturbed forest areas. These estimates are likely artificially inflated because the aerial photographic interpretation methods used did not effectively account for obscured landslides in forested terrain. This gave greater emphasis to landslides “seen” in clearcut areas compared to those “unseen” in forested areas.

With the availability of high-resolution LiDAR, a better correlation between timber harvest and landslide genesis should have been possible in the Little North Santiam River Basin; however, due to the extent of landslide deposits and the establishment of predefined mapping protocols, certain problems arose. For example, large swaths of the lower basin, where all of the logging occurred, are completely covered by complex landslide deposits. These flowing, denuded slopes are much larger than the timber harvest plots, therefore, making it inappropriate to draw a causal link. Conversely, the smaller landslides, such as those associated with logging road failures, are often ignored in the analysis because they are smaller than the established 0.5-acre minimum mapping unit. Since these small landslides are not mapped, no correlation between sediment transport to streams from these features could be quantified.

7.3: Sediment Source Area Distribution

Since the Little North Santiam River Basin covers 111 mi² [287 km²], most discussion about sediment input focuses on a basinwide analysis tied to the four monitoring reaches. As mentioned in the literature review, the likelihood of landslide movement and increased surface erosion relates directly to how land is managed, especially in landslide-prone areas. This complex interaction of sediment-supplying landscape features and erosion-prone land use activities drive much of the sediment transport in the basin.

Even though there are 401 landslides, only one or two active earth flows (Evans Creek Landslide and Bear Trap Slide) are needed to supply a significant percentage of the suspended sediment measured in the Little North Santiam River. For example, during the winter 2009–2010 study period the Evans Creek Landslide contributed nearly 28% of the suspended-sediment load measured at the mouth of the Little North Santiam River (Station 1). Other smaller landslides or surface erosion propagated by gully incision, stream bank erosion, or sediment production from other anthropogenic driving forces, such as clearcutting, likely accounted for the remainder.

The following assessment of sediment sources and estimated instream suspended-sediment loads demonstrate that the Little North Santiam River Basin functions, at least during the winter 2009–2010, as essentially two distinct regions: an upper basin (Reach D) and a lower basin (Reaches A, B, and C). Based on the landslide inventory, stream density, land management activities, and observed instream turbidity, the lower basin is a higher sediment-producing landscape than the upper basin. The area with the greatest sediment input, Reach C, supplies such a disproportionate amount of sediment that it requires more in-depth discussion. Most of the suspended-sediment load in Reach C

came from Evans Creek; therefore, this tributary is parsed out from the lower basin and evaluated on its own.

7.3.1: Upper Basin Sediment Supply

Based on a number of theoretical erosion and sediment transport models, such as USLE (U.S. Department of Agriculture, 1978), GeoWEPP (Renschler, 2008), and SHETRAN (Ewen and others, 2000; Birkinshaw and others, 2010), steep slopes and areas of heavy rainfall should produce more sediment than flatter regions in lower parts of a basin. In contrast, the upper basin of the Little North Santiam River Basin, where there are steeper slopes and more rainfall, less sediment was produced. In fact, Reach D transported the smallest amount of suspended sediment of any reach during the period of study. Although the upper basin accounts for 47% of the total basin area, it contributed only 9% of the total suspended sediment observed in the Little North Santiam River.

Similarly, when examining the available streamflow data the limited sediment production in the upper basin was also less than expected. Based on streamflow estimates 67% of the stream discharge was already incorporated in the Little North Santiam River by Station 4, indicating that most of the power necessary for sediment transport was already present in the river. However, the lack of sediment sources in the upper basin limits the amount of material that is available for transport. The upper basin has few landslide deposits, is mostly covered by federally-protected forests with no logging, has limited road and trail construction or maintenance, and has hillsides composed of resistant bedrock with shallow soils. All these factors contribute to its low potential for sediment production. Most of the landslides mapped in the upper reach are coarse-grain,

timber-rich debris torrents, therefore, contribute minimally to downstream suspended-sediment loads.

7.3.2: Lower Basin Sediment Supply

The lower basin, as defined by Reach A, B, and C, contributed 91% of the suspended-sediment load observed in the Little North Santiam River during the winter 2009–2010. Based on the aforementioned empirical sediment production models (GeoWEPP and USLE), this 10x increase compared to the upper basin is much greater than what would have been expected. Generally, the low-gradient slopes and lower rainfall seen in the lower basin should produce less sediment than the steep-sided slopes and heavy rainfall found in the upper basin. The observed disparity between predicted and actual sediment input can be attributed to the addition of numerous potential sediment sources found in the lower basin. Besides surface erosion along gullies and streambanks, the lower basin also has considerable landslide activity. Many of these landslide deposits have either failed directly into streams or have been eroded by rills and gullies atop the deposits. In addition, erosion from recently logged timber plots and runoff along the dense network of lower basin roadways likely supply additional sediment. Most of the suspended sediment measured in the Little North Santiam River entered in the lower basin, with nearly half of it (48%) incorporated along Reach C. The primary source of sediment in this reach was Evans Creek, which supplied 910 T.

7.3.3: Evans Creek Sediment Supply

Sediment from Evans Creek affects turbidity all the way downstream along the Little North Santiam River. Although there are a few potential sediment sources within the Evans Creek watershed, such as sizable clearcut in the upper western extent (harvested between 2005 and 2009), a number of recent small debris flows, and the extensive Fawn Creek Landslide, most of the sediment observed in the creek actually comes from an earth flow off the western slope of Evans Mountain (Figure 26). This landslide covers 23-acres (0.0004% of the Little North Santiam River Basin) yet supplied nearly a third (28%) of the sediment transported during the winter 2009–2010. During the study, the difference in turbidity between Evans Creek and the Little North Santiam River just upstream at Station 4 was commonly an order of magnitude higher (Figure 30). The fact that one of the smaller landslides in the basin contributes such a sizable portion of the sediment load is interesting. Size does not necessarily matter for the amount of sediment produced from a landslide, instead environmental and hydrologic setting, antecedent conditions, amount of precipitation, movement rates, and other unknown factors control sediment input.

7.4: Limitations of the Study

Research presented in this report does contain some limitations in data collection, processing, and application. Limitations include:

- A short data collection period (December 1, 2009 through February 28, 2010) did not represent the typically highest 3-month historical suspended-sediment load and streamflow period (November through January);
- Due to the below average streamflow and rainfall conditions during the winter 2009–2010, results from this study may not represent sediment sources that dominate during higher flow conditions.
- Significant rainfall and erosion occurred in March through July 2010, after turbidity monitors were removed, so the December through February suspended-sediment loads may not represent the majority of the annual loads in water year 2010 (October 31, 2009 to September 30, 2010);
- The landslide inventory had minimal ground-truthing and the timber harvest change data set was not field checked;
- Sediment delivery ratio calculations were relatively simplistic and had a large margin of error; however, represented the best option given the available information; and
- Rectification accuracy of historical aerial photographs of Evans Creek was highly variable due to limited reference points, especially in the older photographs from 1945, 1955, 1962, and 1970; therefore, there was high variability and potential error in the landslide movement rates.

Chapter 8. Management Implications

Since the scope of this research focuses on identifying sediment sources, primarily landslides, the scope of management recommendations in this section follows suit. Landslides contribute sediment to streams two ways: 1) massive failure into a stream or river; or 2) surface erosion of weakly-consolidated and highly-erodible landslide deposits. Therefore, landslide sediment contribution can be reduced by controlling one or both of these mechanisms.

8.1: Slope Stability Techniques

The failure of a landslide into a stream can supply as much, or more, sediment into a river than surface erosion from the same landslide. Therefore, the first approach for reducing sediment contribution from landslides focuses on slope stabilization. Engineered solutions can be employed in many cases to reduce the driving forces responsible for triggering landslide failure. Techniques, such as dewatering and buttressing, are routinely used and have proven to be effective (Gedney and Weber, 1978; Johnson and DeGraff, 1988; Holtz and Schuster, 1996).

8.1.1: Dewatering Methods

Landslides in the Little North Santiam River Basin typically mobilize in the winter months after heavy rainfall saturates hillslopes. Based on a review of soil survey data for the basin (Natural Resources Conservation Service, 2007), one common failure plane for earth flows (in the lower basin) is a dense silt fragipan layer within the Bx-soil horizon. This dense layer is impermeable and retards downward groundwater movement.

The undrained water eventually builds up pore pressures and causes the slope to fail. One way to restrict this type of failure is by removing or reducing the driving force of water.

Water can be removed by improving the drainage from landslides or landslide-prone areas through the use of both surface drainage, such as diversion ditches and interceptor drains and subsurface drainage, such as horizontal or vertical drains.

Horizontal drains have been successfully used along the North Fork Road to mitigate landslide movement near Mile Post 4. Engineered drainage effectively transports water away from a landslide. Drainage systems improve slope stability and often remain effective for upwards of 20 years (Johnson and DeGraff, 1988). Of course, dewatering the landslide-prone slope is not the only solution for slope stabilization. Another common, yet more expensive technique, involves buttressing or reinforcing the base of the landslide.

8.1.2: Buttressing and Internal Stabilization Solutions

Along with dewatering, slope stabilization can be achieved by having: 1) a resisting force applied to the toe of the landslide, such as with a buttress; or 2) the internal strength of the slope improved, such as through the use of geotextiles or natural plantings (Holtz and Schuster, 1996). Buttressing the toe of a landslide with gabion baskets, riprap, gravity walls, or other engineered anchor systems improve stability by restricting movement of a slope. However, these structures are often expensive and only effective over a limited area. They are used primarily along roads in highly-travelled areas and may not be cost-effective for remote areas or along lengthy stretches of roadway.

If buttressing cannot be used, another approach focuses on increasing the internal strength of the landslide. This stabilization technique is achieved through the use of geotextile and geomembrane products, by natural plantings, or by other integrated design elements (Rogers, 1992; Natural Resources Conservation Service, 1992). Table 16 lists examples of soil bioengineering and vegetative planting techniques that have been used elsewhere (Natural Resources Conservation Service, 1992). Vegetation stabilizes slopes by binding the soils, filtering sediments, and reducing both overland or groundwater flow through interception and evaporation. Also, unlike previous solutions, vegetated structures assimilate into the environment and provide a much more aesthetic backdrop.

Table 16. Approaches for slope protection and stabilization (modified from Natural Resources Conservation Service, 1992).

Category	Type	Examples	Appropriate Uses	Vegetation Effectiveness
Living	Vegetative Plantings			
	Conventional plantings	Grass seedings Transplants Forbs	Control water and wind erosion Minimize frost effects	Control weeds Bind and restrain soil Filter soil from runoff Intercept rainfall Maintain infiltration Moderate ground temperature
	Soil Bioengineering			
Nonliving	Woody plants used as reinforcement, as barriers to soil movement, and in the frontal openings or interstices of retaining structures	Live staking Live fascine Brush layer Branch packing Live cribwall Live gully repair Vegetated rock gabion Vegetated rock wall Joint planting	Control of rills and gullies Control of shallow translational landslides Filter sediment Improve resistance to low or moderate slope movement	Control weeds Bind and restrain soil Filter soil from runoff Intercept rainfall Reinforce soil Transpire excess water Minimize slope movement Reinforce fill Improve appearance and structural performance
	Vegetated Structures			
	Inert structures with vegetative treatments	Wall or revetment with slope face planting tiered structures with bench planting	Control erosion on cut and fill slopes Limit scour and undermining	Stop or limit erosion Stop or prevent shallow slope failure

8.2: Erosion Control Techniques

Surface erosion can be controlled with basic soil conservation methods, including limiting timber harvesting and establishing check dams (Table 17). Similar to landslide stabilization techniques, methods for reducing erosion are extensive and include both natural and engineered solutions and range from prevention to repair (Table 17). In order to reduce sediment transport, the most important area to focus remediation is along rivers, streams, and gullies. River restoration and riparian buffers are vital for filtering runoff, trapping sediment, and stabilizing slopes, especially in the recently timber-harvested areas (U.S. General Accounting Office, 1998; Washington State Department of Natural Resources, 2009). For exposed areas, the use of drainage structures, such as relief culverts, water bars, rolling dips, and ditch-outs aid in controlling soil erosion (Washington State Department of Natural Resources, 2009).

Table 17. Guidelines for successful watershed management (modified from Gregersen and others, 2007).

Basic soil conservation methods					
Situation					
Surface Erosion		Steep Slopes	Gully Erosion	Landslides	
Method	Prevention	Limit timber harvest		Avoid road cuts (especially at toe)	
		Limit road construction	Avoid timber harvesting	Maintain buffer (riparian)	
		Limit land use change (conversion to agriculture)	Avoid or limit activity in landslide prone areas.		
	Maintenance	Lay roads and trails so that runoff is not channelized on steep, susceptible areas	If developing, construct terraces with reverse slope benches to promote infiltration	Lay straw or cover fill	Maintain trees and deep rooted plants on steep hillslopes
		Repair	Develop overland flow control structures	Construct furrows and trenches perpendicular to slope to intercept runoff and promote infiltration	Channel reforestation
	Maintain or develop vegetated buffers around water bodies			Establish check dams (gabions, woody debris, etc.)	Establish bioengineered structures to stabilize soil slips

8.3: Specific Management Solutions for Evans Creek Landslide

Reducing the sediment supply from the Evans Creek Landslide has been a priority for land managers with the BLM. Recent mitigation efforts implemented during the summer of 2009 included spraying straw on exposed surfaces and placing 40 large trees with root wads at the base of the earth flow (Patrick Hawe, Bureau of Land Management, written commun., 2009). These two basic techniques were employed to potentially address both surface erosion and landslide movement issues. However, turbidity readings from the winter 2009–2010 indicate sediment is still being supplied to Evans Creek. More time is needed to fully assess if the implemented procedures prove successful. Additional control devices, such as sediment fences and temporary detention basins could be deployed, and may prove more useful at retaining more sediment.

Since the Evans Creek Landslide supplies a disproportionate amount of suspended sediment to the Little North Santiam River, any remediation efforts developed from results of this study should focus foremost on this particular earth flow. If turbidity and suspended sediment is important to land managers and inhabitants in the Little North Santiam River Basin, then the landslide should be evaluated by a professional engineering geologist and assessed for a more long-term geoengineered solution. Until a professional assessment is completed, no timber should be harvested from the landslide area or adjacent slopes.

Chapter 9. Summary

The Cascade Range of western Oregon represents a unique environment to study erosion and sedimentation. Unlike other regions where surface erosion along streambanks and gullies supply much of the sediment found in rivers and streams, factors in the Cascade Range, such as landslide activity, are just as influential. This study was designed to investigate, at a basinwide scale, how landscape features (landslides) and land management practices (logging) potentially work together to contribute sediment to the Little North Santiam River. Using LiDAR-derived imagery, aerial photographic interpretation, and continuous instream turbidity monitoring a number of landscape parameters were mapped and investigated to determine their respective influence on sediment input to the Little North Santiam River. The Little North Santiam River Basin was chosen to take advantage of the abundant historical turbidity and streamflow data that was available, as well as address specific concerns related to sediment input from known landslides in the basin.

The Little North Santiam River is a tributary of the North Santiam River and drains 111 mi² [287 km²] of north-central Marion County. Since the North Santiam River is the source of drinking water for the City of Salem and the surrounding communities, any changes to the water quality in the Little North Santiam River will have widespread effects downstream. One common water-quality concern is high turbidity, or “dirty water.” Previous studies indicate that 60% to 90% of the suspended sediment responsible for increased turbidity in some Western Cascade streams comes from landslide source areas. Sediment production from other sources, such as clearcutting and road building, also contribute to suspended-sediment loads, but are harder to evaluate, therefore are only briefly discussed in this study.

The 401 mapped landslides cover 24 mi² [62 km²], or about 22% of the Little North Santiam River Basin extent. The LiDAR-based landslide inventory is an improvement over previous geologic mapping efforts based on aerial photographs, showing 40x more landslides and twice the depositional area. The size and distribution of landslide deposits is heterogeneous, with 37% of the lower half of the basin covered by deposits compared to only 4% of the upper half. The classification also varies by upper and lower basin extents, with most of the larger earth flow and complex landslide deposits seen in the lower basin and the debris flows and rock falls in the upper basin. There are 190 earth flows, 164 debris flows, 21 complex landslides, 13 rock fall deposits, nine rotational earth slumps, and four translational earth slides. Ninety percent of the landslide depositional extent was either earth flow deposits or earth flow-dominant complex landslide deposits.

For this study, the Little North Santiam River Basin was divided into four reach segments (Reach A, B, C, and D), with turbidity monitors installed at roughly equidistant locations along the river. An additional turbidity monitor was installed at Evans Creek, a tributary historically more turbid than the mainstem Little North Santiam River. According to the suspended-sediment load estimates, 3,300 T [3,000,000 kg] of material was transported from the basin during the 3-month study period between December 1, 2009 and February 28, 2010. Most of the suspended load, 2,990 T [2,700,000 kg], entered the river in the lower three reaches, or lower basin. This was in stark contrast to the 310 T [280,000 kg], or 9%, supplied by the upper basin (Reach D), even though the upper basin comprised 47% percent of the total basin area.

The extent of landslide deposits shows a similar distribution as the suspended-sediment loads. Reach D has the smallest extent of landslide deposits (4% of the reach),

followed by 25% of Reach C, 46% of Reach B, and 45% of Reach A. Although, 28% of the stream drainage network crosses landslide deposits, nearly a third (28%) of the total suspended-sediment load measured in winter 2009–2010 came from a single landslide in the upper extent of Reach C, the Evans Creek Landslide. The remaining suspended-sediment load likely came from other smaller landslides or other landscape features such as gully and bank erosion, stream–road crossings or recent timber harvest plots.

The Evans Creek Landslide is a 23-acre [0.9 km²] active earth flow that intersects Evans Creek. Based on historic aerial photographs, the landslide has shown periods of activity as far back as 1945. The first evidence of the earth flow entering Evans Creek can be seen in the 1955 aerial photograph. As with most earth flows, movement rates vary over time depending on rainfall intensity and antecedent conditions. Generally, the average earth flow movement is between 5 and 12 ft/yr [2 to 4 m/yr], although, it has been shown to move as quickly as of 29 ft/yr [9 m/yr]. Most landslide movement surges during isolated periods such as in 1996 and 2004. Nearly 910 T [830,000 kg] of suspended sediment, with a margin of error of between 380 and 2200 T [340,000 to 2,000,000 kg], came from Evans Creek during the 3-month study period.

Lastly, since land management plays a vital role in how sediment mobilizes into the Little North Santiam River, slope stabilization and erosion control measures are necessary to retain a safe drinking-water supply. Whether mitigating landslide movement, decreasing surface runoff, or buffering streams with vegetated riparian zones, land managers must continue to remain aware of how poor management practices not only affect local safety (landslide or road failure), but also potentially the health and safety of 100,000s of people downstream (drinking water).

Chapter 10. Future Studies

The most pressing work that should be continued is subsequent monitoring of Evans Creek. Since a sizable suspended-sediment load comes from this stream, addressing turbidity concerns from this creek would account for much of the sediment that enters the Little North Santiam River system. Likewise, additional geotechnical work examining the Evans Creek Landslide might lead to a cost-effective solution for stabilizing the earth flow, thereby reducing future erosion and sediment transport concerns.

Another area of research that was briefly examined, but not fully addressed, was a discussion of a thorough debris flow hazard map. Many of the upper basin drainages and some of the lower basin channels show remnants of previous debris flow activity. During intense storms and flooding, such as in February 1996, debris flow activity increases significantly. Since debris flows are a risk to people and infrastructure, and to a lesser degree water quality, additional research on the location and likelihood of debris flows should be completed.

As with most research, time and money constraints dictated how much time was spent on each of the tasks completed in this study. This “crunch” left a lot of data unexamined and some quality assurance and field verification underdeveloped. With more time, there could be further utilization of the high-resolution LiDAR data set to assess other landscape features, including a much better geologic map of the region. Similarly, with more time additional field verification of mapped landslide deposits and timber harvest plots could be completed.

Lastly, streamflow conditions for the winter of 2009–2010 were well below normal. It wasn’t until after the monitoring network was removed that subsequent rainfall

increased system-wide streamflow conditions. Therefore, the research presented here only represents a brief analysis of potential trends in both sediment rates and input distribution. Similarly, although there was 10 years of water-quality data available at the mouth of the Little North Santiam River, these data only paint a broad picture of what actually controls sediment delivery in the basin. A three to ten year “extension” study of the contribution of the four reaches would provide a more complete sediment input and response within the Little North Santiam River Basin.

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Appendices

A – Tables and Graphs

A.1 – Suspended-Sediment Samples at Station 1 near Mouth of Little North Santiam River

[**Abbreviations:** FNU, Formazin Nephelometric Units; ft³/s, cubic feet per second; m³/s, cubic meters per second; SSC, suspended-sediment concentrations; mg/L, milligrams per liter; na, no data available]

Date & Time	Sample Type	Turbidity (FNU)	Streamflow (ft ³ /s) [m ³ /s]	SSC (mg/L)	% Fines
1/27/99 14:45	Equal Width Integrated	683	2.7 [0.1]	3	52
2/2/99 12:15	Equal Width Integrated	772	5.1 [0.1]	4	51
2/17/99 13:15	Equal Width Integrated	1170	3.7 [0.1]	4	62
2/23/99 14:00	Equal Width Integrated	3540	47 [1.3]	124	33
3/2/99 10:40	Equal Width Integrated	1640	2.8 [0.1]	8	54
3/10/99 10:30	Equal Width Integrated	549	1.6 [0.1]	3	61
3/17/99 12:00	Equal Width Integrated	677	1.2 [0]	3	38
3/22/99 13:00	Equal Width Integrated	863	1.4 [0]	7	78
3/31/99 14:00	Equal Width Integrated	677	2.2 [0.1]	1	70
4/13/99 14:36	Equal Width Integrated	694	4.8 [0.1]	4	35
4/21/99 14:30	Equal Width Integrated	909	1.2 [0]	2	64
5/18/99 13:52	Equal Width Integrated	1810	5 [0.1]	8	45
7/1/99 10:16	Equal Width Integrated	384	0.7 [0]	3	53
11/5/99 14:15	Equal Width Integrated	216	0.7 [0]	1	58
12/1/99 10:42	Equal Width Integrated	867	11 [0.3]	5	85
12/7/99 11:27	Dip	2170	22 [0.6]	22	74
12/14/99 14:31	Equal Width Integrated	1650	7.6 [0.2]	8	75
12/14/99 14:50	Dip	1660	7.6 [0.2]	7	80
12/17/99 10:38	Equal Width Integrated	3760	44 [1.3]	49	68
12/20/99 14:58	Dip	1560	7.4 [0.2]	8	72
1/6/00 10:57	Equal Width Integrated	1240	3.2 [0.1]	4	80
1/22/00 10:25	Equal Width Integrated	927	2.6 [0.1]	7	36
2/2/00 11:00	Equal Width Integrated	3810	47 [1.3]	65	60
2/15/00 11:10	Dip	1990	5.5 [0.2]	7	63
2/22/00 10:10	Equal Width Integrated	750	2 [0.1]	5	36
2/22/00 15:55	Dip	835	2.2 [0.1]	2	64
3/3/00 10:25	Equal Width Integrated	895	1.8 [0.1]	1	94
3/16/00 12:16	Equal Width Integrated	1190	4.5 [0.1]	3	82
4/5/00 12:45	Equal Width Integrated	895	1.1 [0]	1	67
5/3/00 14:30	Equal Width Integrated	724	1.5 [0]	5	48
6/12/00 12:40	Equal Width Integrated	6660	170 [4.8]	249	56
6/12/00 15:30	Dip	5880	130 [3.7]	118	71
6/13/00 9:35	Dip	2360	14 [0.4]	21	49
6/14/00 18:25	Equal Width Integrated	1130	3.2 [0.1]	3	79

Date & Time	Sample Type	Turbidity	Streamflow	SSC	%
		(FNU)	(ft ³ /s) [m ³ /s]	(mg/L)	Fines
6/22/00 16:40	Equal Width Integrated	280	0.6 [0]	2	61
10/20/00 20:00	Dip	1040	14 [0.4]	17	92
10/20/00 23:00	Dip	1690	12 [0.3]	26	78
11/8/00 12:30	Equal Width Integrated	544	2 [0.1]	4	83
11/9/00 17:45	Dip	718	2.2 [0.1]	2	64
11/27/00 11:30	Dip	1270	5.5 [0.2]	14	74
11/29/00 15:50	Equal Width Integrated	685	1.4 [0]	4	97
12/14/00 11:45	Equal Width Integrated	674	3.7 [0.1]	8	59
12/15/00 9:05	Equal Width Integrated	2350	15 [0.4]	24	73
12/23/00 10:00	Equal Width Integrated	2090	4.6 [0.1]	9	67
12/27/00 14:15	Equal Width Integrated	870	1 [0]	2	53
1/9/01 15:32	Equal Width Integrated	363	0.9 [0]	1	77
1/23/01 15:22	Equal Width Integrated	720	0.5 [0]	1	63
2/5/01 12:15	Dip	1500	3 [0.1]	11	38
3/15/01 10:32	Equal Width Integrated	320	0.5 [0]	3	47
3/15/01 19:30	Equal Width Integrated	375	1.7 [0.1]	10	36
3/18/01 12:40	Equal Width Integrated	909	6.1 [0.2]	8	82
3/19/01 9:40	Equal Width Integrated	2780	24 [0.7]	47	59
3/19/01 16:33	Equal Width Integrated	2260	9.7 [0.3]	18	54
3/19/01 17:14	Dip	2230	9.4 [0.3]	15	52
3/28/01 9:32	Dip	1900	5.3 [0.2]	8	54
3/28/01 9:58	Equal Width Integrated	1830	5.2 [0.2]	8	65
3/28/01 16:05	Dip	1680	3.8 [0.1]	5	73
4/17/01 16:12	Equal Width Integrated	906	0.8 [0]	3	67
4/30/01 12:53	Equal Width Integrated	2010	16 [0.5]	28	67
4/30/01 13:24	Dip	2320	26 [0.7]	42	68
4/30/01 13:59	Equal Width Integrated	2850	41 [1.2]	72	56
4/30/01 17:18	Equal Width Integrated	4520	110 [3.1]	158	52
5/1/01 11:43	Equal Width Integrated	1920	8.2 [0.2]	10	68
5/1/01 19:23	Dip	1610	3.7 [0.1]	7	61
5/15/01 8:55	Equal Width Integrated	3030	18 [0.5]	34	49
5/16/01 8:06	Equal Width Integrated	2660	9.1 [0.3]	12	51
5/16/01 8:14	Dip	2660	8.6 [0.2]	13	49
10/11/01 11:29	Equal Width Integrated	207	6.8 [0.2]	9	94
10/23/01 12:06	Equal Width Integrated	1240	3.5 [0.1]	2	43
10/31/01 19:24	Equal Width Integrated	2440	8.5 [0.2]	14	62
11/14/01 11:55	Equal Width Integrated	2270	12 [0.3]	18	55
11/14/01 12:50	Dip	2140	11 [0.3]	15	52
11/22/01 18:45	Dip	5860	85 [2.4]	227	43
11/23/01 9:31	Equal Width Integrated	3240	16 [0.5]	23	62
11/23/01 9:46	Dip	3210	16 [0.5]	29	54
11/29/01 11:56	Equal Width Integrated	3780	22 [0.6]	25	63
11/29/01 12:19	Dip	3730	18 [0.5]	30	51
12/6/01 12:15	Equal Width Integrated	3100	18 [0.5]	29	52
12/13/01 13:58	Equal Width Integrated	4270	37 [1.1]	58	56
12/14/01 11:55	Equal Width Integrated	4560	37 [1.1]	59	44

Date & Time	Sample Type	Turbidity (FNU)	Streamflow (ft ³ /s) [m ³ /s]	SSC (mg/L)	% Fines
12/14/01 12:44	Dip	4430	34 [1]	75	46
12/16/01 13:45	Dip	5940	49 [1.4]	135	38
12/16/01 13:52	Equal Width Integrated	5980	49 [1.4]	107	48
1/8/02 12:15	Equal Width Integrated	3560	16 [0.5]	29	41
1/8/02 12:55	Equal Width Integrated	3540	16 [0.5]	31	43
1/25/02 10:58	Equal Width Integrated	2470	17 [0.5]	33	56
1/25/02 14:33	Equal Width Integrated	2820	18 [0.5]	42	44
2/19/02 11:16	Equal Width Integrated	782	2.4 [0.1]	2	71
3/12/02 14:10	Equal Width Integrated	2970	10 [0.3]	20	51
3/12/02 15:05	Dip	2940	9.9 [0.3]	18	49
4/14/02 11:30	Dip	5920	110 [3.1]	193	53
12/12/02 14:32	Equal Width Integrated	830	1.9 [0.1]	1	84
12/13/02 11:16	Dip	1140	2.8 [0.1]	4	69
12/16/02 10:33	Equal Width Integrated	2130	19 [0.5]	21	73
12/16/02 12:00	Dip	1960	16 [0.5]	22	68
12/27/02 11:51	Equal Width Integrated	1760	11 [0.3]	17	77
12/31/02 7:00	Dip	2680	20 [0.6]	39	57
1/3/03 12:07	Equal Width Integrated	2330	10 [0.3]	16	69
1/30/03 15:05	Equal Width Integrated	7670	90 [2.6]	180	40
1/30/03 16:05	Dip	8400	100 [2.8]	160	48
1/31/03 12:50	Equal Width Integrated	7050	63 [1.8]	166	45
1/31/03 17:22	Dip	8120	75 [2.1]	274	38
2/1/03 11:55	Equal Width Integrated	3910	23 [0.7]	41	53
3/7/03 11:16	Equal Width Integrated	4360	42 [1.2]	94	48
3/7/03 11:42	Dip	4290	41 [1.2]	86	49
3/8/03 13:40	Equal Width Integrated	5200	33 [0.9]	64	58
3/21/03 17:00	Dip	1940	24 [0.7]	44	50
3/22/03 12:30	Equal Width Integrated	5940	44 [1.3]	121	38
3/22/03 13:17	Dip	6180	46 [1.3]	142	36
4/15/03 14:20	Equal Width Integrated	1030	1.1 [0]	1	88
5/15/03 11:10	Equal Width Integrated	588	0.8 [0]	2	
12/12/03 13:40	Equal Width Integrated	1800	9 [0.3]	13	72
12/13/03 14:52	Equal Width Integrated	11000	180 [5.1]	520	50
12/13/03 15:28	Dip	11400	190 [5.4]	629	38
12/14/03 11:27	Equal Width Integrated	2820	21 [0.6]	43	48
1/29/04 11:12	Equal Width Integrated	12100	210 [6]	451	61
1/29/04 11:50	Dip	11500	200 [5.7]	523	43
1/29/04 14:53	Dip	10400	170 [4.8]	525	37
1/30/04 11:40	Equal Width Integrated	4440	68 [1.9]	118	62
12/8/04 14:45	Equal Width Integrated	3260	37 [1.1]	78	52
12/8/04 15:33	Equal Width Integrated	3100	38 [1.1]	74	55
1/18/05 14:18	Equal Width Integrated	5090	52 [1.5]	129	47
3/28/05 14:35	Equal Width Integrated	2750	13 [0.4]	19	59
11/1/05 14:31	Equal Width Integrated	2360	14 [0.4]	18	
1/11/06 17:28	Dip	4160	36 [1]	65	55
1/17/06 14:45	Equal Width Integrated	4410	33 [0.9]	72	44

Date & Time	Sample Type	Turbidity (FNU)	Streamflow (ft³/s) [m³/s]	SSC (mg/L)	% Fines
11/7/06 13:16	Equal Width Integrated	19200	410 [11.6]	755	70
11/8/06 11:33	Equal Width Integrated	3090	88 [2.5]	122	73
12/13/06 13:04	Equal Width Integrated	6090	150 [4.3]	258	64
10/10/07 12:31	Equal Width Integrated	163	0.5 [0]	2	59.1
12/4/07 13:35	Equal Width Integrated	4570	27 [0.8]	41	60.8

A.2 – Landslide Inventory

[Highlighted landslide is the Evans Creek Landslide. * were field checked. **Abbreviations:** °, degrees; ft, feet; yd³, cubic yard; na, not available]

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Slope		Head Scarp Height		Fan Height	Fail Depth	Depth Classification	Flow Direction	Area	Volume
					(°)	(ft)	(ft)	(ft)						
Bagby Hot Springs_01	Translational	High	Pre-Historic	Tba	28	76	0	67			Deep	247.5	16	1737593
Bagby Hot Springs_02	Debris Flow	High	Pre-Historic	Tlm	24	0	35	0			na	180.0	2	42549
Bagby Hot Springs_03	Debris Flow	High	Pre-Historic	Tlm	23	0	35	0			na	0.0	2	31001
Bagby Hot Springs_04	Debris Flow	Moderate	Pre-Historic	Tum	25	0	20	0			na	225.0	11	120229
Battle Ax_01	Debris Flow	High	Pre-Historic	Tum	26	0	40	0			na	270.0	2	47086
Battle Ax_02	Earth Flow	High	Historic	Tum	40	60	0	46			Deep	270.0	16	1206304
Battle Ax_03	Complex	Low	Pre-Historic	Tsa1	28	40	0	35			Deep	225.0	21	1169337
Battle Ax_04	Debris Flow	Moderate	Pre-Historic	Qgf	20	0	30	0			na	112.5	3	54554
Battle Ax_05	Earth Flow	High	Pre-Historic	Qyt	38	40	0	32			Deep	202.5	4	223206
Battle Ax_06	Earth Flow	High	Historic	Tr	25	60	0	54			Deep	337.5	11	1002078
Battle Ax_07	Rotational	High	Pre-Historic	Tr	27	60	0	53			Deep	0.0	10	897341
Battle Ax_08	Translational	High	Pre-Historic	Tr	22	15	0	14			Shallow	247.5	24	538504
Battle Ax_09	Earth Flow	Low	Pre-Historic	Tr	22	40	0	37			Deep	247.5	14	809800
Battle Ax_10	Earth Flow	Low	Pre-Historic	Tr	21	22	0	21			Deep	225.0	6	212614
Battle Ax_11	Earth Flow	High	Pre-Historic	Tiha	30	16	0	14			Shallow	270.0	17	373667
Battle Ax_12	Earth Flow	Low	Pre-Historic	Tiha	30	30	0	26			Deep	270.0	5	228857
Battle Ax_13	Earth Flow	High	Pre-Historic	Tu	28	40	0	35			Deep	67.5	6	364208
Battle Ax_14	Rock Fall	Moderate	Pre-Historic	Tum	35	0	40	0			na	135.0	8	176148
Battle Ax_15	Debris Flow	Moderate	Pre-Historic	Tum	34	0	40	0			na	202.5	3	69516
Battle Ax_16	Earth Flow	High	Pre-Historic	Tu	22	60	0	56			Deep	45.0	14	1216959
Battle Ax_17	Earth Flow	High	Historic	Tiha	30	35	0	30			Deep	67.5	21	1013933
Battle Ax_18	Earth Flow	High	Historic	Tu	20	15	0	14			Shallow	90.0	3	61263
Battle Ax_19	Earth Flow	High	Pre-Historic	Tu	30	60	0	52			Deep	45.0	15	1288985

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Depth Classification	Flow Direction	Area (acres)	Volume (yd ³)
					Slope (°)	Height (ft)	Fan Height (ft)				
Battle Ax_20	Earth Flow	High	Historic	Qgf	15	40	0	39	45.0	2	148347
Battle Ax_21	Earth Flow	High	Pre-Historic	Tu	28	17	0	15	67.5	5	116217
Battle Ax_22	Earth Flow	High	Pre-Historic	Tu	32	15	0	13	112.5	5	104016
Battle Ax_23	Earth Flow	High	Pre-Historic	Tu	25	75	0	68	67.5	25	2772948
Battle Ax_24	Earth Flow	High	Pre-Historic	Tba	28	30	0	26	270.0	17	747504
Battle Ax_25	Debris Flow	Moderate	Pre-Historic	Tu	30	0	35	0	90.0	9	164201
Battle Ax_26	Earth Flow	High	Historic	Tu	20	80	0	75	270.0	47	5665000
Battle Ax_27	Earth Flow	Moderate	Pre-Historic	Tu	25	30	0	27	67.5	10	449056
Battle Ax_28	Debris Flow	Moderate	Pre-Historic	Qgf	15	0	35	0	90.0	1	14700
Battle Ax_29	Debris Flow	Moderate	Pre-Historic	Qgf	26	0	35	0	270.0	20	368384
Battle Ax_30	Earth Flow	Moderate	Pre-Historic	Tiha	25	8	0	7	45.0	13	148190
Battle Ax_31	Earth Flow	High	Pre-Historic	Tba	36	30	0	24	247.5	44	1717330
Battle Ax_32	Earth Flow	Moderate	Pre-Historic	Tu	18	80	0	76	45.0	29	3512156
Battle Ax_33	Debris Flow	Moderate	Pre-Historic	Tu	27	0	25	0	90.0	2	29373
Battle Ax_34	Debris Flow	Moderate	Pre-Historic	Tba	25	0	10	0	292.5	1	6653
Battle Ax_35	Earth Flow	High	Pre-Historic	Tum	26	20	0	18	157.5	45	1293252
Battle Ax_36	Earth Flow	Moderate	Pre-Historic	Tlm	28	120	0	106	247.5	11	1934926
Battle Ax_37	Translational	High	Pre-Historic	Tum	30	15	0	13	225.0	131	2745544
Battle Ax_38	Earth Flow	High	Pre-Historic	Tum	30	15	0	13	180.0	8	172831
Battle Ax_39*	Earth Flow	High	Historic	Qls	40	60	0	46	247.5	97	7203852
Battle Ax_40*	Translational	Moderate	Pre-Historic	Tum	35	14	0	11	247.5	100	1843448
Battle Ax_41	Debris Flow	Moderate	Pre-Historic	Tu	35	0	25	0	292.5	2	28831
Battle Ax_42	Debris Flow	Moderate	Pre-Historic	Qgf	38	0	40	0	270.0	2	40999
Battle Ax_43	Debris Flow	Moderate	Pre-Historic	Tu	24	0	40	0	22.5	1	27300
Battle Ax_44	Debris Flow	High	Historic	Tiha	40	0	25	0	292.5	19	254289
Battle Ax_45	Debris Flow	Moderate	Historic	Qyt	16	0	20	0	225.0	4	38020
Battle Ax_46	Earth Flow	High	Pre-Historic	Tr	24	18	0	16	202.5	2	62552

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Depth Classification	Flow Direction	Area (acres)	Volume (yd ³)
					Slope (°)	Height (ft)	Fan Height (ft)				
Battle Ax_47	Debris Flow	Moderate	Pre-Historic	Tu	35	0	10	0	337.5	1	5755
Battle Ax_48	Debris Flow	Moderate	Pre-Historic	Tu	30	0	15	0	135.0	1	8054
Battle Ax_49	Debris Flow	High	Pre-Historic	Tu	30	0	15	0	135.0	6	51411
Battle Ax_50	Debris Flow	High	Pre-Historic	Tu	28	0	15	0	90.0	4	31818
Battle Ax_51	Debris Flow	Moderate	Pre-Historic	Qgf	16	0	17	0	292.5	1	8634
Battle Ax_52	Debris Flow	Moderate	Pre-Historic	Tu	28	0	15	0	112.5	5	40378
Battle Ax_53	Rock Fall	High	Historic	Tb	30	45	0	39	247.5	27	1701804
Battle Ax_54	Debris Flow	Moderate	Pre-Historic	Tlm	10	0	25	0	45.0	17	221507
Battle Ax_55	Debris Flow	Moderate	Pre-Historic	Tlm	10	0	40	0	45.0	10	205717
Battle Ax_56	Debris Flow	Moderate	Pre-Historic	Tlm	10	0	30	0	225.0	11	173901
Battle Ax_57	Debris Flow	Moderate	Pre-Historic	Tlm	13	0	35	0	45.0	6	106727
Battle Ax_58	Debris Flow	Moderate	Pre-Historic	Tlm	10	0	35	0	202.5	6	116873
Battle Ax_59	Debris Flow	Moderate	Historic	Tlm	30	0	20	0	225.0	5	53565
Battle Ax_60	Debris Flow	Moderate	Pre-Historic	Yyt	11	0	30	0	292.5	1	17449
Battle Ax_61	Debris Flow	Moderate	Pre-Historic	Yyt	15	0	20	0	22.5	1	13491
Battle Ax_62	Debris Flow	Moderate	Pre-Historic	Yyt	7	0	25	0	45.0	1	15489
Battle Ax_63	Debris Flow	High	Historic	Yyt	24	0	10	0	225.0	5	29131
Battle Ax_64	Debris Flow	Moderate	Pre-Historic	Tu	20	0	30	0	270.0	1	20220
Battle Ax_65	Debris Flow	Moderate	Pre-Historic	Tu	14	0	35	0	45.0	1	16013
Battle Ax_66	Debris Flow	Moderate	Pre-Historic	Tu	15	0	25	0	337.5	1	13014
Battle Ax_67	Debris Flow	Moderate	Pre-Historic	Tu	18	0	20	0	45.0	1	10499
Battle Ax_68	Debris Flow	High	Pre-Historic	Tu	20	0	30	0	225.0	6	93205
Battle Ax_69	Debris Flow	Moderate	Pre-Historic	Tu	25	0	8	0	22.5	2	10621
Battle Ax_70	Debris Flow	Moderate	Pre-Historic	Tu	20	0	20	0	337.5	3	27185
Battle Ax_71	Debris Flow	Moderate	Pre-Historic	Tu	18	0	10	0	45.0	3	13842
Battle Ax_72	Debris Flow	Moderate	Pre-Historic	Tba	24	0	45	0	270.0	1	12778
Battle Ax_73	Debris Flow	Moderate	Pre-Historic	Tu	25	0	30	0	22.5	1	14738

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Fail Depth	Depth Classification	Flow		Volume
					Slope (°)	Height (ft)	Fan Height (ft)			Direction (°)	Area (acres)	
Battle Ax_74	Debris Flow	Moderate	Pre-Historic	Tu	20	0	40	0	na	22.5	1	23292
Battle Ax_75	Debris Flow	Moderate	Pre-Historic	Qgf	20	0	45	0	na	315.0	1	35666
Battle Ax_76	Debris Flow	Moderate	Pre-Historic	Qgf	15	0	40	0	na	22.5	3	73941
Battle Ax_77	Debris Flow	Moderate	Pre-Historic	Qgf	20	0	35	0	na	315.0	3	50534
Battle Ax_78	Debris Flow	Moderate	Pre-Historic	Qgf	23	0	40	0	na	315.0	2	33926
Battle Ax_79	Debris Flow	Moderate	Pre-Historic	Qgf	22	0	35	0	na	315.0	1	10652
Battle Ax_80	Debris Flow	Moderate	Pre-Historic	Qgf	22	0	10	0	na	315.0	2	10979
Battle Ax_81	Debris Flow	Moderate	Historic	Qgf	20	0	45	0	na	315.0	1	20612
Battle Ax_82	Debris Flow	Moderate	Pre-Historic	Qgf	20	0	45	0	na	315.0	1	19955
Battle Ax_83	Debris Flow	Moderate	Pre-Historic	Qgf	20	0	40	0	na	315.0	2	33519
Elkhorn_01	Rock Fall	Moderate	Pre-Historic	Tu	35	0	150	0	na	180.0	151	12094444
Elkhorn_02	Rock Fall	Moderate	Historic	Tu	32	0	15	0	na	0.0	3	20962
Elkhorn_03	Rock Fall	Moderate	Historic	Tu	50	0	25	0	na	135.0	2	32147
Elkhorn_04	Rock Fall	Low	Historic	Tu	45	0	35	0	na	45.0	6	103262
Elkhorn_05	Earth Flow	Moderate	Historic	Tu	30	40	0	35	Deep	315.0	9	479044
Elkhorn_06	Earth Flow	Moderate	Historic	Tu	30	25	0	22	Deep	202.5	20	708548
Elkhorn_07	Debris Flow	High	Pre-Historic	Tu	30	0	20	0	na	202.5	14	151330
Elkhorn_08	Rock Fall	High	Pre-Historic	Tu	30	0	10	0	na	202.5	6	32722
Elkhorn_09	Rock Fall	High	Pre-Historic	Tu	30	0	10	0	na	202.5	5	27056
Elkhorn_10	Rock Fall	High	Pre-Historic	Tu	30	0	15	0	na	202.5	4	32907
Elkhorn_11	Debris Flow	High	Pre-Historic	Tu	25	0	45	0	na	180.0	5	117053
Elkhorn_12	Rock Fall	High	Pre-Historic	Tu	28	0	40	0	na	180.0	4	89238
Elkhorn_13	Rock Fall	High	Pre-Historic	Tu	25	0	40	0	na	202.5	56	1183156
Elkhorn_14	Debris Flow	Moderate	Pre-Historic	Tu	23	0	45	0	na	180.0	4	102254
Elkhorn_15	Debris Flow	Moderate	Pre-Historic	Tu	25	0	45	0	na	0.0	5	107881
Elkhorn_16	Debris Flow	Moderate	Pre-Historic	Tu	18	0	30	0	na	0.0	40	632937
Elkhorn_17	Rotational	Moderate	Pre-Historic	Tfc	28	20	0	18	Deep	112.5	219	6233963

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Slope (°)	Fan Height (ft)	Fail Depth (ft)	Depth Classification	Flow Direction (°)	Area (acres)	Volume (yd ³)
					Height (ft)	Height (ft)	Depth (ft)							
Elkhorn_18	Earth Flow	Moderate	Pre-Historic	Tfc	30	0	28	20	30	0	Deep	225.0	123	5577667
Elkhorn_19	Earth Flow	Moderate	Pre-Historic	Tu	30	0	29	16	30	0	Deep	180.0	15	674678
Elkhorn_20*	Earth Flow	High	Historic	Tu	40	0	31	40	40	0	Deep	202.5	6	294276
Elkhorn_21*	Earth Flow	High	Historic	Tfc	30	0	25	35	30	0	Deep	247.5	23	910722
Elkhorn_22*	Earth Flow	High	Historic	Tu	20	0	18	28	20	0	Deep	337.5	27	760256
Elkhorn_23	Earth Flow	Moderate	Pre-Historic	Tu	50	0	38	40	50	0	Deep	270.0	39	2437141
Elkhorn_24*	Earth Flow	High	Historic	Tu	80	0	67	33	80	0	Deep	315.0	33	3549811
Elkhorn_25	Complex	High	Historic	Qls	70	0	66	20	70	0	Deep	0.0	689	73110000
Elkhorn_26	Earth Flow	High	Pre-Historic	Tu	19	0	16	30	19	0	Deep	0.0	1	26930
Elkhorn_27	Earth Flow	High	Pre-Historic	Qls	10	0	9	26	10	0	Shallow	135.0	1	14319
Elkhorn_28	Debris Flow	Moderate	Pre-Historic	Tu	0	10	0	20	0	10	na	270.0	2	12458
Elkhorn_29	Debris Flow	Moderate	Pre-Historic	Tu	0	20	0	25	0	20	na	292.5	3	37240
Elkhorn_30	Debris Flow	High	Historic	Tu	0	40	0	33	0	40	na	0.0	2	42724
Elkhorn_31	Debris Flow	Moderate	Pre-Historic	Tu	0	35	0	19	0	35	na	315.0	1	22246
Elkhorn_32	Debris Flow	Moderate	Pre-Historic	Tu	0	40	0	22	0	40	na	270.0	4	79606
Elkhorn_33	Debris Flow	High	Pre-Historic	Tu	0	30	0	20	0	30	na	270.0	8	121911
Elkhorn_34	Debris Flow	Moderate	Pre-Historic	Tu	0	35	0	20	0	35	na	270.0	1	24240
Elkhorn_35*	Earth Flow	High	Historic	Qls	34	0	32	20	34	0	Deep	135.0	343	17667926
Elkhorn_36	Earth Flow	High	Historic	Tu	40	0	35	30	40	0	Deep	247.5	4	229840
Elkhorn_37*	Earth Flow	High	Pre-Historic	Tu	20	0	19	14	20	0	Deep	67.5	6	178421
Elkhorn_38	Earth Flow	High	Pre-Historic	Tu	35	0	27	39	35	0	Deep	45.0	2	107699
Elkhorn_39	Earth Flow	Moderate	Pre-Historic	Tu	50	0	42	32	50	0	Deep	45.0	16	1085919
Elkhorn_40	Debris Flow	Moderate	Pre-Historic	Qt	0	10	0	5	0	10	na	315.0	1	3990
Elkhorn_41	Debris Flow	Moderate	Pre-Historic	Tu	0	25	0	7	0	25	na	0.0	1	8487
Elkhorn_42	Debris Flow	Moderate	Pre-Historic	Tu	0	35	0	20	0	35	na	22.5	10	177648
Elkhorn_43	Debris Flow	Moderate	Pre-Historic	Tu	0	15	0	10	0	15	na	22.5	1	10392
Elkhorn_44	Debris Flow	Moderate	Pre-Historic	Tu	0	25	0	8	0	25	na	180.0	49	653574

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Slope		Head Scarp Height		Fan Height	Fail Depth	Depth Classification	Flow Direction	Area (acres)	Volume (yd ³)
					(°)	(ft)	(ft)	(ft)				(°)		
Elkhorn_45	Debris Flow	Moderate	Pre-Historic	Tu	8	0	0	0	35	0	na	157.5	30	565841
Elkhorn_46	Debris Flow	Moderate	Pre-Historic	Qt	12	0	0	0	35	0	na	292.5	16	298866
Elkhorn_47	Debris Flow	High	Historic	Tu	33	0	0	0	20	0	na	157.5	11	121500
Elkhorn_48	Debris Flow	Moderate	Pre-Historic	Tu	36	0	0	0	25	0	na	22.5	1	10633
Elkhorn_49	Debris Flow	High	Historic	Tu	34	0	0	0	25	0	na	202.5	1	11434
Elkhorn_50	Rock Fall	Moderate	Historic	Tu	36	0	0	0	30	0	na	180.0	4	70558
Elkhorn_51	Rock Fall	Moderate	Historic	Tu	37	0	0	0	20	0	na	157.5	3	28768
Elkhorn_52	Debris Flow	Moderate	Pre-Historic	Tu	5	0	0	0	35	0	na	22.5	6	112573
Elkhorn_53	Debris Flow	Moderate	Pre-Historic	Tlm	30	0	0	0	45	0	na	247.5	2	55954
Elkhorn_54	Debris Flow	Moderate	Pre-Historic	Tlm	31	0	0	0	35	0	na	157.5	4	67355
Elkhorn_55	Debris Flow	High	Historic	Tu	30	0	0	0	30	0	na	135.0	18	293663
Elkhorn_56	Debris Flow	High	Historic	Tu	30	0	0	0	40	0	na	135.0	13	269553
Elkhorn_57	Debris Flow	High	Historic	Tu	30	0	0	0	25	0	na	67.5	3	37137
Elkhorn_58	Debris Flow	High	Historic	Tu	15	0	0	0	40	0	na	202.5	11	234909
Elkhorn_59	Debris Flow	High	Historic	Tu	28	0	0	0	40	0	na	202.5	5	96213
Elkhorn_60	Debris Flow	High	Historic	Tu	32	0	0	0	30	0	na	22.5	6	96415
Elkhorn_61	Debris Flow	High	Historic	Tu	32	0	0	0	35	0	na	0.0	4	70445
Elkhorn_62	Debris Flow	High	Historic	Tu	32	0	0	0	35	0	na	0.0	3	48226
Elkhorn_63	Debris Flow	High	Historic	Tu	13	0	0	0	25	0	na	315.0	2	23914
Elkhorn_64	Debris Flow	Moderate	Pre-Historic	Tu	38	0	0	0	35	0	na	22.5	2	28541
Elkhorn_65	Debris Flow	Moderate	Pre-Historic	Tu	30	0	0	0	45	0	na	67.5	3	64241
Elkhorn_66	Debris Flow	Moderate	Pre-Historic	Tu	35	0	0	0	35	0	na	315.0	2	37612
Elkhorn_67	Debris Flow	Moderate	Pre-Historic	Tu	35	0	0	0	20	0	na	315.0	1	8794
Elkhorn_68	Debris Flow	Moderate	Pre-Historic	Tu	8	0	0	0	15	0	na	337.5	1	7962
Elkhorn_69	Debris Flow	Moderate	Pre-Historic	Tu	15	0	0	0	20	0	na	157.5	4	39054
Elkhorn_70	Debris Flow	Moderate	Pre-Historic	Qt	25	0	0	0	30	0	na	0.0	4	63877
Elkhorn_71	Debris Flow	Moderate	Pre-Historic	Qt	25	0	0	0	20	0	na	337.5	1	11568

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Fan Height	Fail Depth	Depth Classification	Flow Direction	Area (acres)	Volume (yd ³)
					Slope (°)	Height (ft)	Height (ft)						
Elkhorn_72	Debris Flow	Moderate	Pre-Historic	Qt	22	0	50	0	0	na	315.0	15	391719
Elkhorn_73	Debris Flow	Moderate	Pre-Historic	Qt	4	0	25	0	0	na	315.0	4	50527
Elkhorn_74	Debris Flow	Moderate	Pre-Historic	Qt	5	0	25	0	0	na	315.0	6	76583
Elkhorn_75	Debris Flow	Moderate	Pre-Historic	Qt	4	0	20	0	0	na	337.5	2	20508
Elkhorn_76	Debris Flow	Moderate	Pre-Historic	Qls	25	0	40	0	0	na	315.0	38	805678
Elkhorn_77	Debris Flow	Moderate	Pre-Historic	Qls	10	0	10	0	0	na	157.5	2	8406
Elkhorn_78	Debris Flow	Moderate	Pre-Historic	Qls	3	0	14	0	0	na	157.5	5	37479
Elkhorn_79	Debris Flow	Moderate	Pre-Historic	Tu	5	0	14	0	0	na	202.5	9	68378
Elkhorn_80	Debris Flow	Moderate	Pre-Historic	Tu	4	0	20	0	0	na	180.0	4	41638
Elkhorn_81	Debris Flow	Moderate	Pre-Historic	Qt	4	0	25	0	0	na	202.5	4	57614
Elkhorn_82	Debris Flow	Moderate	Pre-Historic	Tu	10	0	45	0	0	na	180.0	50	1196437
Lyons_01*	Complex	High	Historic	Qls	15	100	0	0	97	Deep	180.0	1341	209034074
Lyons_02	Earth Flow	Moderate	Historic	Tba	20	120	0	0	113	Deep	225.0	40	7194407
Lyons_03	Complex	High	Historic	Tba	20	70	0	0	66	Deep	157.5	111	11821037
Lyons_04	Earth Flow	High	Historic	Tc	22	60	0	0	56	Deep	180.0	9	796004
Lyons_05	Earth Flow	High	Historic	Tu	20	40	0	0	38	Deep	180.0	104	6290593
Lyons_06	Earth Flow	Moderate	Historic	Tu	20	16	0	0	15	Shallow	157.5	7	170794
Lyons_07	Earth Flow	High	Pre-Historic	Tu	25	35	0	0	32	Deep	0.0	71	3633174
Lyons_08	Complex	High	Historic	Tc	18	20	0	0	19	Deep	180.0	370	11350222
Lyons_09	Complex	High	Historic	Tfc	15	60	0	0	58	Deep	180.0	426	39811852
Lyons_10	Complex	High	Historic	Qls	15	80	0	0	77	Deep	0.0	553	68957037
Lyons_11*	Earth Flow	Moderate	Pre-Historic	Qls	20	100	0	0	94	Deep	157.5	87	13180222
Lyons_12	Earth Flow	High	Historic	Qls	25	40	0	0	36	Deep	180.0	10	568967
Lyons_13	Earth Flow	Moderate	Pre-Historic	Qls	37	40	0	0	32	Deep	337.5	10	498459
Lyons_14	Rotational	Moderate	Pre-Historic	Qt	44	50	0	0	36	Deep	45.0	5	294108
Lyons_15	Earth Flow	High	Historic	Tu	20	20	0	0	19	Deep	202.5	7	206951
Lyons_16*	Earth Flow	High	Historic	Tu	20	20	0	0	19	Deep	202.5	3	101460

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Depth Classification	Flow Direction	Area (acres)	Volume (yd ³)
					Slope (°)	Height (ft)	Fan Height (ft)				
Lyons_17*	Earth Flow	High	Historic	Tu	20	20	0	19	202.5	20	606600
Lyons_18*	Complex	High	Historic	Tu	20	60	0	56	202.5	114	10335778
Lyons_19	Earth Flow	High	Historic	Tba	12	30	0	29	180.0	17	797011
Lyons_20	Earth Flow	Moderate	Pre-Historic	Tu	28	100	0	88	22.5	64	9106407
Lyons_21*	Earth Flow	High	Historic	Tu	30	60	0	52	225.0	10	847400
Lyons_22	Debris Flow	High	Historic	Qau	3	0	15	0	0.0	2	12570
Lyons_23	Debris Flow	Moderate	Pre-Historic	Qal	8	0	10	0	315.0	14	76769
Lyons_24	Debris Flow	Moderate	Pre-Historic	Qau	3	0	15	0	22.5	2	14870
Lyons_25	Debris Flow	Moderate	Pre-Historic	Qau	3	0	15	0	0.0	1	7465
Lyons_26	Debris Flow	Moderate	Pre-Historic	Tu	22	0	30	0	337.5	6	95154
Lyons_27	Debris Flow	Moderate	Pre-Historic	Qt	4	0	20	0	337.5	2	17351
Lyons_28	Debris Flow	Moderate	Pre-Historic	Qt	4	0	25	0	337.5	1	10578
Lyons_29	Debris Flow	Moderate	Pre-Historic	Qt	3	0	20	0	0.0	4	43762
Lyons_30	Debris Flow	Moderate	Pre-Historic	Qt	3	0	25	0	0.0	2	29293
Lyons_31	Debris Flow	Moderate	Pre-Historic	Qt	3	0	15	0	0.0	1	6680
Lyons_32	Debris Flow	Moderate	Pre-Historic	Qt	3	0	30	0	337.5	1	13645
Lyons_33	Debris Flow	Moderate	Pre-Historic	Qls	8	0	20	0	270.0	3	31394
Lyons_34	Debris Flow	Moderate	Pre-Historic	Qt	10	0	20	0	337.5	1	10541
Lyons_35	Debris Flow	Moderate	Pre-Historic	Qls	5	0	15	0	157.5	2	14464
Lyons_36	Debris Flow	Moderate	Pre-Historic	Qls	3	0	35	0	202.5	16	295806
Lyons_37	Debris Flow	High	Historic	Tba	5	0	15	0	225.0	1	5294
Lyons_38	Debris Flow	High	Historic	Tba	7	0	40	0	157.5	2	32514
Lyons_39	Debris Flow	Moderate	Pre-Historic	Qt	5	0	40	0	22.5	7	143187
Lyons_40	Debris Flow	Moderate	Pre-Historic	Qt	5	0	10	0	22.5	1	5583
Lyons_41	Debris Flow	High	Pre-Historic	Tu	6	0	25	0	202.5	2	28115
Lyons_42	Debris Flow	High	Pre-Historic	Tu	6	0	25	0	202.5	2	21856
Lyons_43	Earth Flow	High	Pre-Historic	Tc	25	10	0	9	157.5	5	74152

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Depth Classification	Flow Direction	Area (acres)	Volume (yd ³)
					Slope (°)	Height (ft)	Fan Height (ft)				
Lyons_44	Earth Flow	High	Pre-Historic	Tba	20	30	0	Deep	180.0	11	515585
Lyons_45	Earth Flow	High	Pre-Historic	Tc	20	15	0	Shallow	180.0	13	294642
Lyons_46*	Rotational	Moderate	Pre-Historic	Tu	22	15	0	Shallow	180.0	15	335949
Lyons_47	Earth Flow	High	Pre-Historic	Tu	25	40	0	Deep	90.0	10	576285
Lyons_48	Earth Flow	Moderate	Pre-Historic	Tu	18	20	0	Deep	67.5	3	79890
Lyons_49	Earth Flow	High	Pre-Historic	Tu	15	25	0	Deep	67.5	11	444822
Lyons_50	Earth Flow	Moderate	Pre-Historic	Tu	24	20	0	Deep	45.0	11	333857
Lyons_51	Earth Flow	High	Pre-Historic	Qls	26	60	0	Deep	292.5	17	1507385
Lyons_52	Earth Flow	High	Pre-Historic	Tu	20	30	0	Deep	270.0	4	181066
Lyons_53	Earth Flow	High	Pre-Historic	Qt	10	40	0	Deep	337.5	22	1366507
Lyons_54	Earth Flow	High	Historic	Tu	15	50	0	Deep	90.0	24	1907230
Lyons_55	Rotational	High	Historic	Tba	24	20	0	Deep	180.0	2	47485
Mill City North_01	Earth Flow	High	Pre-Historic	Qt	37	20	0	Deep	22.5	5	135988
Mill City North_02	Earth Flow	High	Historic	Tu	28	70	0	Deep	225.0	44	4396111
Mill City North_03	Earth Flow	Low	Pre-Historic	Tu	16	40	0	Deep	225.0	29	1812633
Mill City North_04	Earth Flow	High	Pre-Historic	Qls	28	21	0	Deep	22.5	9	263682
Mill City North_05	Rotational	Low	Pre-Historic	Tu	25	60	0	Deep	0.0	16	1417574
Mill City North_06	Earth Flow	Moderate	Pre-Historic	Tu	18	40	0	Deep	180.0	2	149544
Mill City North_07	Earth Flow	High	Historic	Qls	20	29	0	Deep	112.5	42	1845781
Mill City North_08*	Earth Flow	Moderate	Historic	Qls	15	20	0	Deep	202.5	8	253648
Mill City North_09*	Complex	High	Pre-Historic	Qls	15	800	0	Deep	135.0	1776	2213600000
Mill City North_10*	Earth Flow	High	Historic	Qls	15	70	0	Deep	135.0	1109	121023704
Mill City North_11	Earth Flow	High	Pre-Historic	Qls	13	15	0	Shallow	90.0	4	99641
Mill City North_12	Earth Flow	High	Pre-Historic	Tu	21	60	0	Deep	22.5	53	4753667
Mill City North_13	Earth Flow	Moderate	Pre-Historic	Tu	14	20	0	Deep	45.0	22	687967
Mill City North_14	Earth Flow	Moderate	Pre-Historic	Tu	22	40	0	Deep	315.0	37	2209330
Mill City North_15	Debris Flow	Moderate	Historic	Qt	17	0	20	na	0.0	5	55731

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Depth Classification	Flow Direction	Area (acres)	Volume (yd ³)
					Slope (°)	Height (ft)	Fan Height (ft)				
Mill City North_16	Earth Flow	High	Pre-Historic	Tu	13	40	0	Deep	22.5	7	465067
Mill City North_17	Earth Flow	High	Pre-Historic	Tu	20	20	0	Deep	0.0	2	64166
Mill City North_18	Earth Flow	High	Pre-Historic	Tu	20	40	0	Deep	315.0	5	296823
Mill City North_19*	Earth Flow	High	Pre-Historic	Tu	20	20	0	Deep	315.0	2	59080
Mill City North_20*	Complex	Moderate	Pre-Historic	Tu	18	60	0	Deep	90.0	138	12683889
Mill City North_21	Earth Flow	High	Historic	Qls	15	25	0	Deep	112.5	19	750126
Mill City North_22	Earth Flow	High	Historic	Tfc	36	30	0	Deep	202.5	1	34653
Mill City North_23*	Earth Flow	High	Pre-Historic	Tfc	15	60	0	Deep	202.5	26	2418356
Mill City North_24	Earth Flow	Moderate	Pre-Historic	Tu	20	8	0	Shallow	202.5	1	17153
Mill City North_25*	Earth Flow	Moderate	Pre-Historic	Tfc	16	10	0	Shallow	135.0	3	39821
Mill City North_26	Earth Flow	Low	Pre-Historic	Tu	30	20	0	Deep	225.0	1	21196
Mill City North_27	Earth Flow	Moderate	Historic	Tfc	34	30	0	Deep	225.0	1	32968
Mill City North_28	Earth Flow	High	Historic	Tfc	20	30	0	Deep	202.5	3	133904
Mill City North_29	Earth Flow	Moderate	Pre-Historic	Tfc	40	60	0	Deep	0.0	18	1366941
Mill City North_30	Earth Flow	High	Pre-Historic	Tfc	23	30	0	Deep	180.0	6	254209
Mill City North_31*	Earth Flow	High	Pre-Historic	Tfc	22	20	0	Deep	135.0	1	21701
Mill City North_32	Earth Flow	Moderate	Historic	Qls	15	25	0	Deep	112.5	169	6585037
Mill City North_33	Earth Flow	High	Pre-Historic	Tfc	25	60	0	Deep	202.5	5	395330
Mill City North_34	Earth Flow	High	Pre-Historic	Qls	25	60	0	Deep	202.5	45	3929000
Mill City North_35	Earth Flow	Moderate	Pre-Historic	Qls	20	40	0	Deep	225.0	10	577693
Mill City North_36	Earth Flow	Moderate	Pre-Historic	Tfc	29	50	0	Deep	135.0	6	436615
Mill City North_37	Earth Flow	Moderate	Pre-Historic	Tfc	19	20	0	Deep	202.5	13	394893
Mill City North_38	Earth Flow	Low	Pre-Historic	Tfc	22	20	0	Deep	225.0	4	119436
Mill City North_39	Earth Flow	High	Historic	Tfc	22	16	0	Shallow	202.5	4	91031
Mill City North_40	Earth Flow	High	Historic	Tfc	23	20	0	Deep	202.5	2	67846
Mill City North_41	Earth Flow	High	Historic	Tfc	22	20	0	Deep	202.5	4	130104
Mill City North_42	Earth Flow	High	Historic	Tfc	20	18	0	Deep	202.5	7	188404

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Depth Classification	Flow Direction	Area (acres)	Volume (yd ³)
					Slope (°)	Height (ft)	Fan Height (ft)				
Mill City North_43	Earth Flow	Moderate	Pre-Historic	Qls	15	250	0	Deep	112.5	98	38208148
Mill City North_44	Earth Flow	High	Historic	Tfc	22	10	0	Shallow	202.5	3	48627
Mill City North_45	Earth Flow	High	Pre-Historic	Tu	26	40	0	Deep	90.0	1	70996
Mill City North_46	Earth Flow	Moderate	Pre-Historic	Tu	28	30	0	Deep	157.5	1	29546
Mill City North_47	Earth Flow	Moderate	Pre-Historic	Tu	28	30	0	Deep	135.0	1	38704
Mill City North_48	Earth Flow	Moderate	Pre-Historic	Tu	24	30	0	Deep	135.0	1	38820
Mill City North_49	Earth Flow	High	Historic	Tu	32	23	0	Deep	270.0	3	82422
Mill City North_50	Earth Flow	High	Historic	Tu	30	15	0	Shallow	270.0	5	107097
Mill City North_51	Earth Flow	High	Historic	Tu	22	18	0	Deep	225.0	1	38945
Mill City North_52	Earth Flow	High	Historic	Tu	15	10	0	Shallow	202.5	8	119903
Mill City North_53	Earth Flow	High	Historic	Tfc	25	24	0	Deep	225.0	3	109930
Mill City North_54	Rotational	Low	Pre-Historic	Tus	20	53	0	Deep	90.0	17	1395504
Mill City North_55	Earth Flow	High	Pre-Historic	Tu	30	12	0	Shallow	135.0	1	14622
Mill City North_56	Earth Flow	High	Historic	Tu	15	25	0	Deep	247.5	61	2363200
Mill City North_57	Earth Flow	High	Pre-Historic	Tu	18	18	0	Deep	225.0	3	91455
Mill City North_58	Earth Flow	High	Historic	Tu	30	30	0	Deep	157.5	13	530559
Mill City North_59	Earth Flow	Moderate	Pre-Historic	Tu	28	25	0	Deep	112.5	3	99194
Mill City North_60	Earth Flow	High	Historic	Tu	12	28	0	Deep	247.5	1	58802
Mill City North_61	Earth Flow	Moderate	Pre-Historic	Tu	11	45	0	Deep	270.0	7	479800
Mill City North_62	Earth Flow	Moderate	Pre-Historic	Tu	32	32	0	Deep	90.0	1	59102
Mill City North_63	Earth Flow	High	Historic	Tfc	15	44	0	Deep	247.5	6	382481
Mill City North_64	Earth Flow	High	Historic	Tfc	26	50	0	Deep	90.0	8	548459
Mill City North_65	Earth Flow	Moderate	Pre-Historic	Tba	35	40	0	Deep	180.0	5	288527
Mill City North_66	Earth Flow	High	Historic	Tfc	25	50	0	Deep	225.0	15	1093300
Mill City North_67	Earth Flow	High	Pre-Historic	Tfc	30	45	0	Deep	67.5	1	75102
Mill City North_68	Earth Flow	High	Historic	Tu	22	30	0	Deep	180.0	5	218270
Mill City North_69	Earth Flow	Moderate	Pre-Historic	Tfc	16	60	0	Deep	90.0	18	1689763

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Fail Depth	Depth Classification	Flow		Volume
					Slope (°)	Height (ft)	Fan Height (ft)			Direction (°)	Area (acres)	
Mill City North_70	Earth Flow	Moderate	Historic	Tfc	22	20	0	19	Deep	90.0	3	92939
Mill City North_71	Earth Flow	High	Historic	Tfc	25	25	0	23	Deep	90.0	3	110955
Mill City North_72	Earth Flow	High	Pre-Historic	Tu	28	50	0	44	Deep	22.5	2	146840
Mill City North_73*	Earth Flow	Moderate	Pre-Historic	Tu	34	20	0	17	Deep	270.0	1	23482
Mill City North_74	Earth Flow	Moderate	Pre-Historic	Tu	25	60	0	54	Deep	202.5	1	123317
Mill City North_75	Earth Flow	High	Historic	Tfc	15	20	0	19	Deep	202.5	4	116445
Mill City North_76	Complex	High	Pre-Historic	Tu	12	50	0	49	Deep	0.0	77	6086370
Mill City North_77	Earth Flow	High	Historic	Tu	25	25	0	23	Deep	157.5	7	246252
Mill City North_78	Earth Flow	Moderate	Historic	Tu	20	40	0	38	Deep	202.5	4	258079
Mill City North_79	Earth Flow	Moderate	Historic	Tu	18	40	0	38	Deep	247.5	2	119349
Mill City North_80	Earth Flow	Moderate	Pre-Historic	Tu	23	40	0	37	Deep	315.0	17	985863
Mill City North_81	Earth Flow	High	Historic	Tu	24	15	0	14	Shallow	247.5	2	53208
Mill City North_82	Earth Flow	High	Historic	Tu	24	18	0	16	Deep	202.5	7	174419
Mill City North_83	Earth Flow	High	Historic	Tu	21	50	0	47	Deep	180.0	5	358511
Mill City North_84	Earth Flow	High	Historic	Tu	22	40	0	37	Deep	135.0	7	427089
Mill City North_85	Earth Flow	High	Historic	Tu	20	30	0	28	Deep	202.5	5	232841
Mill City North_86	Earth Flow	High	Historic	Tu	24	15	0	14	Shallow	157.5	2	41583
Mill City North_87	Rotational	Moderate	Pre-Historic	Tfc	30	10	0	9	Shallow	112.5	2	30218
Mill City North_88	Earth Flow	High	Historic	Tu	24	30	0	27	Deep	135.0	3	125009
Mill City North_89	Earth Flow	High	Historic	Tu	24	40	0	37	Deep	135.0	1	85318
Mill City North_90	Earth Flow	High	Historic	Tu	24	20	0	18	Deep	225.0	2	65260
Mill City North_91*	Earth Flow	High	Pre-Historic	Qls	14	18	0	17	Deep	225.0	3	80586
Mill City North_92	Earth Flow	Moderate	Pre-Historic	Tu	14	10	0	10	Shallow	247.5	8	129873
Mill City North_93	Earth Flow	High	Historic	Tfc	28	8	0	7	Shallow	180.0	1	15267
Mill City North_94	Earth Flow	High	Pre-Historic	Tu	25	60	0	54	Deep	292.5	56	4880259
Mill City North_95	Complex	High	Historic	Qls	16	100	0	96	Deep	157.5	3874	601603704
Mill City North_96	Earth Flow	Moderate	Historic	Tba	15	16	0	15	Shallow	202.5	6	137336

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp		Fan Height	Fail Depth	Depth Classification	Flow		Volume
					Slope (°)	Height (ft)				Direction (°)	Area (acres)	
Mill City North_97	Earth Flow	Moderate	Pre-Historic	Tba	20	50	0	47	Deep	157.5	31	2326796
Mill City North_98	Earth Flow	High	Historic	Tu	31	80	0	69	Deep	135.0	28	3113607
Mill City North_99	Earth Flow	Moderate	Pre-Historic	Tu	31	15	0	13	Shallow	135.0	1	20018
Mill City North_100	Rotational	Moderate	Historic	Tu	20	10	0	9	Shallow	157.5	18	265643
Mill City North_101	Earth Flow	High	Pre-Historic	Tu	14	18	0	17	Deep	247.5	23	641819
Mill City North_102	Earth Flow	High	Pre-Historic	Tba	12	60	0	59	Deep	112.5	80	7607889
Mill City North_103	Earth Flow	High	Historic	Tba	23	100	0	92	Deep	157.5	98	14627593
Mill City North_104	Earth Flow	Moderate	Historic	Tfc	24	60	0	55	Deep	157.5	48	4279148
Mill City North_105	Complex	High	Historic	Qls	13	50	0	49	Deep	0.0	729	57260741
Mill City North_106	Earth Flow	High	Historic	Tu	15	10	0	10	Shallow	157.5	7	113415
Mill City North_107	Earth Flow	High	Historic	Qls	12	50	0	49	Deep	0.0	146	11516815
Mill City North_108	Earth Flow	High	Historic	Tu	20	17	0	16	Shallow	225.0	5	107483
Mill City North_109	Earth Flow	High	Pre-Historic	Qls	25	50	0	45	Deep	67.5	4	265702
Mill City North_110	Complex	High	Pre-Historic	Tu	20	50	0	47	Deep	0.0	79	5998593
Mill City North_111	Complex	High	Historic	Tu	15	100	0	97	Deep	0.0	149	23287407
Mill City North_112	Earth Flow	High	Pre-Historic	Tu	26	35	0	31	Deep	112.5	5	238109
Mill City North_113	Earth Flow	Moderate	Historic	Qls	12	40	0	39	Deep	0.0	63	3967852
Mill City North_114	Earth Flow	High	Historic	Qt	14	16	0	16	Shallow	45.0	9	233859
Mill City North_115	Earth Flow	Moderate	Historic	Tu	20	40	0	38	Deep	225.0	7	431281
Mill City North_116	Earth Flow	Moderate	Historic	Tu	15	15	0	14	Shallow	157.5	18	423656
Mill City North_117	Earth Flow	High	Pre-Historic	Tu	25	60	0	54	Deep	202.5	6	518596
Mill City North_118	Earth Flow	High	Historic	Tu	15	45	0	43	Deep	67.5	39	2726915
Mill City North_119	Earth Flow	High	Pre-Historic	Tu	16	30	0	29	Deep	22.5	6	273437
Mill City North_120	Earth Flow	High	Historic	Tu	20	40	0	38	Deep	292.5	14	827922
Mill City North_121	Complex	High	Historic	Tu	18	60	0	57	Deep	292.5	102	9352926
Mill City North_122	Complex	High	Pre-Historic	Tu	12	20	0	20	Deep	67.5	51	1618307
Mill City North_123	Earth Flow	Low	Pre-Historic	Tfc	30	40	0	35	Deep	337.5	3	161228

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Depth Classification	Flow Direction	Area (acres)	Volume (yd ³)
					Slope (°)	Height (ft)	Fan Height (ft)				
Mill City North_124	Complex	High	Historic	Tu	15	50	0	48	0.0	105	8193704
Mill City North_125	Debris Flow	Moderate	Pre-Historic	Tfc	32	0	20	0	202.5	3	28453
Mill City North_126	Debris Flow	Moderate	Pre-Historic	Tfc	30	0	15	0	180.0	1	4784
Mill City North_127	Debris Flow	Moderate	Pre-Historic	Tfc	15	0	25	0	135.0	1	12690
Mill City North_128	Debris Flow	Moderate	Pre-Historic	Tfc	15	0	25	0	135.0	1	10341
Mill City North_129	Debris Flow	Moderate	Pre-Historic	Tfc	20	0	40	0	135.0	14	306760
Mill City North_130	Debris Flow	Moderate	Pre-Historic	Qls	20	0	30	0	135.0	11	174920
Mill City North_131	Debris Flow	Moderate	Pre-Historic	Qls	20	0	15	0	135.0	4	31765
Mill City North_132	Debris Flow	Moderate	Pre-Historic	Qt	5	0	30	0	270.0	3	48412
Mill City North_133	Debris Flow	Moderate	Pre-Historic	Qt	5	0	10	0	270.0	5	24061
Mill City North_134	Debris Flow	Moderate	Pre-Historic	Qls	4	0	30	0	135.0	45	724133
Mill City North_135	Debris Flow	Moderate	Pre-Historic	Tus	20	0	20	0	135.0	5	48851
Mill City North_136	Debris Flow	Moderate	Pre-Historic	Tus	20	0	30	0	135.0	7	115747
Mill City North_137	Debris Flow	Moderate	Pre-Historic	Qls	13	0	20	0	135.0	13	136525
Mill City North_138	Debris Flow	Moderate	Pre-Historic	Qt	4	0	20	0	315.0	32	341329
Mill City North_139	Debris Flow	Moderate	Pre-Historic	Qt	4	0	30	0	315.0	45	716815
Mill City North_140	Debris Flow	Moderate	Pre-Historic	Qt	4	0	15	0	0.0	4	31795
Mill City North_141	Debris Flow	Moderate	Pre-Historic	Qt	3	0	20	0	0.0	3	30102
Mill City North_142	Debris Flow	Moderate	Pre-Historic	Qt	3	0	35	0	292.5	7	138061
Mill City North_143*	Debris Flow	Moderate	Pre-Historic	Tu	4	0	30	0	337.5	15	247407
Mill City North_144	Debris Flow	Moderate	Pre-Historic	Tu	20	0	12	0	202.5	1	3406
Mill City North_145	Debris Flow	Moderate	Pre-Historic	Tu	20	0	20	0	180.0	2	18132
Mill City North_146	Debris Flow	Moderate	Pre-Historic	Tu	20	0	15	0	157.5	1	7060
Mill City North_147	Debris Flow	Moderate	Pre-Historic	Tu	6	0	20	0	180.0	5	57283
Mill City North_148	Debris Flow	Moderate	Pre-Historic	Tu	30	0	30	0	180.0	1	9919
Mill City North_149	Debris Flow	Moderate	Pre-Historic	Tu	5	0	35	0	180.0	6	105913
Mill City North_150	Earth Flow	High	Historic	Qt	32	40	0	34	292.5	6	306432

Unique ID	Movement Type	Confidence	Relative Age	Primary Lithology	Head Scarp			Depth Classification	Flow Direction	Area (acres)	Volume (yd ³)
					Slope (°)	Height (ft)	Fan Height (ft)				
Mill City North_151	Earth Flow	High	Historic	Qt	44	30	0	22	22.5	1	19664
Mill City North_152	Earth Flow	High	Historic	Qt	33	10	0	8	292.5	1	10471
Mill City North_153	Earth Flow	High	Historic	Qt	8	15	0	15	292.5	1	12713
Mill City North_154	Earth Flow	High	Historic	Qt	35	15	0	12	292.5	1	10304
Mill City North_155	Debris Flow	High	Historic	Tfc	30	0	35	0	180.0	1	23514
Mill City North_156	Debris Flow	High	Historic	Tfc	20	0	20	0	112.5	1	7366
Mill City North_157	Debris Flow	Moderate	Pre-Historic	Tfc	25	0	10	0	180.0	1	4226
Mill City North_158*	Debris Flow	High	Historic	Qt	8	0	15	0	0.0	1	8126
Mill City North_159	Earth Flow	High	Pre-Historic	Qt	20	60	0	56	0.0	6	574185
Mill City North_160*	Earth Flow	High	Pre-Historic	Qt	20	50	0	47	0.0	6	433600
Mill City North_161	Earth Flow	High	Pre-Historic	Qt	20	30	0	28	0.0	1	56246
Mill City North_162	Complex	High	Historic	Tba	15	40	0	39	202.5	264	16434333
Mill City North_163	Earth Flow	High	Pre-Historic	Tu	14	30	0	29	67.5	14	655411
Mill City North_164	Debris Flow	Moderate	Pre-Historic	Qt	17	0	35	0	292.5	4	72818
Mill City North_165	Earth Flow	High	Pre-Historic	Tu	19	40	0	38	292.5	16	979319
Mill City North_166	Complex	High	Historic	Tu	15	40	0	39	0.0	220	13698852
Mill City North_167	Complex	High	Pre-Historic	Tu	15	30	0	29	0.0	72	3387956
Mill City North_168	Debris Flow	Moderate	Pre-Historic	Tu	15	0	8	0	0.0	1	2373
Mill City North_169	Debris Flow	Moderate	Pre-Historic	Tu	15	0	12	0	0.0	1	7123
Mill City North_170	Debris Flow	Moderate	Pre-Historic	Tu	15	0	10	0	0.0	1	4905
Mill City North_171	Debris Flow	Moderate	Pre-Historic	Tu	15	0	10	0	0.0	1	2732
Mill City North_172	Debris Flow	Moderate	Pre-Historic	Tu	15	0	10	0	0.0	1	5474
Mill City North_173	Debris Flow	Moderate	Pre-Historic	Tu	15	0	10	0	0.0	1	2870
Mill City North_174	Earth Flow	High	Historic	Qls	18	30	0	29	337.5	2	108673
Rooster Rock_01	Earth Flow	Low	Pre-Historic	Tum	42	15	0	11	135.0	1	20967
Rooster Rock_02	Debris Flow	Moderate	Pre-Historic	Tfc	30	0	40	0	112.5	1	15670
Rooster Rock_03	Earth Flow	Moderate	Pre-Historic	Tfc	31	50	0	43	67.5	10	671289

A.3 – Continuous Turbidity, Estimated Streamflow, and Suspended-Sediment Loads

[Abbreviations: FNU, Formazin Nephelometric Units; ft^3/s , cubic feet per second; SSC, suspended-sediment concentrations; mg/L , milligrams per liter; SSL, suspended-sediment loads; T, short tons]

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft^3/s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft^3/s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft^3/s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft^3/s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft^3/s)	SSC (mg/L)	SSL (T)
12/1/09 0:30	1.7	617	3.1	0.1	0.3	539	0.5	0.0	0.3	474	0.5	0.0	0.4	375	0.7	0.0	12.0	19	16.6	0.0
12/1/09 1:00	1.7	611	3.1	0.1	0.4	534	0.7	0.0	0.3	469	0.5	0.0	0.4	372	0.7	0.0	12.0	19	16.6	0.0
12/1/09 1:30	1.9	611	3.5	0.1	0.3	533	0.5	0.0	0.3	467	0.5	0.0	1.2	368	2.2	0.0	13.0	19	18.1	0.0
12/1/09 2:00	1.9	611	3.5	0.1	0.3	534	0.5	0.0	0.4	469	0.7	0.0	0.4	372	0.7	0.0	13.0	19	18.1	0.0
12/1/09 2:30	1.7	605	3.1	0.1	0.4	529	0.7	0.0	0.4	465	0.7	0.0	0.4	368	0.7	0.0	13.0	19	18.1	0.0
12/1/09 3:00	2.0	605	3.7	0.1	0.3	529	0.5	0.0	0.3	465	0.5	0.0	0.4	368	0.7	0.0	12.0	19	16.6	0.0
12/1/09 3:30	1.8	599	3.3	0.1	0.3	524	0.5	0.0	0.4	460	0.7	0.0	0.4	365	0.7	0.0	11.0	18	15.2	0.0
12/1/09 4:00	1.7	599	3.1	0.1	0.3	524	0.5	0.0	0.3	460	0.5	0.0	0.4	365	0.7	0.0	12.0	18	16.6	0.0
12/1/09 4:30	1.7	599	3.1	0.1	0.5	523	0.9	0.0	0.3	458	0.5	0.0	0.5	361	0.9	0.0	14.0	18	19.6	0.0
12/1/09 5:00	1.7	599	3.1	0.1	0.5	523	0.9	0.0	0.3	458	0.5	0.0	0.4	361	0.7	0.0	12.0	18	16.6	0.0
12/1/09 5:30	3.4	593	6.3	0.2	0.3	519	0.5	0.0	0.3	456	0.5	0.0	0.6	361	1.1	0.0	14.0	18	19.6	0.0
12/1/09 6:00	2.1	593	3.9	0.1	0.6	517	1.1	0.0	0.3	454	0.5	0.0	0.4	358	0.7	0.0	14.0	18	19.6	0.0
12/1/09 6:30	1.8	588	3.3	0.1	0.4	514	0.7	0.0	0.3	451	0.5	0.0	0.4	358	0.7	0.0	11.0	18	15.2	0.0
12/1/09 7:00	1.7	582	3.1	0.1	0.3	510	0.5	0.0	0.5	449	0.9	0.0	0.3	358	0.5	0.0	12.0	18	16.6	0.0
12/1/09 7:30	1.7	588	3.1	0.1	0.6	512	1.1	0.0	0.3	449	0.5	0.0	0.4	354	0.7	0.0	12.0	18	16.6	0.0
12/1/09 8:00	1.7	582	3.1	0.1	0.3	509	0.5	0.0	0.4	447	0.7	0.0	0.5	354	0.9	0.0	14.0	18	19.6	0.0
12/1/09 8:30	1.5	576	2.7	0.1	0.3	504	0.5	0.0	0.4	442	0.7	0.0	0.4	351	0.7	0.0	12.0	18	16.6	0.0
12/1/09 9:00	1.6	576	2.9	0.1	0.4	504	0.7	0.0	0.3	442	0.5	0.0	0.4	351	0.7	0.0	13.0	18	18.1	0.0
12/1/09 9:30	1.7	570	3.1	0.1	0.4	500	0.7	0.0	0.3	440	0.5	0.0	0.4	351	0.7	0.0	12.0	18	16.6	0.0
12/1/09 10:00	1.7	570	3.1	0.1	0.3	499	0.5	0.0	0.6	438	1.1	0.0	0.4	347	0.7	0.0	13.0	18	18.1	0.0
12/1/09 10:30	1.7	570	3.1	0.1	0.3	499	0.5	0.0	0.4	438	0.7	0.0	0.5	347	0.9	0.0	14.0	18	19.6	0.0
12/1/09 11:00	1.7	565	3.1	0.1	0.3	494	0.5	0.0	0.3	434	0.5	0.0	0.4	344	0.7	0.0	12.0	17	16.6	0.0
12/1/09 11:30	1.8	570	3.3	0.1	0.5	497	0.9	0.0	0.6	436	1.1	0.0	0.4	344	0.7	0.0	12.0	17	16.6	0.0
12/1/09 12:00	1.6	570	2.9	0.1	0.4	496	0.7	0.0	0.3	434	0.5	0.0	0.4	341	0.7	0.0	13.0	17	18.1	0.0
12/1/09 12:30	1.7	565	3.1	0.1	0.4	493	0.7	0.0	0.3	432	0.5	0.0	0.4	341	0.7	0.0	14.0	17	19.6	0.0
12/1/09 13:00	1.6	565	2.9	0.1	0.3	493	0.5	0.0	0.3	432	0.5	0.0	0.4	341	0.7	0.0	14.0	17	19.6	0.0
12/1/09 13:30	1.8	565	3.3	0.1	0.3	491	0.5	0.0	0.3	430	0.5	0.0	0.3	337	0.5	0.0	12.0	17	16.6	0.0
12/1/09 14:00	1.5	559	2.7	0.1	0.3	488	0.5	0.0	0.4	428	0.7	0.0	0.4	337	0.7	0.0	13.0	17	18.1	0.0
12/1/09 14:30	1.8	559	3.3	0.1	0.3	487	0.5	0.0	0.3	426	0.5	0.0	0.4	334	0.7	0.0	11.0	17	15.2	0.0
12/1/09 15:00	2.0	559	3.7	0.1	0.4	488	0.7	0.0	0.4	428	0.7	0.0	1.1	337	2.0	0.0	14.0	17	19.6	0.0
12/1/09 15:30	1.5	553	2.7	0.1	0.3	483	0.5	0.0	0.3	423	0.5	0.0	0.4	334	0.7	0.0	11.0	17	15.2	0.0
12/1/09 16:00	1.8	548	3.3	0.1	0.3	479	0.5	0.0	0.4	421	0.7	0.0	0.3	334	0.5	0.0	11.0	17	15.2	0.0
12/1/09 16:30	1.8	553	3.3	0.1	0.3	482	0.5	0.0	0.3	421	0.5	0.0	0.4	331	0.7	0.0	12.0	17	16.6	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/1/09 17:00	1.5	548	2.7	0.1	0.3	478	0.5	0.0	0.3	419	0.5	0.0	0.6	331	1.1	0.0	11.0	17	15.2	0.0
12/1/09 17:30	1.5	548	2.7	0.1	0.3	478	0.5	0.0	0.4	419	0.7	0.0	0.4	331	0.7	0.0	11.0	17	15.2	0.0
12/1/09 18:00	1.8	542	3.3	0.1	0.4	473	0.7	0.0	0.4	415	0.7	0.0	0.4	327	0.7	0.0	12.0	17	16.6	0.0
12/1/09 18:30	1.6	542	2.9	0.1	0.4	473	0.7	0.0	0.4	415	0.7	0.0	0.7	327	1.3	0.0	11.0	17	15.2	0.0
12/1/09 19:00	1.6	553	2.9	0.1	0.4	481	0.7	0.0	0.6	419	1.1	0.0	0.4	327	0.7	0.0	11.0	17	15.2	0.0
12/1/09 19:30	1.4	542	2.6	0.1	0.3	472	0.5	0.0	0.4	413	0.7	0.0	0.4	324	0.7	0.0	11.0	17	15.2	0.0
12/1/09 20:00	1.7	531	3.1	0.1	0.3	465	0.5	0.0	0.4	408	0.7	0.0	0.3	324	0.5	0.0	10.0	17	13.7	0.0
12/1/09 20:30	1.5	531	2.7	0.1	0.3	464	0.5	0.0	0.3	407	0.5	0.0	0.3	321	0.5	0.0	12.0	16	16.6	0.0
12/1/09 21:00	1.8	537	3.3	0.1	0.1	467	0.2	0.0	0.4	409	0.7	0.0	0.4	321	0.7	0.0	11.0	16	15.2	0.0
12/1/09 21:30	1.7	531	3.1	0.1	0.2	463	0.4	0.0	0.3	405	0.5	0.0	0.3	318	0.5	0.0	11.0	16	15.2	0.0
12/1/09 22:00	1.7	537	3.1	0.1	0.3	466	0.5	0.0	0.4	407	0.7	0.0	0.4	318	0.7	0.0	13.0	16	18.1	0.0
12/1/09 22:30	1.5	526	2.7	0.1	0.3	459	0.5	0.0	0.4	402	0.7	0.0	0.4	318	0.7	0.0	11.0	16	15.2	0.0
12/1/09 23:00	1.7	526	3.1	0.1	0.2	459	0.4	0.0	0.4	402	0.7	0.0	0.3	318	0.5	0.0	11.0	16	15.2	0.0
12/1/09 23:30	1.5	521	2.7	0.1	0.9	454	1.6	0.0	0.4	398	0.7	0.0	0.4	314	0.7	0.0	13.0	16	18.1	0.0
12/2/09 0:00	1.9	521	3.5	0.1	0.3	454	0.5	0.0	0.3	398	0.5	0.0	0.5	314	0.9	0.0	12.0	16	16.6	0.0
12/2/09 0:30	1.8	526	3.3	0.1	0.3	457	0.5	0.0	0.3	399	0.5	0.0	0.4	311	0.7	0.0	19.0	16	27.1	0.0
12/2/09 1:00	1.7	521	3.1	0.1	0.4	453	0.7	0.0	0.3	396	0.5	0.0	0.4	311	0.7	0.0	13.0	16	18.1	0.0
12/2/09 1:30	1.9	521	3.5	0.1	0.2	452	0.4	0.0	0.3	395	0.5	0.0	0.4	308	0.7	0.0	13.0	16	18.1	0.0
12/2/09 2:00	2.0	510	3.7	0.1	0.3	445	0.5	0.0	0.4	390	0.7	0.0	0.4	308	0.7	0.0	13.0	16	18.1	0.0
12/2/09 2:30	1.7	515	3.1	0.1	0.3	448	0.5	0.0	0.4	392	0.7	0.0	0.3	308	0.5	0.0	18.0	16	25.6	0.0
12/2/09 3:00	1.8	515	3.3	0.1	0.3	448	0.5	0.0	0.3	392	0.5	0.0	0.3	308	0.5	0.0	15.0	16	21.1	0.0
12/2/09 3:30	1.8	510	3.3	0.1	0.2	444	0.4	0.0	0.4	388	0.7	0.0	0.3	305	0.5	0.0	15.0	16	21.1	0.0
12/2/09 4:00	1.8	504	3.3	0.1	0.3	440	0.5	0.0	0.3	386	0.5	0.0	0.3	305	0.5	0.0	17.0	16	24.1	0.0
12/2/09 4:30	1.8	510	3.3	0.1	0.2	444	0.4	0.0	0.4	388	0.7	0.0	0.4	305	0.7	0.0	13.0	16	18.1	0.0
12/2/09 5:00	1.6	510	2.9	0.1	0.3	444	0.5	0.0	0.4	388	0.7	0.0	0.4	305	0.7	0.0	14.0	16	19.6	0.0
12/2/09 5:30	1.7	504	3.1	0.1	0.3	438	0.5	0.0	0.3	382	0.5	0.0	0.4	299	0.7	0.0	17.0	15	24.1	0.0
12/2/09 6:00	1.8	499	3.3	0.1	0.4	436	0.7	0.0	0.3	382	0.5	0.0	0.4	302	0.7	0.0	16.0	15	22.6	0.0
12/2/09 6:30	1.6	499	2.9	0.1	0.4	435	0.7	0.0	0.3	380	0.5	0.0	0.4	299	0.7	0.0	14.0	15	19.6	0.0
12/2/09 7:00	1.7	499	3.1	0.1	0.3	435	0.5	0.0	0.3	380	0.5	0.0	0.4	299	0.7	0.0	16.0	15	22.6	0.0
12/2/09 7:30	1.9	499	3.5	0.1	0.5	435	0.9	0.0	0.4	380	0.7	0.0	0.4	299	0.7	0.0	17.0	15	24.1	0.0
12/2/09 8:00	1.5	499	2.7	0.1	0.4	434	0.7	0.0	0.4	378	0.7	0.0	0.5	296	0.9	0.0	16.0	15	22.6	0.0
12/2/09 8:30	1.9	494	3.5	0.1	0.3	430	0.5	0.0	0.4	376	0.7	0.0	0.4	296	0.7	0.0	15.0	15	21.1	0.0
12/2/09 9:00	1.5	489	2.7	0.1	0.2	427	0.4	0.0	0.3	374	0.5	0.0	0.6	296	1.1	0.0	17.0	15	24.1	0.0
12/2/09 9:30	1.7	489	3.1	0.1	0.3	427	0.5	0.0	0.3	374	0.5	0.0	0.4	296	0.7	0.0	16.0	15	22.6	0.0
12/2/09 10:00	1.8	484	3.3	0.1	0.2	422	0.4	0.0	0.3	370	0.5	0.0	0.4	293	0.7	0.0	17.0	15	24.1	0.0
12/2/09 10:30	1.7	489	3.1	0.1	0.4	426	0.7	0.0	0.4	372	0.7	0.0	0.3	293	0.5	0.0	15.0	15	21.1	0.0
12/2/09 11:00	1.9	484	3.5	0.1	0.2	421	0.4	0.0	0.3	368	0.5	0.0	0.3	290	0.5	0.0	19.0	15	27.1	0.0
12/2/09 11:30	1.7	489	3.1	0.1	0.3	426	0.5	0.0	0.4	372	0.7	0.0	0.4	293	0.7	0.0	17.0	15	24.1	0.0
12/2/09 12:00	1.9	484	3.5	0.1	0.3	421	0.5	0.0	0.3	368	0.5	0.0	0.4	290	0.7	0.0	17.0	15	24.1	0.0
12/2/09 12:30	1.5	478	2.7	0.1	0.3	418	0.5	0.0	0.3	366	0.5	0.0	0.4	290	0.7	0.0	17.0	15	24.1	0.0
12/2/09 13:00	1.5	478	2.7	0.1	0.2	418	0.4	0.0	0.6	366	1.1	0.0	0.3	290	0.5	0.0	17.0	15	24.1	0.0
12/2/09 13:30	1.5	478	2.7	0.1	0.1	417	0.2	0.0	0.4	365	0.7	0.0	0.4	286	0.7	0.0	18.0	15	25.6	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/2/09 14:00	1.7	484	3.1	0.1	0.3	420	0.5	0.0	0.3	367	0.5	0.0	0.3	286	0.5	0.0	18.0	15	25.6	0.0
12/2/09 14:30	1.6	478	2.9	0.1	0.2	417	0.4	0.0	0.3	365	0.5	0.0	0.4	286	0.7	0.0	18.0	15	25.6	0.0
12/2/09 15:00	1.6	473	2.9	0.1	0.2	412	0.4	0.0	0.3	361	0.5	0.0	0.4	283	0.7	0.0	17.0	15	24.1	0.0
12/2/09 15:30	1.6	473	2.9	0.1	0.1	412	0.2	0.0	0.3	361	0.5	0.0	1.1	283	2.0	0.0	17.0	15	24.1	0.0
12/2/09 16:00	1.6	468	2.9	0.1	0.3	409	0.5	0.0	0.3	359	0.5	0.0	0.4	283	0.7	0.0	18.0	15	25.6	0.0
12/2/09 16:30	1.6	468	2.9	0.1	0.2	409	0.4	0.0	0.3	359	0.5	0.0	0.3	283	0.5	0.0	19.0	15	27.1	0.0
12/2/09 17:00	1.6	468	2.9	0.1	0.2	408	0.4	0.0	0.4	357	0.5	0.0	0.4	280	0.7	0.0	18.0	14	25.6	0.0
12/2/09 17:30	1.7	463	3.1	0.1	0.1	404	0.2	0.0	0.4	355	0.7	0.0	0.3	280	0.5	0.0	17.0	14	24.1	0.0
12/2/09 18:00	1.7	473	3.1	0.1	0.3	410	0.5	0.0	0.3	357	0.5	0.0	0.5	277	0.9	0.0	19.0	14	27.1	0.0
12/2/09 18:30	1.8	463	3.3	0.1	0.2	403	0.4	0.0	0.3	353	0.5	0.0	0.4	277	0.7	0.0	18.0	14	25.6	0.0
12/2/09 19:00	1.6	468	2.9	0.1	0.2	407	0.4	0.0	0.3	355	0.5	0.0	0.4	277	0.7	0.0	18.0	14	25.6	0.0
12/2/09 19:30	1.4	468	2.6	0.1	0.4	406	0.7	0.0	0.4	353	0.7	0.0	0.5	275	0.9	0.0	18.0	14	25.6	0.0
12/2/09 20:00	1.7	458	3.1	0.1	0.3	399	0.5	0.0	0.4	349	0.7	0.0	0.5	275	0.9	0.0	19.0	14	27.1	0.0
12/2/09 20:30	1.7	453	3.1	0.1	0.3	396	0.5	0.0	0.3	347	0.5	0.0	0.5	275	0.9	0.0	19.0	14	27.1	0.0
12/2/09 21:00	1.5	458	2.7	0.1	0.2	399	0.4	0.0	0.3	349	0.5	0.0	0.4	275	0.7	0.0	18.0	14	25.6	0.0
12/2/09 21:30	1.6	453	2.9	0.1	0.2	395	0.4	0.0	0.3	345	0.5	0.0	0.3	272	0.5	0.0	18.0	14	25.6	0.0
12/2/09 22:00	2.2	453	4.0	0.1	0.2	395	0.4	0.0	0.4	345	0.7	0.0	0.4	272	0.7	0.0	19.0	14	27.1	0.0
12/2/09 22:30	1.6	453	2.9	0.1	0.2	395	0.4	0.0	0.3	345	0.5	0.0	0.4	272	0.7	0.0	18.0	14	25.6	0.0
12/2/09 23:00	1.5	453	2.7	0.1	0.2	394	0.4	0.0	0.3	344	0.5	0.0	0.4	269	0.7	0.0	18.0	14	25.6	0.0
12/2/09 23:30	1.6	443	2.9	0.1	0.2	387	0.4	0.0	0.3	340	0.5	0.0	0.3	269	0.5	0.0	24.0	14	34.8	0.0
12/3/09 0:00	1.5	448	2.7	0.1	0.2	389	0.4	0.0	0.4	340	0.7	0.0	0.3	266	0.5	0.0	19.0	14	27.1	0.0
12/3/09 1:00	1.8	443	3.3	0.1	0.2	386	0.4	0.0	0.3	338	0.5	0.0	0.3	266	0.5	0.0	26.0	14	37.8	0.0
12/3/09 1:30	1.6	443	2.9	0.1	0.2	386	0.4	0.0	0.4	338	0.7	0.0	0.4	266	0.7	0.0	18.0	14	25.6	0.0
12/3/09 2:00	1.6	438	2.9	0.1	0.2	383	0.4	0.0	0.4	336	0.7	0.0	0.4	266	0.7	0.0	21.0	14	30.2	0.0
12/3/09 2:30	1.7	438	3.1	0.1	0.2	382	0.4	0.0	0.4	334	0.7	0.0	0.3	263	0.5	0.0	18.0	14	25.6	0.0
12/3/09 3:00	1.7	438	3.1	0.1	0.2	382	0.4	0.0	0.3	334	0.5	0.0	0.6	263	1.0	0.0	18.0	14	25.6	0.0
12/3/09 3:30	1.6	438	2.9	0.1	0.7	381	1.3	0.0	0.3	333	0.5	0.0	0.3	260	0.5	0.0	22.0	13	31.7	0.0
12/3/09 4:00	3.7	438	6.9	0.2	0.6	382	1.1	0.0	0.3	334	0.5	0.0	0.4	263	0.7	0.0	15.0	14	21.1	0.0
12/3/09 4:30	1.5	433	2.7	0.1	0.3	378	0.5	0.0	0.4	331	0.7	0.0	0.4	260	0.7	0.0	17.0	13	24.1	0.0
12/3/09 5:00	1.7	433	3.1	0.1	0.3	378	0.5	0.0	0.4	331	0.7	0.0	0.4	260	0.7	0.0	19.0	13	27.1	0.0
12/3/09 5:30	1.5	429	2.7	0.1	1.7	373	3.1	0.1	0.3	327	0.5	0.0	0.5	257	0.9	0.0	19.0	13	27.1	0.0
12/3/09 6:00	1.8	433	3.3	0.1	0.2	377	0.4	0.0	0.3	329	0.5	0.0	0.3	257	0.5	0.0	19.0	13	27.1	0.0
12/3/09 6:30	1.8	429	3.3	0.1	0.4	373	0.7	0.0	0.4	327	0.7	0.0	0.4	257	0.7	0.0	18.0	13	25.6	0.0
12/3/09 7:00	2.4	429	4.4	0.1	0.2	373	0.4	0.0	0.3	325	0.5	0.0	0.3	254	0.5	0.0	24.0	13	34.8	0.0
12/3/09 7:30	1.7	429	3.1	0.1	0.2	373	0.4	0.0	0.3	325	0.5	0.0	0.4	254	0.7	0.0	18.0	13	25.6	0.0
12/3/09 8:00	1.6	424	2.9	0.1	0.3	369	0.5	0.0	0.3	323	0.5	0.0	0.5	254	0.9	0.0	20.0	13	28.6	0.0
12/3/09 8:30	1.7	424	3.1	0.1	0.2	369	0.4	0.0	0.6	323	1.1	0.0	0.3	254	0.5	0.0	19.0	13	27.1	0.0
12/3/09 9:00	1.6	419	2.9	0.1	0.6	365	1.1	0.0	0.3	320	0.5	0.0	0.3	252	0.5	0.0	19.0	13	27.1	0.0
12/3/09 9:30	1.6	419	2.9	0.1	0.3	365	0.5	0.0	0.4	320	0.7	0.0	0.3	252	0.5	0.0	20.0	13	28.6	0.0
12/3/09 10:00	1.6	419	2.9	0.1	0.1	365	0.2	0.0	0.3	320	0.5	0.0	0.3	252	0.5	0.0	35.0	13	51.9	0.0
12/3/09 10:30	1.6	419	2.9	0.1	0.2	365	0.4	0.0	0.3	320	0.5	0.0	0.3	252	0.5	0.0	27.0	13	39.4	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/3/09 11:00	1.4	419	2.6	0.1	0.2	364	0.4	0.0	0.3	318	0.5	0.0	0.3	249	0.5	0.0	27.0	13	39.4	0.0
12/3/09 11:30	1.5	414	2.7	0.1	0.3	361	0.5	0.0	0.3	316	0.5	0.0	0.3	249	0.5	0.0	21.0	13	30.2	0.0
12/3/09 12:00	1.5	410	2.7	0.1	0.1	358	0.2	0.0	0.3	314	0.5	0.0	0.3	249	0.5	0.0	30.0	13	44.0	0.0
12/3/09 12:30	1.5	414	2.7	0.1	0.2	360	0.4	0.0	0.2	314	0.4	0.0	0.4	246	0.7	0.0	35.0	13	51.9	0.0
12/3/09 13:00	1.7	410	3.1	0.1	2.4	357	4.4	0.1	0.3	313	0.5	0.0	0.3	246	0.5	0.0	21.0	13	30.2	0.0
12/3/09 13:30	1.5	410	2.7	0.1	0.2	357	0.4	0.0	0.3	313	0.5	0.0	0.3	246	0.5	0.0	23.0	13	33.2	0.0
12/3/09 14:00	1.6	410	2.9	0.1	0.1	357	0.2	0.0	0.3	313	0.5	0.0	0.4	246	0.7	0.0	22.0	13	31.7	0.0
12/3/09 14:30	1.5	410	2.7	0.1	0.2	357	0.4	0.0	0.3	313	0.5	0.0	0.3	246	0.5	0.0	27.0	13	39.4	0.0
12/3/09 15:00	1.6	405	2.9	0.1	0.3	354	0.5	0.0	0.4	311	0.7	0.0	0.4	246	0.7	0.0	35.0	13	51.9	0.0
12/3/09 15:30	1.5	405	2.7	0.1	0.1	353	0.2	0.0	0.3	309	0.5	0.0	0.5	243	0.9	0.0	20.0	13	28.6	0.0
12/3/09 16:00	1.4	400	2.6	0.1	0.2	350	0.4	0.0	0.5	307	0.9	0.0	0.5	243	0.9	0.0	24.0	13	34.8	0.0
12/3/09 16:30	1.6	405	2.9	0.1	0.1	353	0.2	0.0	0.3	309	0.5	0.0	0.4	243	0.7	0.0	22.0	13	31.7	0.0
12/3/09 17:00	1.6	400	2.9	0.1	0.2	350	0.4	0.0	0.3	307	0.5	0.0	0.3	243	0.5	0.0	26.0	13	37.8	0.0
12/3/09 17:30	1.4	400	2.6	0.1	0.2	350	0.4	0.0	0.2	307	0.4	0.0	0.3	243	0.5	0.0	28.0	13	40.9	0.0
12/3/09 18:00	1.6	400	2.9	0.1	0.1	349	0.2	0.0	0.2	306	0.4	0.0	0.3	241	0.5	0.0	22.0	12	31.7	0.0
12/3/09 18:30	1.5	400	2.7	0.1	0.2	349	0.4	0.0	0.3	306	0.5	0.0	0.3	241	0.5	0.0	23.0	12	33.2	0.0
12/3/09 19:00	1.4	396	2.6	0.1	0.1	346	0.2	0.0	0.4	304	0.7	0.0	0.3	241	0.5	0.0	24.0	12	34.8	0.0
12/3/09 19:30	1.6	396	2.9	0.1	0.2	346	0.4	0.0	0.3	304	0.5	0.0	0.4	241	0.7	0.0	23.0	12	33.2	0.0
12/3/09 20:00	1.6	396	2.9	0.1	0.1	346	0.2	0.0	0.3	304	0.5	0.0	0.4	241	0.7	0.0	36.0	12	53.5	0.0
12/3/09 20:30	1.5	396	2.7	0.1	0.3	345	0.5	0.0	0.3	302	0.5	0.0	0.4	238	0.7	0.0	21.0	12	30.2	0.0
12/3/09 21:00	1.4	391	2.6	0.1	0.2	342	0.4	0.0	0.5	300	0.9	0.0	0.4	238	0.7	0.0	22.0	12	31.7	0.0
12/3/09 21:30	1.4	387	2.6	0.1	0.1	339	0.2	0.0	0.3	298	0.5	0.0	0.3	238	0.5	0.0	21.0	12	30.2	0.0
12/3/09 22:00	1.6	387	2.9	0.1	0.2	338	0.4	0.0	0.4	297	0.7	0.0	0.4	235	0.7	0.0	23.0	12	33.2	0.0
12/3/09 22:30	1.4	391	2.6	0.1	0.1	341	0.2	0.0	0.3	299	0.5	0.0	0.3	235	0.5	0.0	26.0	12	37.8	0.0
12/3/09 23:00	1.5	387	2.7	0.1	0.1	338	0.7	0.0	0.3	297	0.5	0.0	0.4	235	0.7	0.0	26.0	12	37.8	0.0
12/3/09 23:30	2.0	387	3.7	0.1	0.2	338	0.4	0.0	0.3	297	0.5	0.0	0.3	235	0.5	0.0	27.0	12	39.4	0.0
12/4/09 0:00	1.5	387	2.7	0.1	0.1	337	0.2	0.0	0.3	295	0.5	0.0	0.3	232	0.5	0.0	25.0	12	36.3	0.0
12/4/09 0:30	1.4	382	2.6	0.1	0.3	334	0.5	0.0	0.3	293	0.5	0.0	0.9	232	1.6	0.0	22.0	12	31.7	0.0
12/4/09 1:00	1.4	382	2.6	0.1	0.3	334	0.5	0.0	0.3	293	0.5	0.0	0.3	232	0.5	0.0	24.0	12	34.8	0.0
12/4/09 1:30	1.5	382	2.7	0.1	0.1	334	0.2	0.0	0.3	293	0.5	0.0	0.3	232	0.5	0.0	30.0	12	44.0	0.0
12/4/09 2:00	1.3	382	2.4	0.1	0.2	333	0.4	0.0	0.3	292	0.5	0.0	0.3	230	0.5	0.0	37.0	12	55.0	0.0
12/4/09 2:30	2.0	378	3.7	0.1	0.4	330	0.7	0.0	0.3	290	0.5	0.0	0.3	230	0.5	0.0	32.0	12	47.2	0.0
12/4/09 3:00	1.5	378	2.7	0.1	0.1	330	0.2	0.0	0.3	290	0.5	0.0	0.3	230	0.5	0.0	25.0	12	36.3	0.0
12/4/09 3:30	1.4	374	2.6	0.1	0.2	328	0.4	0.0	0.3	288	0.5	0.0	0.3	230	0.5	0.0	29.0	12	42.5	0.0
12/4/09 4:00	1.6	378	2.9	0.1	0.1	329	0.2	0.0	0.3	288	0.5	0.0	0.3	227	0.5	0.0	26.0	12	37.8	0.0
12/4/09 4:30	1.4	378	2.6	0.1	0.2	329	0.4	0.0	0.3	288	0.5	0.0	0.3	227	0.5	0.0	29.0	12	42.5	0.0
12/4/09 5:00	1.4	378	2.6	0.1	0.3	329	0.5	0.0	0.4	288	0.7	0.0	0.3	227	0.5	0.0	26.0	12	37.8	0.0
12/4/09 5:30	1.5	374	2.7	0.1	0.3	326	0.5	0.0	0.3	285	0.5	0.0	0.3	225	0.5	0.0	21.0	12	30.2	0.0
12/4/09 6:00	1.4	370	2.6	0.1	0.2	324	0.4	0.0	0.3	285	0.5	0.0	0.3	227	0.5	0.0	24.0	12	34.8	0.0
12/4/09 6:30	1.4	370	2.6	0.1	0.1	323	0.2	0.0	0.3	284	0.5	0.0	0.4	225	0.7	0.0	23.0	12	33.2	0.0
12/4/09 7:00	1.4	366	2.6	0.1	0.1	320	0.2	0.0	0.4	282	0.7	0.0	0.3	225	0.5	0.0	23.0	12	33.2	0.0
12/4/09 7:30	1.3	370	2.4	0.0	0.1	323	0.2	0.0	0.3	284	0.5	0.0	0.3	225	0.5	0.0	26.0	12	37.8	0.0

Date & Time	Station 1					Station 2					Station 3					Station 4					Station 5				
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)		Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)		Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)		Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)		Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	
12/4/09 8:00	1.7	370	3.1	0.1		0.1	322	0.2	0.0		0.3	282	0.5	0.0		0.4	222	0.7	0.0		20.0	12	28.6	0.0	
12/4/09 8:30	1.4	370	2.6	0.1		1.0	323	1.8	0.0		0.3	284	0.5	0.0		0.4	225	0.7	0.0		19.0	12	27.1	0.0	
12/4/09 9:00	1.4	366	2.6	0.1		0.2	320	0.4	0.0		0.3	281	0.5	0.0		0.3	222	0.5	0.0		24.0	12	34.8	0.0	
12/4/09 9:30	1.5	366	2.7	0.1		0.2	320	0.4	0.0		0.3	281	0.5	0.0		0.4	222	0.7	0.0		21.0	12	30.2	0.0	
12/4/09 10:00	3.2	366	5.9	0.1		0.2	319	0.4	0.0		0.3	279	0.5	0.0		0.3	219	0.5	0.0		21.0	11	30.2	0.0	
12/4/09 10:30	1.5	362	2.7	0.1		0.1	316	0.2	0.0		0.3	277	0.5	0.0		0.4	219	0.7	0.0		18.0	11	25.6	0.0	
12/4/09 11:00	1.5	362	2.7	0.1		0.1	316	0.2	0.0		0.3	277	0.5	0.0		0.4	219	0.7	0.0		21.0	11	30.2	0.0	
12/4/09 11:30	1.5	362	2.7	0.1		0.1	316	0.2	0.0		0.3	277	0.5	0.0		0.3	219	0.5	0.0		21.0	11	30.2	0.0	
12/4/09 12:00	1.5	362	2.7	0.1		0.1	316	0.2	0.0		0.3	277	0.5	0.0		0.3	219	0.5	0.0		29.0	11	42.5	0.0	
12/4/09 12:30	1.4	362	2.6	0.1		0.1	315	0.2	0.0		0.3	276	0.5	0.0		0.3	217	0.5	0.0		31.0	11	45.6	0.0	
12/4/09 13:00	1.2	358	2.2	0.0		0.2	313	0.4	0.0		0.3	274	0.5	0.0		0.3	217	0.5	0.0		32.0	11	47.2	0.0	
12/4/09 13:30	1.5	358	2.7	0.1		0.1	313	0.2	0.0		0.3	274	0.5	0.0		0.3	217	0.5	0.0		31.0	11	45.6	0.0	
12/4/09 14:00	1.5	358	2.7	0.1		0.1	313	0.2	0.0		0.3	274	0.5	0.0		0.3	217	0.5	0.0		26.0	11	37.8	0.0	
12/4/09 14:30	1.6	358	2.9	0.1		0.1	313	0.2	0.0		0.3	274	0.5	0.0		0.4	217	0.7	0.0		26.0	11	37.8	0.0	
12/4/09 15:00	1.4	354	2.6	0.1		0.1	310	0.2	0.0		0.3	273	0.5	0.0		0.3	217	0.5	0.0		22.0	11	31.7	0.0	
12/4/09 15:30	1.4	354	2.6	0.1		0.1	309	0.2	0.0		0.3	271	0.5	0.0		0.4	214	0.7	0.0		26.0	11	37.8	0.0	
12/4/09 16:00	1.4	354	2.6	0.1		0.1	309	0.2	0.0		0.3	271	0.5	0.0		0.3	214	0.5	0.0		37.0	11	55.0	0.0	
12/4/09 16:30	1.5	354	2.7	0.1		0.1	309	0.2	0.0		0.4	271	0.7	0.0		0.3	214	0.5	0.0		26.0	11	37.8	0.0	
12/4/09 17:00	1.4	354	2.7	0.1		0.2	309	0.4	0.0		0.3	271	0.5	0.0		0.3	214	0.5	0.0		26.0	11	37.8	0.0	
12/4/09 17:30	1.5	354	2.7	0.1		0.1	309	0.4	0.0		0.3	271	0.5	0.0		0.3	214	0.5	0.0		22.0	11	31.7	0.0	
12/4/09 18:00	1.5	351	2.7	0.1		0.2	306	0.4	0.0		0.3	268	0.5	0.0		0.3	212	0.5	0.0		27.0	11	39.4	0.0	
12/4/09 18:30	1.5	351	2.7	0.1		0.2	306	0.4	0.0		0.4	268	0.7	0.0		0.4	212	0.7	0.0		25.0	11	36.3	0.0	
12/4/09 19:00	1.6	351	2.9	0.1		0.1	306	0.2	0.0		0.3	268	0.5	0.0		0.3	212	0.5	0.0		21.0	11	30.2	0.0	
12/4/09 19:30	1.4	351	2.6	0.1		0.1	306	0.2	0.0		0.3	268	0.5	0.0		0.3	212	0.5	0.0		24.0	11	34.8	0.0	
12/4/09 20:00	1.6	347	2.9	0.1		0.1	302	0.2	0.0		0.2	265	0.4	0.0		0.3	209	0.5	0.0		22.0	11	31.7	0.0	
12/4/09 20:30	1.4	347	2.6	0.0		0.7	303	1.3	0.0		0.3	267	0.5	0.0		0.3	212	0.5	0.0		22.0	11	31.7	0.0	
12/4/09 21:00	1.6	347	2.9	0.1		0.1	302	0.2	0.0		0.3	265	0.5	0.0		0.4	209	0.7	0.0		23.0	11	33.2	0.0	
12/4/09 21:30	1.6	347	2.9	0.1		0.1	302	0.2	0.0		0.3	265	0.5	0.0		0.5	209	0.9	0.0		31.0	11	45.6	0.0	
12/4/09 22:00	1.5	347	2.7	0.1		0.1	302	0.2	0.0		0.2	265	0.4	0.0		0.4	209	0.7	0.0		56.0	11	88.5	0.1	
12/4/09 22:30	1.4	343	2.6	0.0		0.1	300	0.2	0.0		0.3	264	0.5	0.0		0.3	209	0.5	0.0		35.0	11	51.9	0.0	
12/4/09 23:00	1.5	347	2.7	0.1		0.1	302	0.2	0.0		0.3	265	0.5	0.0		0.4	209	0.7	0.0		23.0	11	33.2	0.0	
12/4/09 23:30	1.4	343	2.6	0.0		0.1	299	0.2	0.0		0.3	262	0.5	0.0		0.3	207	0.5	0.0		25.0	11	36.3	0.0	
12/5/09 0:00	1.8	343	3.3	0.1		0.2	299	0.4	0.0		0.3	262	0.5	0.0		0.3	207	0.5	0.0		34.0	11	50.3	0.0	
12/5/09 0:30	1.7	343	3.1	0.1		0.2	299	0.4	0.0		0.3	262	0.5	0.0		0.4	207	0.7	0.0		28.0	11	40.9	0.0	
12/5/09 1:00	1.5	343	2.7	0.1		0.2	299	0.4	0.0		0.2	262	0.4	0.0		0.3	207	0.5	0.0		28.0	11	40.9	0.0	
12/5/09 1:30	1.4	343	2.6	0.0		0.3	299	0.5	0.0		0.3	262	0.5	0.0		0.3	207	0.5	0.0		37.0	11	55.0	0.0	
12/5/09 2:00	1.3	339	2.4	0.0		0.1	296	0.2	0.0		0.4	259	0.7	0.0		0.3	204	0.5	0.0		29.0	11	42.5	0.0	
12/5/09 2:30	1.5	335	2.7	0.1		0.2	294	0.4	0.0		0.3	259	0.5	0.0		0.4	207	0.7	0.0		27.0	11	39.4	0.0	
12/5/09 3:00	1.7	339	3.1	0.1		0.1	296	0.2	0.0		0.3	259	0.5	0.0		0.4	204	0.7	0.0		35.0	11	51.9	0.0	
12/5/09 3:30	1.4	339	2.6	0.0		0.1	296	0.2	0.0		0.3	259	0.5	0.0		0.3	204	0.5	0.0		31.0	11	45.6	0.0	
12/5/09 4:00	1.4	339	2.6	0.0		0.1	296	0.2	0.0		0.3	259	0.5	0.0		0.3	204	0.5	0.0		24.0	11	34.8	0.0	
12/5/09 4:30	1.4	339	2.6	0.0		0.2	295	0.4	0.0		0.3	258	0.5	0.0		0.3	202	0.5	0.0		31.0	11	45.6	0.0	

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/5/09 5:00	1.4	335	2.6	0.0	0.1	292	0.2	0.0	0.3	256	0.5	0.0	0.4	202	0.7	0.0	32.0	11	47.2	0.0
12/5/09 5:30	1.4	335	2.6	0.0	0.1	292	0.2	0.0	0.2	256	0.4	0.0	0.3	202	0.5	0.0	23.0	11	33.2	0.0
12/5/09 6:00	2.3	335	4.2	0.1	0.1	292	0.2	0.0	0.4	255	0.7	0.0	0.3	199	0.5	0.0	26.0	10	37.8	0.0
12/5/09 6:30	1.4	332	2.6	0.0	0.1	289	0.2	0.0	0.3	253	0.5	0.0	0.3	199	0.5	0.0	26.0	10	37.8	0.0
12/5/09 7:00	1.6	332	2.9	0.1	0.2	289	0.4	0.0	0.4	253	0.7	0.0	0.3	199	0.5	0.0	25.0	10	36.3	0.0
12/5/09 7:30	1.3	332	2.4	0.0	0.1	289	0.2	0.0	0.3	253	0.5	0.0	0.4	199	0.7	0.0	20.0	10	28.6	0.0
12/5/09 8:00	1.6	332	2.9	0.1	0.4	289	0.7	0.0	0.6	253	1.1	0.0	0.3	199	0.5	0.0	23.0	10	33.2	0.0
12/5/09 8:30	1.4	332	2.6	0.0	0.1	289	0.2	0.0	0.3	253	0.5	0.0	0.3	199	0.5	0.0	22.0	10	31.7	0.0
12/5/09 9:00	3.2	328	5.9	0.1	0.1	286	0.2	0.0	0.4	252	0.7	0.0	0.4	199	0.7	0.0	55.0	10	83.9	0.0
12/5/09 9:30	1.4	328	2.6	0.0	0.1	286	0.2	0.0	0.3	250	0.5	0.0	0.3	197	0.5	0.0	46.0	10	69.4	0.0
12/5/09 10:00	1.5	328	2.7	0.1	0.3	286	0.5	0.0	0.3	250	0.5	0.0	0.4	197	0.7	0.0	30.0	10	44.0	0.0
12/5/09 10:30	1.5	328	2.7	0.1	0.1	286	0.2	0.0	0.3	250	0.5	0.0	0.3	197	0.5	0.0	25.0	10	36.3	0.0
12/5/09 11:00	1.5	324	2.7	0.0	0.1	283	0.2	0.0	0.3	249	0.5	0.0	0.4	197	0.7	0.0	29.0	10	42.5	0.0
12/5/09 11:30	1.5	328	2.7	0.1	0.1	285	0.2	0.0	0.2	249	0.4	0.0	0.3	194	0.5	0.0	28.0	10	40.9	0.0
12/5/09 12:00	1.4	324	2.6	0.0	0.1	282	0.2	0.0	0.4	247	0.7	0.0	0.3	194	0.5	0.0	23.0	10	33.2	0.0
12/5/09 12:30	1.5	320	2.7	0.0	0.1	280	0.2	0.0	0.3	246	0.5	0.0	0.3	194	0.5	0.0	16.0	10	22.6	0.0
12/5/09 13:00	1.8	324	3.3	0.1	0.4	282	0.7	0.0	0.3	247	0.5	0.0	0.3	192	0.5	0.0	19.0	10	27.1	0.0
12/5/09 13:30	1.5	320	2.7	0.0	0.5	279	0.9	0.0	0.2	244	0.4	0.0	0.3	192	0.5	0.0	29.0	10	42.5	0.0
12/5/09 14:00	1.4	320	2.6	0.0	0.2	280	0.4	0.0	0.2	246	0.4	0.0	0.3	194	0.5	0.0	26.0	10	37.8	0.0
12/5/09 14:30	1.6	320	2.9	0.1	0.1	279	0.2	0.0	0.3	244	0.5	0.0	0.3	192	0.5	0.0	16.0	10	22.6	0.0
12/5/09 15:00	1.4	320	2.6	0.0	0.2	279	0.4	0.0	0.4	244	0.7	0.0	0.3	192	0.5	0.0	38.0	10	56.6	0.0
12/5/09 15:30	1.3	320	2.4	0.0	0.2	279	0.4	0.0	0.3	244	0.5	0.0	0.3	192	0.5	0.0	26.0	10	37.8	0.0
12/5/09 16:00	1.4	320	2.6	0.0	0.1	279	0.2	0.0	0.3	244	0.5	0.0	0.3	192	0.5	0.0	24.0	10	34.8	0.0
12/5/09 16:30	1.4	317	2.6	0.0	0.1	277	0.2	0.0	0.2	243	0.7	0.0	0.4	190	0.7	0.0	22.0	10	31.7	0.0
12/5/09 17:00	2.0	317	3.7	0.1	0.1	276	0.2	0.0	0.2	241	0.4	0.0	0.3	190	0.5	0.0	18.0	10	25.6	0.0
12/5/09 17:30	1.4	317	2.6	0.0	0.1	276	0.2	0.0	0.3	241	0.5	0.0	0.4	190	0.7	0.0	19.0	10	27.1	0.0
12/5/09 18:00	1.5	313	2.7	0.0	0.1	273	0.2	0.0	0.3	240	0.5	0.0	0.3	190	0.5	0.0	21.0	10	30.2	0.0
12/5/09 18:30	1.3	313	2.4	0.0	0.1	273	0.2	0.0	0.2	240	0.4	0.0	0.3	190	0.5	0.0	22.0	10	31.7	0.0
12/5/09 19:00	1.4	313	2.6	0.0	0.1	273	0.2	0.0	0.2	240	0.4	0.0	0.5	190	0.9	0.0	21.0	10	30.2	0.0
12/5/09 19:30	1.5	313	2.7	0.0	0.1	273	0.2	0.0	0.3	240	0.5	0.0	0.3	187	0.5	0.0	24.0	10	34.8	0.0
12/5/09 20:00	1.4	313	2.6	0.0	0.3	273	0.5	0.0	0.3	239	0.5	0.0	0.3	187	0.5	0.0	25.0	10	36.3	0.0
12/5/09 20:30	1.4	310	2.6	0.0	0.1	270	0.2	0.0	0.3	237	0.4	0.0	0.3	187	0.5	0.0	26.0	10	37.8	0.0
12/5/09 21:00	1.5	310	2.7	0.0	0.1	270	0.2	0.0	0.2	237	0.4	0.0	0.4	187	0.7	0.0	22.0	10	31.7	0.0
12/5/09 21:30	1.5	310	2.7	0.0	0.2	270	0.4	0.0	0.3	237	0.5	0.0	0.3	187	0.5	0.0	16.0	10	22.6	0.0
12/5/09 22:00	1.4	313	2.6	0.0	0.1	273	0.2	0.0	0.3	239	0.5	0.0	0.3	185	0.5	0.0	18.0	10	25.6	0.0
12/5/09 22:30	1.5	310	2.7	0.0	0.1	269	0.2	0.0	0.3	236	0.5	0.0	0.3	185	0.5	0.0	16.0	10	22.6	0.0
12/5/09 23:00	1.5	310	2.7	0.0	0.1	269	0.2	0.0	0.2	236	0.4	0.0	0.3	185	0.5	0.0	22.0	10	31.7	0.0
12/5/09 23:30	1.7	310	3.1	0.1	0.3	269	0.5	0.0	0.3	236	0.5	0.0	0.3	185	0.5	0.0	18.0	10	25.6	0.0
12/6/09 0:00	1.5	306	2.7	0.0	0.2	267	0.4	0.0	0.4	236	0.7	0.0	0.3	185	0.5	0.0	16.0	10	22.6	0.0
12/6/09 0:30	1.4	310	2.6	0.0	0.1	269	0.2	0.0	0.3	234	0.5	0.0	0.4	185	0.7	0.0	17.0	10	24.1	0.0
12/6/09 1:00	1.6	306	2.9	0.1	0.1	267	0.2	0.0	0.3	234	0.5	0.0	0.4	185	0.7	0.0	17.0	10	24.1	0.0
12/6/09 1:30	1.4	306	2.6	0.0	0.1	267	0.2	0.0	0.3	234	0.5	0.0	0.3	185	0.5	0.0				

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/6/09 2:00	1.3	306	2.4	0.0	0.1	266	0.2	0.0	0.3	233	0.5	0.0	0.3	183	0.5	0.0	14.0	10	19.6	0.0
12/6/09 2:30	1.4	306	2.6	0.0	0.1	266	0.2	0.0	0.3	233	0.5	0.0	0.4	183	0.7	0.0	17.0	10	24.1	0.0
12/6/09 3:00	1.4	306	2.6	0.0	0.3	266	0.5	0.0	0.3	233	0.5	0.0	0.4	183	0.7	0.0	22.0	10	31.7	0.0
12/6/09 3:30	1.5	306	2.7	0.0	0.1	266	0.2	0.0	0.3	233	0.5	0.0	0.4	183	0.7	0.0	18.0	10	25.6	0.0
12/6/09 4:00	1.4	306	2.6	0.0	0.1	266	0.2	0.0	0.2	233	0.4	0.0	0.3	183	0.5	0.0	18.0	10	25.6	0.0
12/6/09 4:30	1.4	303	2.6	0.0	0.1	264	0.2	0.0	0.4	231	0.7	0.0	0.6	183	1.1	0.0	14.0	10	19.6	0.0
12/6/09 5:00	1.4	303	2.6	0.0	0.1	263	0.2	0.0	0.4	230	0.7	0.0	0.3	180	0.5	0.0	14.0	10	19.6	0.0
12/6/09 5:30	1.5	299	2.7	0.0	0.1	261	0.2	0.0	0.3	229	0.5	0.0	0.3	180	0.5	0.0	16.0	10	22.6	0.0
12/6/09 6:00	1.5	299	2.7	0.0	0.1	261	0.2	0.0	0.2	229	0.4	0.0	0.3	180	0.5	0.0	16.0	10	22.6	0.0
12/6/09 6:30	1.4	299	2.6	0.0	0.1	261	0.2	0.0	0.3	229	0.5	0.0	0.7	180	1.3	0.0	17.0	10	24.1	0.0
12/6/09 7:00	1.4	299	2.6	0.0	0.1	260	0.2	0.0	0.3	227	0.5	0.0	0.3	178	0.5	0.0	18.0	9	25.6	0.0
12/6/09 7:30	1.5	299	2.7	0.0	0.1	260	0.2	0.0	0.3	227	0.5	0.0	0.3	178	0.5	0.0	16.0	9	22.6	0.0
12/6/09 8:00	3.5	299	6.5	0.1	0.1	260	0.2	0.0	0.3	227	0.5	0.0	0.3	178	0.5	0.0	16.0	9	22.6	0.0
12/6/09 8:30	1.5	299	2.7	0.0	0.1	260	0.2	0.0	0.3	227	0.5	0.0	0.4	178	0.7	0.0	16.0	9	22.6	0.0
12/6/09 9:00	1.6	296	2.9	0.0	0.1	258	0.2	0.0	0.3	226	0.5	0.0	0.3	178	0.5	0.0	21.0	9	30.2	0.0
12/6/09 9:30	1.4	296	2.6	0.0	0.1	258	0.2	0.0	0.3	226	0.5	0.0	0.3	178	0.5	0.0	15.0	9	21.1	0.0
12/6/09 10:00	1.5	296	2.7	0.0	0.1	257	0.2	0.0	0.2	225	0.4	0.0	0.3	176	0.5	0.0	15.0	9	21.1	0.0
12/6/09 10:30	1.5	292	2.7	0.0	0.1	255	0.2	0.0	0.3	224	0.5	0.0	0.3	178	0.5	0.0	17.0	9	24.1	0.0
12/6/09 11:00	1.6	296	2.9	0.0	0.2	257	0.4	0.0	0.3	225	0.5	0.0	0.4	176	0.7	0.0	23.0	9	33.2	0.0
12/6/09 11:30	1.3	296	2.4	0.0	0.1	257	0.2	0.0	0.3	225	0.5	0.0	0.4	176	0.7	0.0	22.0	9	31.7	0.0
12/6/09 12:00	1.4	292	2.6	0.0	0.1	254	0.2	0.0	0.2	222	0.4	0.0	0.3	174	0.5	0.0	18.0	9	25.6	0.0
12/6/09 12:30	2.2	296	4.0	0.1	0.1	257	0.2	0.0	0.3	225	0.5	0.0	0.3	176	0.5	0.0	15.0	9	21.1	0.0
12/6/09 13:00	1.6	292	2.9	0.0	0.1	254	0.2	0.0	0.2	222	0.4	0.0	0.3	174	0.5	0.0	18.0	9	25.6	0.0
12/6/09 13:30	1.4	292	2.6	0.0	0.1	254	0.2	0.0	0.2	222	0.5	0.0	0.4	174	0.7	0.0	10.0	9	13.7	0.0
12/6/09 14:00	1.4	292	2.6	0.0	0.1	254	0.2	0.0	0.2	222	0.4	0.0	0.4	174	0.7	0.0	9.6	9	13.1	0.0
12/6/09 14:30	1.4	289	2.6	0.0	0.1	252	0.2	0.0	0.2	220	0.4	0.0	0.3	174	0.5	0.0	11.0	9	15.2	0.0
12/6/09 15:00	1.3	289	2.4	0.0	0.1	252	0.2	0.0	0.3	220	0.5	0.0	0.3	174	0.5	0.0	12.0	9	16.6	0.0
12/6/09 15:30	1.4	289	2.6	0.0	0.0	251	0.0	0.0	0.3	219	0.5	0.0	0.3	171	0.5	0.0	15.0	9	21.1	0.0
12/6/09 16:00	1.6	289	2.9	0.0	0.1	252	0.2	0.0	0.3	220	0.5	0.0	0.3	174	0.5	0.0	14.0	9	19.6	0.0
12/6/09 16:30	1.4	285	2.6	0.0	0.1	249	0.2	0.0	0.4	218	0.7	0.0	0.3	171	0.5	0.0	24.0	9	34.8	0.0
12/6/09 17:00	1.5	285	2.7	0.0	0.1	249	0.2	0.0	0.3	218	0.5	0.0	0.3	171	0.5	0.0	12.0	9	16.6	0.0
12/6/09 18:00	1.6	285	2.9	0.0	0.1	248	0.2	0.0	0.4	216	0.7	0.0	0.3	169	0.5	0.0	13.0	9	18.1	0.0
12/6/09 18:30	1.5	285	2.7	0.0	0.1	248	0.2	0.0	0.3	216	0.5	0.0	0.3	169	0.5	0.0	7.7	9	10.4	0.0
12/6/09 19:00	1.4	285	2.6	0.0	0.1	247	0.2	0.0	0.3	215	0.5	0.0	0.3	167	0.5	0.0	15.0	9	21.1	0.0
12/6/09 19:30	1.5	282	2.7	0.0	0.1	246	0.2	0.0	0.3	215	0.5	0.0	0.3	169	0.5	0.0	10.0	9	13.7	0.0
12/6/09 20:00	1.4	285	2.6	0.0	0.1	247	0.2	0.0	0.3	215	0.5	0.0	0.3	167	0.5	0.0	11.0	9	15.2	0.0
12/6/09 20:30	1.3	282	2.4	0.0	0.1	245	0.2	0.0	0.2	214	0.4	0.0	0.3	167	0.5	0.0	16.0	9	22.6	0.0
12/6/09 21:00	1.5	282	2.7	0.0	0.1	245	0.2	0.0	0.3	214	0.5	0.0	0.3	167	0.5	0.0	34.0	9	50.3	0.0
12/6/09 21:30	1.4	282	2.6	0.0	0.1	244	0.2	0.0	0.2	212	0.4	0.0	0.4	165	0.7	0.0	35.0	9	51.9	0.0
12/6/09 22:00	1.6	282	2.9	0.0	0.1	245	0.2	0.0	0.3	214	0.5	0.0	0.3	167	0.5	0.0	28.0	9	40.9	0.0
12/6/09 22:30	1.4	279	2.6	0.0	0.1	242	0.2	0.0	0.3	211	0.5	0.0	0.4	165	0.7	0.0	28.0	9	40.9	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/6/09 23:00	1.4	279	2.6	0.0	0.1	242	0.2	0.0	0.3	211	0.5	0.0	0.4	165	0.7	0.0	37.0	9	55.0	0.0
12/6/09 23:30	1.7	279	3.1	0.0	0.1	242	0.2	0.0	0.3	211	0.5	0.0	0.4	165	0.7	0.0	24.0	9	34.8	0.0
12/7/09 0:00	1.6	275	2.9	0.0	0.1	240	0.2	0.0	0.4	210	0.7	0.0	0.4	165	0.7	0.0	10.0	9	13.7	0.0
12/7/09 0:30	1.3	275	2.4	0.0	0.1	239	0.2	0.0	0.3	208	0.5	0.0	0.4	163	0.7	0.0	11.0	9	15.2	0.0
12/7/09 1:00	1.3	275	2.4	0.0	0.3	239	0.5	0.0	0.3	208	0.5	0.0	0.3	163	0.5	0.0	18.0	9	25.6	0.0
12/7/09 1:30	1.4	279	2.6	0.0	0.5	241	0.9	0.0	0.3	210	0.5	0.0	0.3	163	0.5	0.0	12.0	9	16.6	0.0
12/7/09 2:00	1.8	272	3.3	0.1	0.2	236	0.4	0.0	0.3	206	0.5	0.0	0.5	160	0.9	0.0	19.0	9	27.1	0.0
12/7/09 2:30	1.4	272	2.6	0.0	0.2	236	0.4	0.0	0.3	206	0.5	0.0	0.3	160	0.5	0.0	9.9	9	13.6	0.0
12/7/09 3:00	1.5	272	2.7	0.0	0.1	235	0.2	0.0	0.3	205	0.5	0.0	0.3	158	0.5	0.0	16.0	8	22.6	0.0
12/7/09 3:30	1.6	272	2.9	0.0	0.3	235	0.5	0.0	0.3	205	0.5	0.0	0.3	158	0.5	0.0	31.0	8	45.6	0.0
12/7/09 4:00	1.6	272	2.9	0.0	0.2	235	0.4	0.0	0.3	203	0.5	0.0	0.4	156	0.7	0.0	12.0	8	16.6	0.0
12/7/09 4:30	1.5	272	2.7	0.0	0.1	235	0.2	0.0	0.3	203	0.5	0.0	0.3	156	0.5	0.0	10.0	8	13.7	0.0
12/7/09 5:00	1.6	269	2.9	0.0	0.1	232	0.2	0.0	0.3	201	0.5	0.0	0.4	154	0.7	0.0	14.0	8	19.6	0.0
12/7/09 5:30	1.4	269	2.6	0.0	0.1	232	0.2	0.0	0.4	201	0.7	0.0	0.3	154	0.5	0.0	12.0	8	16.6	0.0
12/7/09 6:00	1.5	269	2.7	0.0	0.2	232	0.4	0.0	0.3	201	0.5	0.0	0.4	154	0.7	0.0	7.7	8	10.4	0.0
12/7/09 6:30	1.4	269	2.6	0.0	0.7	231	1.3	0.0	0.3	199	0.5	0.0	0.3	152	0.5	0.0	7.3	8	9.8	0.0
12/7/09 7:00	1.4	269	2.6	0.0	0.1	230	0.2	0.0	0.3	198	0.5	0.0	0.4	150	0.7	0.0	6.4	8	8.5	0.0
12/7/09 7:30	1.6	265	2.9	0.0	0.1	228	0.2	0.0	0.3	196	0.5	0.0	0.3	148	0.5	0.0	4.8	8	6.3	0.0
12/7/09 8:00	1.6	265	2.9	0.0	0.0	227	0.0	0.0	0.3	195	0.5	0.0	0.3	146	0.5	0.0	5.6	8	7.4	0.0
12/7/09 8:30	1.3	265	2.4	0.0	0.2	226	0.4	0.0	0.4	193	0.7	0.0	0.3	144	0.5	0.0	3.9	8	5.0	0.0
12/7/09 9:00	1.4	262	2.6	0.0	0.0	223	0.0	0.0	0.3	191	0.5	0.0	0.3	142	0.5	0.0	5.8	8	7.7	0.0
12/7/09 9:30	1.4	262	2.6	0.0	0.3	223	0.5	0.0	0.3	191	0.5	0.0	0.4	142	0.7	0.0	4.4	8	5.7	0.0
12/7/09 10:00	1.4	262	2.6	0.0	0.1	223	0.2	0.0	0.7	190	1.3	0.0	0.4	140	0.7	0.0	3.9	7	5.0	0.0
12/7/09 10:30	1.5	262	2.7	0.0	0.1	223	0.2	0.0	0.4	190	0.7	0.0	0.4	140	0.7	0.0	4.2	7	5.5	0.0
12/7/09 11:00	1.5	259	2.7	0.0	0.1	220	0.2	0.0	0.3	187	0.5	0.0	0.3	138	0.5	0.0	8.5	7	11.5	0.0
12/7/09 11:30	1.4	256	2.6	0.0	0.0	218	0.0	0.0	0.3	186	0.5	0.0	0.3	138	0.5	0.0	7.0	7	9.4	0.0
12/7/09 12:00	1.5	256	2.7	0.0	0.0	217	0.0	0.0	0.4	185	0.7	0.0	0.3	136	0.5	0.0	5.1	7	6.7	0.0
12/7/09 12:30	1.6	256	2.9	0.0	0.1	217	0.2	0.0	0.6	185	1.1	0.0	0.5	136	0.9	0.0	6.6	7	8.8	0.0
12/7/09 13:00	1.4	256	2.6	0.0	0.3	218	0.5	0.0	0.7	186	1.3	0.0	0.3	138	0.5	0.0	7.0	7	9.4	0.0
12/7/09 13:30	1.6	249	2.9	0.0	0.1	214	0.2	0.0	0.4	184	0.7	0.0	0.3	140	0.5	0.0	5.0	7	6.6	0.0
12/7/09 14:00	1.6	249	2.9	0.0	0.5	215	0.9	0.0	0.4	187	0.7	0.0	0.4	144	0.7	0.0	4.1	8	5.3	0.0
12/7/09 14:30	1.5	246	2.7	0.0	1.0	213	1.8	0.0	0.4	186	0.7	0.0	0.3	144	0.5	0.0	4.6	8	6.0	0.0
12/7/09 15:00	1.3	246	2.4	0.0	0.1	214	0.2	0.0	0.3	187	0.5	0.0	0.5	146	0.9	0.0	4.5	8	5.9	0.0
12/7/09 15:30	1.8	243	3.3	0.0	0.1	211	0.2	0.0	0.3	184	0.5	0.0	0.5	144	0.5	0.0	5.8	8	7.7	0.0
12/7/09 16:00	1.6	243	2.9	0.0	0.0	211	0.0	0.0	0.4	184	0.7	0.0	0.3	144	0.5	0.0	9.2	8	12.6	0.0
12/7/09 16:30	1.5	243	2.7	0.0	0.0	211	0.0	0.0	0.4	184	0.7	0.0	0.3	144	0.5	0.0	5.7	8	7.5	0.0
12/7/09 17:00	1.5	240	2.7	0.0	0.1	209	0.2	0.0	0.4	183	0.7	0.0	0.4	144	0.7	0.0	4.8	8	6.3	0.0
12/7/09 17:30	1.5	240	2.7	0.0	0.1	209	0.2	0.0	0.4	183	0.7	0.0	0.3	144	0.5	0.0	4.6	8	6.0	0.0
12/7/09 18:00	1.5	237	2.7	0.0	0.2	207	0.4	0.0	0.3	182	0.5	0.0	0.6	144	1.1	0.0	6.4	8	8.5	0.0
12/7/09 18:30	1.7	240	3.1	0.0	0.3	208	0.5	0.0	0.4	182	0.7	0.0	0.4	142	0.5	0.0	10.0	8	13.7	0.0
12/7/09 19:00	1.4	240	2.6	0.0	0.3	208	0.5	0.0	0.4	182	0.7	0.0	0.4	142	0.7	0.0	9.2	8	12.6	0.0
12/7/09 19:30	1.4	243	2.6	0.0	0.3	210	0.5	0.0	0.4	183	0.7	0.0	0.4	142	0.7	0.0	6.4	8	8.5	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/7/09 20:00	1.6	243	2.9	0.0	0.1	210	0.2	0.0	0.8	183	1.4	0.0	2.1	142	3.9	0.0	5.8	8	7.7	0.0
12/7/09 20:30	2.5	246	4.6	0.1	0.4	212	0.7	0.0	0.3	183	0.5	0.0	0.3	140	0.5	0.0	19.0	7	27.1	0.0
12/7/09 21:00	1.5	249	2.7	0.0	0.0	213	0.0	0.0	0.3	182	0.5	0.0	0.4	136	0.7	0.0	6.4	7	8.5	0.0
12/7/09 21:30	1.5	259	2.7	0.0	0.1	219	0.2	0.0	0.3	186	0.5	0.0	0.5	136	0.9	0.0	5.7	7	7.5	0.0
12/7/09 22:00	1.4	256	2.6	0.0	0.1	217	0.2	0.0	0.5	184	0.9	0.0	0.4	134	0.7	0.0	6.0	7	8.0	0.0
12/7/09 22:30	1.5	256	2.7	0.0	0.1	217	0.2	0.0	0.3	184	0.5	0.0	0.4	134	0.7	0.0	6.3	7	8.4	0.0
12/7/09 23:00	1.6	256	2.9	0.0	0.1	217	0.2	0.0	0.3	184	0.5	0.0	0.3	134	0.5	0.0	6.0	7	8.0	0.0
12/7/09 23:30	1.7	256	3.1	0.0	0.1	216	0.2	0.0	0.3	182	0.5	0.0	0.4	132	0.7	0.0	5.5	7	7.3	0.0
12/8/09 0:00	1.4	249	2.6	0.0	0.1	212	0.2	0.0	0.4	180	0.7	0.0	0.4	132	0.7	0.0	5.8	7	7.7	0.0
12/8/09 0:30	1.5	249	2.7	0.0	0.6	212	1.1	0.0	0.3	180	0.5	0.0	0.4	132	0.7	0.0	5.3	7	7.0	0.0
12/8/09 1:00	1.4	249	2.6	0.0	0.1	211	0.2	0.0	0.4	179	0.7	0.0	0.4	130	0.7	0.0	5.5	7	7.3	0.0
12/8/09 1:30	1.5	246	2.7	0.0	0.4	208	0.7	0.0	0.4	176	0.7	0.0	0.3	128	0.5	0.0	12.0	7	16.6	0.0
12/8/09 2:00	1.4	246	2.6	0.0	0.4	208	0.7	0.0	0.4	176	0.7	0.0	0.3	128	0.5	0.0	3.2	7	4.1	0.0
12/8/09 2:30	1.5	246	2.7	0.0	0.1	208	0.2	0.0	0.4	176	0.7	0.0	0.3	128	0.5	0.0	3.9	7	5.0	0.0
12/8/09 3:00	1.7	243	3.1	0.0	0.3	206	0.5	0.0	0.4	174	0.7	0.0	0.3	127	0.5	0.0	3.4	7	4.4	0.0
12/8/09 3:30	1.7	243	3.1	0.0	0.2	206	0.4	0.0	0.4	174	0.7	0.0	0.3	127	0.5	0.0	4.1	7	5.3	0.0
12/8/09 4:00	1.5	240	2.7	0.0	0.1	203	0.2	0.0	0.4	172	0.7	0.0	0.5	125	0.9	0.0	3.1	7	4.0	0.0
12/8/09 4:30	1.7	237	3.1	0.0	0.2	201	0.4	0.0	0.5	170	0.9	0.0	0.4	125	0.7	0.0	3.4	7	4.4	0.0
12/8/09 5:00	1.6	237	2.9	0.0	0.1	200	0.2	0.0	0.3	169	0.5	0.0	0.4	123	0.7	0.0	3.3	7	4.2	0.0
12/8/09 5:30	1.6	234	2.9	0.0	0.2	198	0.4	0.0	0.4	168	0.7	0.0	0.3	123	0.5	0.0	2.6	7	3.3	0.0
12/8/09 6:00	1.7	237	3.1	0.0	0.1	200	0.2	0.0	0.3	169	0.5	0.0	0.9	123	1.6	0.0	3.1	7	4.0	0.0
12/8/09 6:30	1.7	234	3.1	0.0	0.1	197	0.2	0.0	0.4	167	0.7	0.0	0.3	121	0.5	0.0	3.1	7	4.0	0.0
12/8/09 7:00	1.6	234	2.9	0.0	0.1	197	0.2	0.0	0.6	167	1.1	0.0	0.3	121	0.5	0.0	3.0	7	3.8	0.0
12/8/09 7:30	1.6	234	2.9	0.0	0.1	197	0.2	0.0	0.4	167	0.7	0.0	0.3	121	0.5	0.0	3.3	7	4.2	0.0
12/8/09 8:00	1.5	234	2.7	0.0	0.1	198	0.2	0.0	0.4	168	0.7	0.0	0.3	123	0.5	0.0	3.5	7	4.5	0.0
12/8/09 8:30	1.6	231	2.9	0.0	0.0	196	0.0	0.0	0.3	167	0.5	0.0	0.4	123	0.7	0.0	3.3	7	4.2	0.0
12/8/09 9:00	1.5	228	2.7	0.0	0.1	194	0.2	0.0	0.9	166	1.6	0.0	0.3	123	0.5	0.0	3.6	7	4.6	0.0
12/8/09 9:30	1.5	228	2.7	0.0	0.1	193	0.2	0.0	0.7	164	1.3	0.0	0.3	121	0.5	0.0	3.2	7	4.1	0.0
12/8/09 10:00	1.5	225	2.7	0.0	0.1	191	0.2	0.0	0.4	163	0.7	0.0	0.4	121	0.7	0.0	3.6	7	4.6	0.0
12/8/09 10:30	1.7	225	3.1	0.0	0.1	191	0.2	0.0	0.3	163	0.5	0.0	0.3	121	0.5	0.0	3.6	7	4.6	0.0
12/8/09 11:00	1.8	216	3.3	0.0	0.1	186	0.2	0.0	0.4	161	0.7	0.0	0.3	123	0.5	0.0	3.8	7	4.9	0.0
12/8/09 11:30	1.7	210	3.1	0.0	0.1	182	0.2	0.0	0.3	158	0.5	0.0	0.4	123	0.7	0.0	4.0	7	5.2	0.0
12/8/09 12:00	1.8	207	3.3	0.0	0.1	180	0.2	0.0	0.4	157	0.7	0.0	0.3	123	0.5	0.0	3.9	7	5.0	0.0
12/8/09 12:30	1.6	204	2.9	0.0	0.1	179	0.2	0.0	0.4	157	0.7	0.0	0.3	125	0.5	0.0	3.7	7	4.8	0.0
12/8/09 13:00	1.5	204	2.7	0.0	0.2	179	0.4	0.0	0.4	158	0.7	0.0	0.3	127	0.5	0.0	4.1	7	5.3	0.0
12/8/09 13:30	1.7	204	3.1	0.0	0.1	180	0.2	0.0	0.5	159	0.9	0.0	0.4	128	0.7	0.0	5.9	7	7.8	0.0
12/8/09 14:00	1.7	204	3.1	0.0	0.1	181	0.2	0.0	0.4	160	0.7	0.0	0.4	130	0.7	0.0	6.1	7	8.1	0.0
12/8/09 14:30	1.7	204	3.1	0.0	0.2	181	0.4	0.0	0.5	160	0.9	0.0	0.3	130	0.5	0.0	5.8	7	7.7	0.0
12/8/09 15:00	1.5	207	2.7	0.0	0.2	183	0.4	0.0	0.7	163	1.3	0.0	0.3	132	0.5	0.0	19.0	7	27.1	0.0
12/8/09 15:30	1.6	210	2.9	0.0	0.1	186	0.2	0.0	0.6	165	1.1	0.0	0.3	134	0.5	0.0	7.1	7	9.5	0.0
12/8/09 16:00	1.5	219	2.7	0.0	0.1	192	0.2	0.0	0.4	170	0.7	0.0	0.3	136	0.5	0.0	5.7	7	7.5	0.0
12/8/09 16:30	1.6	219	2.9	0.0	0.2	192	0.4	0.0	0.5	170	0.9	0.0	0.3	136	0.5	0.0	13.0	7	18.1	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/08/09 17:00	1.6	222	2.9	0.0	0.4	194	0.7	0.0	0.4	171	0.7	0.0	0.4	136	0.7	0.0	7.7	7	10.4	0.0
12/08/09 17:30	1.5	228	2.7	0.0	0.8	198	1.4	0.0	0.6	173	1.1	0.0	0.3	136	0.5	0.0	12.0	7	16.6	0.0
12/08/09 18:00	1.7	237	3.1	0.0	0.2	204	0.4	0.0	0.5	177	0.9	0.0	0.3	136	0.5	0.0	5.6	7	7.4	0.0
12/08/09 18:30	1.5	240	2.7	0.0	0.3	206	0.5	0.0	0.5	178	0.9	0.0	0.4	136	0.7	0.0	6.2	7	8.3	0.0
12/08/09 19:00	1.6	240	2.9	0.0	1.4	207	2.6	0.0	0.7	179	1.3	0.0	0.4	138	0.7	0.0	5.5	7	7.3	0.0
12/08/09 19:30	1.6	237	2.9	0.0	0.3	205	0.5	0.0	0.6	178	1.1	0.0	0.3	138	0.5	0.0	4.4	7	5.7	0.0
12/08/09 20:00	1.7	234	3.1	0.0	0.3	203	0.5	0.0	0.4	177	0.7	0.0	0.3	138	0.5	0.0	6.3	7	8.4	0.0
12/08/09 20:30	1.5	234	2.7	0.0	0.3	202	0.5	0.0	0.4	176	0.7	0.0	0.4	136	0.7	0.0	4.5	7	5.9	0.0
12/08/09 21:00	1.8	234	3.3	0.0	0.2	202	0.4	0.0	0.6	176	1.1	0.0	0.3	136	0.5	0.0	6.9	7	9.2	0.0
12/08/09 21:30	1.6	234	2.9	0.0	0.3	202	0.5	0.0	0.4	176	0.7	0.0	0.4	136	0.7	0.0	4.5	7	5.9	0.0
12/08/09 22:00	1.5	234	2.7	0.0	0.1	201	0.2	0.0	0.4	174	0.7	0.0	0.3	132	0.5	0.0	3.8	7	4.9	0.0
12/08/09 22:30	1.7	234	3.1	0.0	0.3	201	0.5	0.0	0.4	174	0.7	0.0	0.3	132	0.5	0.0	5.9	7	7.8	0.0
12/08/09 23:00	1.7	234	3.1	0.0	0.2	201	0.4	0.0	0.4	174	0.7	0.0	0.3	132	0.5	0.0	4.5	7	5.9	0.0
12/08/09 23:30	1.7	231	3.1	0.0	0.1	198	0.2	0.0	0.4	171	0.7	0.0	0.3	130	0.5	0.0	6.5	7	8.7	0.0
12/09/09 0:00	1.6	231	2.9	0.0	0.2	198	0.4	0.0	0.6	170	1.1	0.0	0.4	128	0.7	0.0	6.3	7	8.4	0.0
12/09/09 0:30	1.5	231	2.7	0.0	0.4	198	0.7	0.0	0.3	170	0.5	0.0	0.3	128	0.5	0.0	5.5	7	7.3	0.0
12/09/09 1:00	1.6	228	2.9	0.0	0.1	195	0.2	0.0	0.3	168	0.5	0.0	0.3	127	0.5	0.0	3.5	7	4.5	0.0
12/09/09 1:30	1.6	228	2.9	0.0	0.1	195	0.2	0.0	0.4	167	0.7	0.0	0.8	125	1.4	0.0	9.2	7	12.6	0.0
12/09/09 2:00	1.7	225	3.1	0.0	0.2	192	0.4	0.0	0.3	164	0.5	0.0	0.3	123	0.5	0.0	15.0	7	21.1	0.0
12/09/09 2:30	1.6	225	2.9	0.0	0.1	192	0.2	0.0	0.3	164	0.5	0.0	0.3	123	0.5	0.0	10.0	7	13.7	0.0
12/09/09 3:00	1.5	225	2.7	0.0	0.1	191	0.2	0.0	0.4	163	0.7	0.0	0.3	121	0.5	0.0	14.0	7	19.6	0.0
12/09/09 3:30	1.6	222	2.9	0.0	0.2	189	0.4	0.0	0.4	161	0.7	0.0	0.3	119	0.5	0.0	4.3	6	5.6	0.0
12/09/09 4:00	1.5	222	2.7	0.0	0.3	189	0.5	0.0	0.3	161	0.5	0.0	0.4	119	0.7	0.0	3.9	6	5.0	0.0
12/09/09 4:30	1.6	219	2.9	0.0	0.1	186	0.2	0.0	0.3	159	0.5	0.0	0.5	118	0.9	0.0	3.2	6	4.1	0.0
12/09/09 5:00	1.6	219	2.9	0.0	0.1	186	0.2	0.0	0.4	159	0.7	0.0	0.3	118	0.5	0.0	8.9	6	12.1	0.0
12/09/09 5:30	1.7	219	3.1	0.0	0.2	185	0.4	0.0	0.4	157	0.7	0.0	0.3	114	0.5	0.0	3.4	6	4.4	0.0
12/09/09 6:00	1.5	216	2.7	0.0	0.1	183	0.2	0.0	0.3	155	0.5	0.0	0.3	114	0.5	0.0	2.8	6	3.5	0.0
12/09/09 6:30	1.6	216	2.9	0.0	0.1	182	0.2	0.0	0.3	154	0.5	0.0	0.3	112	0.5	0.0	9.7	6	13.3	0.0
12/09/09 7:00	1.5	210	2.7	0.0	0.2	179	0.4	0.0	0.3	153	0.5	0.0	0.3	114	0.5	0.0	6.8	6	9.1	0.0
12/09/09 7:30	1.8	207	3.3	0.0	0.1	177	0.2	0.0	0.3	151	0.5	0.0	0.3	112	0.5	0.0	9.1	6	12.4	0.0
12/09/09 8:00	1.7	204	3.1	0.0	0.1	175	0.2	0.0	0.3	150	0.5	0.0	0.3	112	0.5	0.0	3.5	6	4.5	0.0
12/09/09 8:30	1.6	204	2.9	0.0	0.2	175	0.4	0.0	0.3	150	0.5	0.0	0.8	112	1.4	0.0	3.6	6	4.6	0.0
12/09/09 9:00	1.5	199	2.7	0.0	0.0	171	0.0	0.0	0.3	147	0.5	0.0	0.3	112	0.5	0.0	3.2	6	4.1	0.0
12/09/09 9:30	1.6	196	2.9	0.0	0.1	169	0.2	0.0	0.4	145	0.7	0.0	0.3	111	0.5	0.0	3.0	6	3.8	0.0
12/09/09 10:00	1.6	196	2.9	0.0	0.0	169	0.0	0.0	0.4	146	0.7	0.0	0.3	112	0.5	0.0	3.0	6	3.8	0.0
12/09/09 10:30	1.7	188	3.1	0.0	0.1	163	0.2	0.0	0.3	142	0.5	0.0	0.3	111	0.5	0.0	2.6	6	3.3	0.0
12/09/09 11:00	1.5	185	2.7	0.0	0.1	162	0.2	0.0	0.3	142	0.5	0.0	0.4	112	0.7	0.0	3.0	6	3.8	0.0
12/09/09 11:30	1.6	188	2.9	0.0	0.1	164	0.2	0.0	0.3	144	0.5	0.0	0.3	114	0.5	0.0	2.7	6	3.4	0.0
12/09/09 12:00	1.5	185	2.7	0.0	0.0	162	0.0	0.0	0.4	143	0.7	0.0	0.3	114	0.5	0.0	3.0	6	3.8	0.0
12/09/09 12:30	1.8	185	3.3	0.0	0.1	163	0.2	0.0	0.3	145	0.5	0.0	0.3	118	0.5	0.0	3.2	6	4.1	0.0
12/09/09 13:00	1.6	188	2.9	0.0	0.1	166	0.2	0.0	0.3	147	0.5	0.0	0.3	119	0.5	0.0	3.3	6	4.2	0.0
12/09/09 13:30	1.6	189	2.8	0.0	0.3	167	0.5	0.0	0.3	148	0.5	0.0	0.3	119	0.5	0.0	5.0	6	6.6	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/09/09 14:00	1.7	192	3.0	0.0	0.2	169	0.4	0.0	0.9	150	1.6	0.0	0.4	121	0.7	0.0	5.7	7	7.5	0.0
12/09/09 14:30	1.6	193	2.9	0.0	0.1	170	0.2	0.0	0.5	150	0.9	0.0	0.3	121	0.5	0.0	4.6	7	6.0	0.0
12/09/09 15:00	1.6	202	2.9	0.0	0.1	178	0.2	0.0	0.5	158	0.9	0.0	0.3	128	0.5	0.0	10.0	7	13.7	0.0
12/09/09 15:30	1.5	202	2.7	0.0	0.2	178	0.4	0.0	0.6	158	1.1	0.0	0.3	128	0.5	0.0	9.6	7	13.1	0.0
12/09/09 16:00	1.6	207	2.9	0.0	0.1	182	0.2	0.0	0.6	162	1.1	0.0	0.4	130	0.7	0.0	6.4	7	8.5	0.0
12/09/09 16:30	1.8	210	3.3	0.0	0.2	185	0.4	0.0	0.5	164	0.9	0.0	0.3	132	0.5	0.0	5.5	7	7.3	0.0
12/09/09 17:00	1.6	210	2.9	0.0	0.3	185	0.5	0.0	0.4	164	0.7	0.0	0.3	132	0.5	0.0	6.7	7	9.0	0.0
12/09/09 17:30	1.6	216	2.9	0.0	0.3	190	0.5	0.0	0.5	167	0.9	0.0	0.3	134	0.5	0.0	5.5	7	7.3	0.0
12/09/09 18:00	1.6	219	2.9	0.0	0.1	192	0.2	0.0	0.5	169	0.9	0.0	0.4	134	0.7	0.0	7.0	7	9.4	0.0
12/09/09 18:30	1.9	222	3.5	0.0	0.5	194	0.9	0.0	0.6	171	1.1	0.0	0.3	136	0.5	0.0	6.3	7	8.4	0.0
12/09/09 19:00	1.6	222	2.9	0.0	0.2	194	0.4	0.0	0.4	170	0.7	0.0	0.3	134	0.5	0.0	4.7	7	6.2	0.0
12/09/09 19:30	1.7	219	3.1	0.0	0.2	192	0.4	0.0	0.4	170	0.7	0.0	0.4	136	0.7	0.0	4.9	7	6.4	0.0
12/09/09 20:00	1.9	219	3.5	0.0	0.3	192	0.5	0.0	0.4	170	0.7	0.0	0.3	136	0.5	0.0	4.7	7	6.2	0.0
12/09/09 20:30	1.7	216	3.1	0.0	0.2	190	0.4	0.0	0.3	169	0.5	0.0	0.3	136	0.5	0.0	6.1	7	8.1	0.0
12/09/09 21:00	1.6	216	2.9	0.0	0.2	190	0.4	0.0	0.3	169	0.5	0.0	0.3	136	0.5	0.0	6.5	7	8.7	0.0
12/09/09 21:30	1.7	216	3.1	0.0	0.4	190	0.7	0.0	0.4	169	0.7	0.0	0.3	136	0.5	0.0	7.4	7	10.0	0.0
12/09/09 22:00	1.7	216	3.1	0.0	0.3	190	0.5	0.0	0.4	169	0.7	0.0	0.7	136	1.3	0.0	7.2	7	9.7	0.0
12/09/09 22:30	1.6	216	2.9	0.0	0.2	190	0.4	0.0	0.3	167	0.5	0.0	0.3	134	0.5	0.0	6.8	7	9.1	0.0
12/09/09 23:00	1.7	216	3.1	0.0	0.6	190	1.1	0.0	0.3	167	0.5	0.0	0.3	132	0.5	0.0	5.8	7	7.7	0.0
12/09/09 23:30	1.7	216	3.1	0.0	0.2	189	0.4	0.0	0.4	166	0.7	0.0	0.3	132	0.5	0.0	4.9	7	6.4	0.0
12/10/09 00:00	1.7	216	3.1	0.0	0.3	189	0.5	0.0	0.3	166	0.5	0.0	0.3	132	0.5	0.0	6.4	7	8.5	0.0
12/10/09 00:30	1.7	216	3.1	0.0	0.1	188	0.2	0.0	0.6	165	1.1	0.0	0.4	130	0.7	0.0	7.3	7	9.8	0.0
12/10/09 1:00	1.7	219	3.1	0.0	0.4	190	0.7	0.0	0.3	166	0.5	0.0	0.3	130	0.5	0.0	7.6	7	10.2	0.0
12/10/09 1:30	1.8	216	3.3	0.0	0.2	188	0.4	0.0	0.3	164	0.5	0.0	0.3	128	0.5	0.0	7.6	7	10.2	0.0
12/10/09 2:00	1.7	216	3.1	0.0	0.1	188	0.2	0.0	0.3	164	0.5	0.0	0.3	128	0.5	0.0	9.6	7	13.1	0.0
12/10/09 2:30	1.5	216	2.7	0.0	0.1	187	0.2	0.0	0.3	163	0.5	0.0	0.4	127	0.7	0.0	8.6	7	11.7	0.0
12/10/09 3:00	1.7	216	3.1	0.0	0.1	187	0.2	0.0	0.3	163	0.5	0.0	0.3	127	0.5	0.0	7.3	7	9.8	0.0
12/10/09 3:30	1.7	216	3.1	0.0	0.1	187	0.2	0.0	0.3	163	0.5	0.0	0.3	127	0.5	0.0	9.3	7	12.7	0.0
12/10/09 4:00	1.5	210	2.7	0.0	0.1	183	0.2	0.0	0.3	159	0.5	0.0	0.7	125	1.3	0.0	16.0	7	22.6	0.0
12/10/09 4:30	1.6	210	2.9	0.0	0.1	183	0.2	0.0	0.3	159	0.5	0.0	0.3	125	0.5	0.0	18.0	7	25.6	0.0
12/10/09 5:00	1.7	210	3.1	0.0	0.1	182	0.2	0.0	0.3	158	0.5	0.0	0.3	123	0.5	0.0	17.0	7	24.1	0.0
12/10/09 5:30	1.8	207	3.3	0.0	0.1	180	0.2	0.0	0.3	157	0.5	0.0	0.3	123	0.5	0.0	8.5	7	11.5	0.0
12/10/09 6:00	1.7	207	3.1	0.0	0.1	180	0.2	0.0	0.3	157	0.5	0.0	0.3	123	0.5	0.0	11.0	7	15.2	0.0
12/10/09 6:30	1.5	207	2.7	0.0	0.1	179	0.2	0.0	0.3	156	0.5	0.0	0.3	121	0.5	0.0	12.0	7	16.6	0.0
12/10/09 7:00	1.6	204	2.9	0.0	0.1	178	0.2	0.0	0.3	155	0.5	0.0	0.3	121	0.5	0.0	9.7	7	13.3	0.0
12/10/09 7:30	1.7	204	3.1	0.0	0.0	177	0.0	0.0	0.2	154	0.4	0.0	0.4	119	0.7	0.0	7.8	6	10.5	0.0
12/10/09 8:00	1.7	204	3.1	0.0	0.1	177	0.2	0.0	0.3	154	0.5	0.0	0.3	119	0.5	0.0	6.2	6	8.3	0.0
12/10/09 8:30	1.8	202	3.3	0.0	0.1	175	0.2	0.0	0.3	153	0.5	0.0	0.3	119	0.5	0.0	3.3	6	4.2	0.0
12/10/09 9:00	2.0	199	3.7	0.0	0.1	173	0.2	0.0	0.3	152	0.5	0.0	0.3	119	0.5	0.0	3.2	6	4.1	0.0
12/10/09 9:30	1.7	196	3.1	0.0	0.0	171	0.0	0.0	0.3	151	0.5	0.0	0.3	119	0.5	0.0	3.5	6	4.5	0.0
12/10/09 10:00	1.5	193	2.7	0.0	0.1	169	0.2	0.0	0.3	149	0.5	0.0	0.3	119	0.5	0.0	3.9	6	5.0	0.0
12/10/09 10:30	1.7	191	3.1	0.0	0.3	168	0.5	0.0	0.3	148	0.5	0.0	0.4	119	0.7	0.0	3.5	6	4.5	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/10/09 11:00	1.8	188	3.3	0.0	0.1	166	0.2	0.0	0.3	147	0.5	0.0	0.3	119	0.5	0.0	4.4	6	5.7	0.0
12/10/09 11:30	1.6	188	2.9	0.0	0.1	166	0.2	0.0	0.3	147	0.5	0.0	0.3	119	0.5	0.0	4.4	6	5.7	0.0
12/10/09 12:00	1.6	191	2.9	0.0	0.1	168	0.2	0.0	0.4	149	0.7	0.0	0.3	121	0.5	0.0	3.9	7	5.0	0.0
12/10/09 12:30	1.5	191	2.7	0.0	0.0	168	0.0	0.0	0.3	149	0.5	0.0	0.3	121	0.5	0.0	9.4	7	12.8	0.0
12/10/09 13:00	1.7	191	3.1	0.0	0.1	168	0.2	0.0	0.4	149	0.7	0.0	0.3	121	0.5	0.0	8.1	7	11.0	0.0
12/10/09 13:30	1.5	193	2.7	0.0	0.1	171	0.2	0.0	0.4	152	0.7	0.0	0.3	123	0.5	0.0	6.2	7	8.3	0.0
12/10/09 14:00	1.5	193	2.7	0.0	1.5	171	2.7	0.0	0.5	153	0.9	0.0	0.3	125	0.5	0.0	6.8	7	9.1	0.0
12/10/09 14:30	1.5	196	2.7	0.0	0.0	173	0.0	0.0	0.4	154	0.7	0.0	0.3	125	0.5	0.0	5.4	7	7.1	0.0
12/10/09 15:00	1.6	202	2.9	0.0	0.0	177	0.0	0.0	0.4	157	0.7	0.0	0.4	127	0.7	0.0	7.1	0.0	7.1	0.0
12/10/09 15:30	2.0	207	3.7	0.0	0.3	181	0.5	0.0	0.4	159	0.7	0.0	0.3	127	0.5	0.0	4.9	7	6.4	0.0
12/10/09 16:00	1.8	219	3.3	0.0	0.1	190	0.2	0.0	1.2	165	2.2	0.0	0.3	128	0.5	0.0	5.4	7	7.1	0.0
12/10/09 16:30	1.7	234	3.1	0.0	0.7	200	1.3	0.0	0.4	171	0.7	0.0	0.3	128	0.5	0.0	14.0	7	19.6	0.0
12/10/09 17:00	1.7	246	3.1	0.0	0.3	208	0.5	0.0	0.4	176	0.7	0.0	0.3	128	0.5	0.0	7.0	7	9.4	0.0
12/10/09 17:30	1.8	256	3.3	0.0	0.1	215	0.2	0.0	0.5	180	0.9	0.0	0.3	128	0.5	0.0	5.2	7	6.8	0.0
12/10/09 18:00	1.7	262	3.1	0.0	0.1	220	0.2	0.0	0.4	184	0.7	0.0	0.3	130	0.5	0.0	7.3	7	9.8	0.0
12/10/09 18:30	1.7	265	3.1	0.0	0.1	222	0.2	0.0	0.4	185	0.7	0.0	0.3	130	0.5	0.0	7.6	7	10.2	0.0
12/10/09 19:00	1.7	262	3.1	0.0	0.1	220	0.2	0.0	0.4	184	0.7	0.0	0.3	130	0.5	0.0	6.5	7	8.7	0.0
12/10/09 19:30	1.9	265	3.5	0.1	0.2	222	0.4	0.0	0.4	185	0.7	0.0	0.3	130	0.5	0.0	6.7	7	9.0	0.0
12/10/09 20:00	1.7	265	3.1	0.0	0.1	222	0.2	0.0	0.3	186	0.5	0.0	0.3	132	0.5	0.0	5.9	7	7.8	0.0
12/10/09 20:30	1.6	265	2.9	0.0	0.7	222	1.3	0.0	0.3	186	0.5	0.0	0.3	132	0.5	0.0	4.9	7	6.4	0.0
12/10/09 21:00	1.8	269	3.3	0.0	0.3	225	0.5	0.0	0.3	188	0.5	0.0	0.3	132	0.5	0.0	5.4	7	7.1	0.0
12/10/09 21:30	1.7	272	3.1	0.0	0.2	227	0.4	0.0	0.3	189	0.5	0.0	0.3	132	0.5	0.0	4.6	7	6.0	0.0
12/10/09 22:00	1.7	272	3.1	0.0	0.2	227	0.4	0.0	0.3	189	0.5	0.0	0.3	132	0.5	0.0	4.9	7	6.4	0.0
12/10/09 22:30	1.8	279	3.3	0.1	0.1	231	0.2	0.0	0.3	191	0.5	0.0	0.3	130	0.5	0.0	6.4	7	8.5	0.0
12/10/09 23:00	1.7	279	3.1	0.0	0.1	231	0.2	0.0	0.4	191	0.7	0.0	0.3	130	0.5	0.0	7.1	7	9.5	0.0
12/10/09 23:30	1.7	282	3.1	0.0	0.3	233	0.5	0.0	0.3	192	0.5	0.0	0.3	130	0.5	0.0	5.6	7	7.4	0.0
12/11/09 00:00	1.7	282	3.1	0.0	0.1	233	0.2	0.0	0.3	191	0.5	0.0	0.5	128	0.9	0.0	4.8	7	6.3	0.0
12/11/09 00:30	1.7	285	3.1	0.0	0.1	235	0.2	0.0	0.4	192	0.7	0.0	0.3	128	0.5	0.0	4.6	7	6.0	0.0
12/11/09 1:00	1.7	282	3.1	0.0	0.1	233	0.2	0.0	0.3	191	0.5	0.0	0.7	128	1.3	0.0	8.5	7	11.5	0.0
12/11/09 1:30	1.6	279	2.9	0.0	0.2	230	0.4	0.0	0.3	188	0.5	0.0	0.3	127	0.5	0.0	4.6	7	6.0	0.0
12/11/09 2:00	1.6	275	2.9	0.0	0.1	227	0.2	0.0	0.3	187	0.5	0.0	0.3	127	0.5	0.0	4.5	7	5.9	0.0
12/11/09 2:30	1.7	272	3.1	0.0	0.1	225	0.2	0.0	0.3	186	0.5	0.0	0.3	127	0.5	0.0	5.4	7	7.1	0.0
12/11/09 3:00	1.8	269	3.3	0.0	0.1	223	0.2	0.0	0.3	184	0.5	0.0	0.3	127	0.5	0.0	5.5	7	7.3	0.0
12/11/09 3:30	1.8	272	3.3	0.1	0.1	225	0.2	0.0	0.3	185	0.5	0.0	0.3	125	0.5	0.0	5.0	7	6.6	0.0
12/11/09 4:00	1.7	272	3.1	0.0	0.1	225	0.2	0.0	0.3	185	0.5	0.0	0.3	125	0.5	0.0	4.0	7	5.2	0.0
12/11/09 4:30	1.6	269	2.9	0.0	0.0	222	0.0	0.0	0.3	183	0.5	0.0	0.3	125	0.5	0.0	4.0	7	5.2	0.0
12/11/09 5:00	1.6	269	2.9	0.0	0.1	222	0.2	0.0	0.3	182	0.5	0.0	0.3	123	0.5	0.0	4.2	7	5.5	0.0
12/11/09 5:30	1.6	269	2.9	0.0	0.0	222	0.0	0.0	0.3	182	0.5	0.0	0.3	123	0.5	0.0	4.2	7	5.5	0.0
12/11/09 6:00	1.7	269	3.1	0.0	0.0	222	0.0	0.0	0.4	182	0.7	0.0	0.3	123	0.5	0.0	5.0	7	6.6	0.0
12/11/09 6:30	1.7	272	3.1	0.0	0.1	224	0.2	0.0	0.4	184	0.7	0.0	0.3	123	0.5	0.0	4.5	7	5.9	0.0
12/11/09 7:00	2.1	272	3.9	0.1	0.0	224	0.0	0.0	0.3	184	0.5	0.0	0.3	123	0.5	0.0	4.2	7	5.5	0.0
12/11/09 7:30	1.6	272	2.9	0.0	0.1	224	0.2	0.0	0.3	184	0.5	0.0	0.3	123	0.5	0.0	4.1	7	5.3	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/11/09 8:00	1.7	272	3.1	0.0	0.1	223	0.2	0.0	0.3	182	0.5	0.0	0.3	121	0.5	0.0	5.9	7	7.8	0.0
12/11/09 8:30	1.7	272	3.1	0.0	0.1	223	0.2	0.0	0.3	182	0.5	0.0	0.3	121	0.5	0.0	8.3	7	11.3	0.0
12/11/09 9:00	1.8	275	3.3	0.1	0.1	226	0.2	0.0	0.3	184	0.5	0.0	0.3	121	0.5	0.0	5.4	7	7.1	0.0
12/11/09 9:30	1.8	275	3.3	0.1	0.1	226	0.2	0.0	0.3	184	0.5	0.0	0.4	121	0.7	0.0	4.8	7	6.3	0.0
12/11/09 10:00	1.7	279	3.1	0.0	0.0	228	0.0	0.0	0.2	185	0.4	0.0	0.3	121	0.5	0.0	4.2	7	5.5	0.0
12/11/09 10:30	1.8	282	3.3	0.1	0.1	230	0.2	0.0	0.3	187	0.5	0.0	0.3	121	0.5	0.0	6.1	7	8.1	0.0
12/11/09 11:00	1.8	282	3.3	0.1	0.1	230	0.2	0.0	0.3	187	0.5	0.0	0.3	121	0.5	0.0	4.9	7	6.4	0.0
12/11/09 11:30	1.7	285	3.1	0.0	0.1	232	0.2	0.0	0.3	188	0.5	0.0	0.3	121	0.5	0.0	7.1	7	9.5	0.0
12/11/09 12:00	1.7	285	3.1	0.0	0.1	233	0.2	0.0	0.3	189	0.5	0.0	0.3	123	0.5	0.0	4.6	7	6.0	0.0
12/11/09 12:30	1.7	289	3.1	0.1	0.0	235	0.0	0.0	0.3	190	0.5	0.0	0.5	123	0.9	0.0	5.4	7	7.1	0.0
12/11/09 13:00	1.7	292	3.1	0.1	0.1	238	0.2	0.0	0.3	193	0.5	0.0	0.3	125	0.5	0.0	4.9	7	6.4	0.0
12/11/09 13:30	1.6	303	2.9	0.0	0.4	245	0.6	0.0	0.3	197	0.5	0.0	0.3	125	0.5	0.0	4.7	7	6.2	0.0
12/11/09 14:00	1.8	310	3.3	0.1	0.6	251	1.1	0.0	0.3	201	0.5	0.0	0.3	127	0.5	0.0	6.7	7	9.0	0.0
12/11/09 14:30	1.7	313	3.1	0.1	0.5	254	0.9	0.0	0.3	204	0.5	0.0	0.3	128	0.5	0.0	4.5	7	5.9	0.0
12/11/09 15:00	1.7	324	3.1	0.1	0.5	261	0.8	0.0	0.4	208	0.7	0.0	0.3	128	0.5	0.0	4.7	7	6.2	0.0
12/11/09 15:30	1.7	332	3.1	0.1	0.4	267	0.7	0.0	0.4	213	0.7	0.0	0.3	132	0.5	0.0	5.1	7	6.7	0.0
12/11/09 16:00	2.4	335	4.4	0.1	0.3	270	0.6	0.0	0.4	215	0.7	0.0	0.3	132	0.5	0.0	4.2	7	5.5	0.0
12/11/09 16:30	1.6	339	2.9	0.1	0.2	272	0.4	0.0	0.3	216	0.5	0.0	0.3	132	0.5	0.0	4.8	7	6.3	0.0
12/11/09 17:00	1.7	332	3.1	0.1	0.2	267	0.3	0.0	0.4	213	0.7	0.0	0.3	132	0.5	0.0	5.6	7	7.4	0.0
12/11/09 17:30	1.8	320	3.3	0.1	0.1	260	0.2	0.0	0.3	209	0.5	0.0	0.3	132	0.5	0.0	6.6	7	8.8	0.0
12/11/09 18:00	1.8	317	3.3	0.1	0.2	258	0.4	0.0	0.3	208	0.5	0.0	0.3	134	0.5	0.0	7.9	7	10.7	0.0
12/11/09 18:30	1.8	317	3.3	0.1	0.2	258	0.4	0.0	0.3	208	0.5	0.0	0.4	134	0.7	0.0	6.0	7	8.0	0.0
12/11/09 19:00	1.7	317	3.1	0.1	0.2	258	0.4	0.0	0.3	208	0.5	0.0	0.3	134	0.5	0.0	4.8	7	6.3	0.0
12/11/09 19:30	1.9	328	3.5	0.1	0.2	265	0.4	0.0	0.3	213	0.5	0.0	0.3	134	0.5	0.0	6.5	7	8.7	0.0
12/11/09 20:00	1.7	332	3.1	0.1	0.3	269	0.5	0.0	0.3	216	0.5	0.0	0.3	136	0.5	0.0	7.3	7	9.8	0.0
12/11/09 20:30	1.8	324	3.3	0.1	0.3	264	0.5	0.0	0.3	213	0.5	0.0	0.3	136	0.5	0.0	6.8	7	9.1	0.0
12/11/09 21:00	1.8	324	3.3	0.1	0.3	264	0.5	0.0	0.4	213	0.7	0.0	0.3	136	0.5	0.0	7.6	7	10.2	0.0
12/11/09 21:30	1.8	328	3.3	0.1	0.3	266	0.5	0.0	0.3	214	0.5	0.0	0.3	136	0.5	0.0	6.7	7	9.0	0.0
12/11/09 22:00	1.9	328	3.5	0.1	0.3	267	0.6	0.0	0.4	215	0.7	0.0	0.3	138	0.5	0.0	5.9	7	7.8	0.0
12/11/09 22:30	1.5	328	2.7	0.1	0.3	267	0.6	0.0	0.3	215	0.5	0.0	0.4	138	0.7	0.0	6.3	7	8.4	0.0
12/11/09 23:00	1.9	332	3.5	0.1	0.4	269	0.6	0.0	0.3	217	0.5	0.0	0.3	138	0.5	0.0	7.9	7	10.7	0.0
12/11/09 23:30	2.1	332	3.9	0.1	0.4	269	0.7	0.0	0.5	216	0.9	0.0	0.4	136	0.7	0.0	8.9	7	12.1	0.0
12/12/09 0:00	1.9	332	3.5	0.1	0.4	269	0.7	0.0	0.4	216	0.7	0.0	0.3	136	0.5	0.0	6.9	7	9.2	0.0
12/12/09 0:30	1.8	328	3.3	0.1	0.4	266	0.7	0.0	0.4	214	0.7	0.0	0.3	136	0.5	0.0	5.7	7	7.5	0.0
12/12/09 1:00	2.0	328	3.7	0.1	0.4	266	0.7	0.0	0.4	214	0.7	0.0	0.3	136	0.5	0.0	6.4	7	8.5	0.0
12/12/09 1:30	1.8	324	3.3	0.1	0.4	264	0.8	0.0	0.3	213	0.5	0.0	0.3	136	0.5	0.0	10.0	7	13.7	0.0
12/12/09 2:00	1.9	324	3.5	0.1	0.4	263	0.8	0.0	0.4	211	0.7	0.0	0.3	134	0.5	0.0	6.2	7	8.3	0.0
12/12/09 2:30	1.8	320	3.3	0.1	0.5	261	0.8	0.0	0.3	211	0.5	0.0	0.3	136	0.5	0.0	14.0	7	19.6	0.0
12/12/09 3:00	1.9	324	3.5	0.1	0.5	263	0.9	0.0	0.4	211	0.7	0.0	0.3	134	0.5	0.0	8.3	7	11.3	0.0
12/12/09 3:30	1.9	320	3.5	0.1	0.5	260	0.9	0.0	0.4	209	0.7	0.0	0.3	132	0.5	0.0	7.2	7	9.7	0.0
12/12/09 4:00	1.8	320	3.3	0.1	0.5	260	0.9	0.0	0.5	209	0.9	0.0	0.3	132	0.5	0.0	6.5	7	8.7	0.0
12/12/09 4:30	1.8	320	3.3	0.1	0.5	260	0.9	0.0	0.6	209	1.1	0.0	0.4	132	0.7	0.0	6.2	7	8.3	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/12/09 5:00	1.9	317	3.5	0.1	0.5	257	1.0	0.0	0.5	207	0.9	0.0	0.3	132	0.5	0.0	12.0	7	16.6	0.0
12/12/09 5:30	3.0	317	5.6	0.1	0.6	257	1.0	0.0	0.5	206	0.9	0.0	0.3	130	0.5	0.0	12.0	7	16.6	0.0
12/12/09 6:00	2.0	313	3.7	0.1	0.6	254	1.0	0.0	0.4	205	0.7	0.0	0.3	130	0.5	0.0	6.3	7	8.4	0.0
12/12/09 6:30	1.8	313	3.3	0.1	0.6	254	1.0	0.0	0.4	205	0.7	0.0	0.4	130	0.7	0.0	8.4	7	11.4	0.0
12/12/09 7:00	2.0	310	3.7	0.1	0.6	252	1.1	0.0	0.4	204	0.7	0.0	0.3	132	0.5	0.0	5.7	7	7.5	0.0
12/12/09 7:30	1.8	310	3.3	0.1	0.2	252	0.4	0.0	0.4	204	0.7	0.0	0.3	132	0.5	0.0	7.7	7	10.4	0.0
12/12/09 8:00	1.8	306	3.3	0.1	0.3	249	0.5	0.0	0.3	202	0.5	0.0	0.3	130	0.5	0.0	7.8	7	10.5	0.0
12/12/09 8:30	1.9	306	3.5	0.1	0.1	249	0.2	0.0	0.4	202	0.7	0.0	0.4	130	0.7	0.0	7.7	7	10.4	0.0
12/12/09 9:00	2.1	306	3.9	0.1	0.2	249	0.4	0.0	0.4	201	0.7	0.0	0.4	128	0.7	0.0	5.4	7	7.1	0.0
12/12/09 9:30	2.2	306	4.0	0.1	0.1	249	0.2	0.0	0.4	202	0.7	0.0	0.5	130	0.9	0.0	6.9	7	9.2	0.0
12/12/09 10:00	2.0	306	3.7	0.1	0.1	249	0.2	0.0	0.3	202	0.5	0.0	0.4	130	0.7	0.0	7.3	7	9.8	0.0
12/12/09 10:30	2.0	303	3.7	0.1	0.2	246	0.4	0.0	0.3	199	0.5	0.0	0.3	128	0.5	0.0	7.1	7	9.5	0.0
12/12/09 11:00	2.2	306	4.0	0.1	0.1	249	0.2	0.0	0.5	201	0.9	0.0	0.3	128	0.5	0.0	7.7	7	10.4	0.0
12/12/09 11:30	2.3	299	4.2	0.1	0.3	245	0.5	0.0	0.5	199	0.9	0.0	0.3	130	0.5	0.0	7.7	7	10.4	0.0
12/12/09 12:00	1.9	303	3.5	0.1	0.4	247	0.7	0.0	0.4	200	0.7	0.0	0.5	130	0.9	0.0	7.9	7	10.7	0.0
12/12/09 12:30	2.3	299	4.2	0.1	0.1	245	0.2	0.0	0.9	200	1.6	0.0	0.4	132	0.7	0.0	8.0	7	10.8	0.0
12/12/09 13:00	2.0	299	3.7	0.1	0.2	247	0.4	0.0	1.2	202	2.2	0.0	0.4	136	0.7	0.0	8.3	7	11.3	0.0
12/12/09 13:30	2.2	299	4.0	0.1	0.1	247	0.2	0.0	0.9	202	1.6	0.0	0.4	136	0.7	0.0	8.9	7	12.1	0.0
12/12/09 14:00	2.1	303	3.9	0.1	0.3	250	0.5	0.0	0.7	205	1.3	0.0	0.3	138	0.5	0.0	13.0	7	18.1	0.0
12/12/09 14:30	2.0	303	3.7	0.1	0.2	250	0.4	0.0	0.9	206	1.6	0.0	0.3	140	0.5	0.0	8.6	7	11.7	0.0
12/12/09 15:00	2.5	303	4.6	0.1	0.3	250	0.5	0.0	0.9	206	1.6	0.0	0.4	140	0.7	0.0	9.1	7	12.4	0.0
12/12/09 15:30	1.9	299	3.5	0.1	0.4	247	0.7	0.0	1.1	204	2.0	0.0	0.4	138	0.7	0.0	8.4	7	11.4	0.0
12/12/09 16:00	2.2	299	4.0	0.1	0.5	248	0.9	0.0	1.2	205	2.2	0.0	0.5	140	0.9	0.0	9.8	7	13.4	0.0
12/12/09 16:30	2.5	299	4.6	0.1	0.5	248	0.9	0.0	0.9	206	1.6	0.0	0.4	142	0.7	0.0	9.1	8	12.4	0.0
12/12/09 17:00	2.2	303	4.0	0.1	0.3	251	0.5	0.0	1.0	207	1.8	0.0	0.4	142	0.7	0.0	11.0	8	15.2	0.0
12/12/09 17:30	2.2	299	4.0	0.1	0.3	248	0.5	0.0	0.8	206	1.4	0.0	0.4	142	0.7	0.0	13.0	8	18.1	0.0
12/12/09 18:00	2.2	299	4.0	0.1	0.5	248	0.9	0.0	0.7	205	1.3	0.0	0.6	140	1.1	0.0	16.0	7	22.6	0.0
12/12/09 18:30	2.4	303	4.4	0.1	0.4	250	0.7	0.0	0.6	206	1.1	0.0	0.4	140	0.7	0.0	20.0	7	28.6	0.0
12/12/09 19:00	2.2	299	4.0	0.1	1.0	248	1.8	0.0	0.6	205	1.1	0.0	0.4	140	0.7	0.0	16.0	7	22.6	0.0
12/12/09 19:30	2.3	299	4.2	0.1	1.2	248	2.2	0.0	0.4	205	0.7	0.0	0.4	140	0.7	0.0	13.0	7	18.1	0.0
12/12/09 20:00	2.7	299	5.0	0.1	0.9	248	1.6	0.0	0.6	205	1.1	0.0	0.5	140	0.9	0.0	16.0	7	22.6	0.0
12/12/09 20:30	2.3	299	4.2	0.1	0.7	248	1.3	0.0	0.4	206	0.7	0.0	0.3	142	0.5	0.0	19.0	8	27.1	0.0
12/12/09 21:00	2.7	296	5.0	0.1	0.6	245	1.1	0.0	0.5	203	0.9	0.0	0.4	140	0.7	0.0	12.0	7	16.6	0.0
12/12/09 21:30	2.3	289	4.2	0.1	0.6	241	1.1	0.0	0.4	200	0.7	0.0	0.4	140	0.7	0.0	12.0	7	16.6	0.0
12/12/09 22:00	2.1	285	3.9	0.1	0.3	239	0.5	0.0	0.4	199	0.7	0.0	0.4	140	0.7	0.0	11.0	7	15.2	0.0
12/12/09 22:30	2.2	279	4.0	0.1	0.4	233	0.7	0.0	0.6	195	1.1	0.0	0.4	138	0.7	0.0	12.0	7	16.6	0.0
12/12/09 23:00	2.1	272	3.9	0.1	0.5	229	0.9	0.0	0.4	192	0.7	0.0	0.4	138	0.7	0.0	11.0	7	15.2	0.0
12/12/09 23:30	2.2	265	4.0	0.1	0.3	224	0.5	0.0	0.5	189	0.9	0.0	0.4	136	0.7	0.0	11.0	7	15.2	0.0
12/13/09 0:00	2.3	259	4.2	0.1	0.3	219	0.5	0.0	0.4	185	0.7	0.0	0.3	134	0.5	0.0	11.0	7	15.2	0.0
12/13/09 0:30	2.4	249	4.4	0.1	0.3	212	0.5	0.0	0.5	181	0.9	0.0	0.4	134	0.7	0.0	12.0	7	16.6	0.0
12/13/09 1:00	2.3	243	4.2	0.1	0.3	208	0.5	0.0	0.6	178	1.1	0.0	0.4	134	0.7	0.0	15.0	7	21.1	0.0
12/13/09 1:30	2.7	240	5.0	0.1	0.3	206	0.5	0.0	0.6	177	1.1	0.0	0.3	134	0.5	0.0	11.0	7	15.2	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/13/09 2:00	2.3	237	4.2	0.1	0.2	204	0.4	0.0	0.8	176	1.4	0.0	0.4	134	0.7	0.0	11.0	7	15.2	0.0
12/13/09 2:30	2.1	234	3.9	0.1	0.4	202	0.7	0.0	0.7	175	1.3	0.0	0.4	134	0.7	0.0	13.0	7	18.1	0.0
12/13/09 3:00	2.3	234	4.2	0.1	0.3	202	0.5	0.0	0.6	176	1.1	0.0	0.4	136	0.7	0.0	12.0	7	16.6	0.0
12/13/09 3:30	2.3	231	4.2	0.1	0.4	200	0.7	0.0	0.6	175	1.1	0.0	0.4	136	0.7	0.0	16.0	7	22.6	0.0
12/13/09 4:00	2.5	228	4.6	0.1	0.5	198	0.9	0.0	0.4	173	0.7	0.0	0.4	136	0.7	0.0	18.0	7	25.6	0.0
12/13/09 4:30	2.4	225	4.4	0.1	0.7	196	1.3	0.0	0.7	172	1.3	0.0	0.4	136	0.7	0.0	14.0	7	19.6	0.0
12/13/09 5:00	2.4	225	4.4	0.1	0.3	196	0.5	0.0	0.6	172	1.1	0.0	0.3	136	0.5	0.0	12.0	7	16.6	0.0
12/13/09 5:30	2.4	222	4.4	0.1	0.3	194	0.5	0.0	0.5	171	0.9	0.0	0.4	136	0.7	0.0	11.0	7	15.2	0.0
12/13/09 6:00	2.6	222	4.8	0.1	0.6	194	1.1	0.0	0.6	171	1.1	0.0	0.4	136	0.7	0.0	13.0	7	18.1	0.0
12/13/09 6:30	2.6	222	4.8	0.1	0.3	194	0.5	0.0	0.6	170	1.1	0.0	0.5	134	0.9	0.0	14.0	7	19.6	0.0
12/13/09 7:00	2.5	219	4.6	0.1	0.4	192	0.7	0.0	0.4	169	0.7	0.0	0.4	134	0.7	0.0	12.0	7	16.6	0.0
12/13/09 7:30	2.4	219	4.4	0.1	0.4	192	0.7	0.0	0.3	169	0.5	0.0	0.4	134	0.7	0.0	15.0	7	21.1	0.0
12/13/09 8:00	2.3	216	4.2	0.1	0.1	189	0.5	0.0	0.4	166	0.7	0.0	0.4	132	0.7	0.0	12.0	7	16.6	0.0
12/13/09 8:30	2.1	219	3.9	0.0	0.7	191	1.3	0.0	0.4	167	0.7	0.0	0.4	132	0.7	0.0	14.0	7	19.6	0.0
12/13/09 9:00	2.2	216	4.0	0.0	0.7	189	1.3	0.0	0.3	166	0.5	0.0	0.4	132	0.7	0.0	14.0	7	19.6	0.0
12/13/09 9:30	2.3	219	4.2	0.1	0.4	191	0.7	0.0	0.4	167	0.7	0.0	0.4	132	0.7	0.0	14.0	7	19.6	0.0
12/13/09 10:00	2.1	219	3.9	0.0	0.4	191	0.7	0.0	0.4	167	0.7	0.0	0.4	130	0.7	0.0	13.0	7	18.1	0.0
12/13/09 10:30	2.1	216	3.9	0.0	0.3	189	0.5	0.0	0.3	166	0.5	0.0	0.3	132	0.5	0.0	12.0	7	16.6	0.0
12/13/09 11:00	2.3	216	4.2	0.1	0.3	188	0.5	0.0	0.4	165	0.7	0.0	0.3	130	0.5	0.0	14.0	7	19.6	0.0
12/13/09 11:30	2.1	216	3.9	0.0	0.3	188	0.5	0.0	0.4	165	0.7	0.0	0.8	130	1.4	0.0	12.0	7	16.6	0.0
12/13/09 12:00	2.5	216	4.6	0.1	0.3	188	0.5	0.0	0.6	165	1.1	0.0	0.4	130	0.7	0.0	15.0	7	21.1	0.0
12/13/09 12:30	2.0	216	3.7	0.0	0.3	188	0.5	0.0	0.4	165	0.7	0.0	0.4	130	0.7	0.0	12.0	7	16.6	0.0
12/13/09 13:00	2.0	210	3.7	0.0	0.2	184	0.4	0.0	0.4	163	0.7	0.0	0.3	130	0.5	0.0	13.0	7	18.1	0.0
12/13/09 13:30	2.1	210	3.9	0.0	0.4	184	0.7	0.0	0.3	162	0.5	0.0	0.4	128	0.7	0.0	11.0	7	15.2	0.0
12/13/09 14:00	2.1	210	3.9	0.0	0.8	183	1.4	0.0	0.4	161	0.7	0.0	0.4	127	0.7	0.0	12.0	7	16.6	0.0
12/13/09 14:30	1.9	210	3.5	0.0	0.2	183	0.4	0.0	0.4	161	0.7	0.0	0.4	127	0.7	0.0	13.0	7	18.1	0.0
12/13/09 15:00	2.2	207	4.0	0.0	0.2	181	0.4	0.0	0.5	158	0.9	0.0	0.3	125	0.5	0.0	13.0	7	18.1	0.0
12/13/09 15:30	2.3	207	4.2	0.0	0.2	181	0.4	0.0	0.5	158	0.9	0.0	0.3	125	0.5	0.0	13.0	7	18.1	0.0
12/13/09 16:00	2.1	207	3.9	0.0	0.7	181	1.3	0.0	0.4	158	0.7	0.0	0.5	125	0.9	0.0	16.0	7	22.6	0.0
12/13/09 16:30	2.1	207	3.9	0.0	0.2	181	0.4	0.0	0.5	158	0.9	0.0	0.4	125	0.7	0.0	13.0	7	18.1	0.0
12/13/09 17:00	2.1	207	3.9	0.0	0.3	181	0.5	0.0	0.4	158	0.7	0.0	0.5	125	0.9	0.0	14.0	7	19.6	0.0
12/13/09 17:30	2.2	204	4.0	0.0	0.3	179	0.5	0.0	0.4	157	0.7	0.0	0.4	125	0.7	0.0	13.0	7	18.1	0.0
12/13/09 18:00	2.2	204	4.0	0.0	0.4	178	0.7	0.0	0.5	156	0.9	0.0	0.4	123	0.7	0.0	12.0	7	16.6	0.0
12/13/09 18:30	2.1	204	3.9	0.0	1.8	178	3.3	0.0	0.4	155	0.7	0.0	0.4	121	0.7	0.0	9.5	7	13.0	0.0
12/13/09 19:00	2.0	202	3.7	0.0	1.2	176	2.2	0.0	0.4	154	0.7	0.0	0.4	121	0.7	0.0	11.0	7	15.2	0.0
12/13/09 19:30	1.9	202	3.5	0.0	0.4	175	0.7	0.0	0.4	153	0.7	0.0	0.4	119	0.7	0.0	9.4	6	12.8	0.0
12/13/09 20:00	2.1	202	3.9	0.0	0.5	175	0.9	0.0	0.4	153	0.7	0.0	0.4	119	0.7	0.0	12.0	6	16.6	0.0
12/13/09 20:30	2.1	199	3.9	0.0	0.3	173	0.5	0.0	0.6	152	1.1	0.0	0.3	119	0.5	0.0	9.8	6	13.4	0.0
12/13/09 21:00	2.1	202	3.9	0.0	0.4	174	0.7	0.0	0.4	152	0.7	0.0	0.3	118	0.5	0.0	10.0	6	13.7	0.0
12/13/09 21:30	2.1	199	3.9	0.0	0.3	173	0.5	0.0	0.3	151	0.5	0.0	0.4	118	0.7	0.0	16.0	6	22.6	0.0
12/13/09 22:00	2.3	199	4.2	0.0	0.3	173	0.5	0.0	0.4	151	0.7	0.0	0.6	118	1.1	0.0	13.0	6	18.1	0.0
12/13/09 22:30	2.0	199	3.7	0.0	0.3	173	0.5	0.0	0.3	151	0.5	0.0	0.3	118	0.5	0.0	15.0	6	21.1	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/13/09 23:00	1.9	196	3.5	0.0	0.3	170	0.5	0.0	0.4	148	0.7	0.0	0.3	116	0.5	0.0	13.0	6	18.1	0.0
12/13/09 23:30	3.1	196	5.7	0.1	0.3	171	0.5	0.0	0.6	149	1.1	0.0	0.3	118	0.5	0.0	15.0	6	21.1	0.0
12/14/09 0:00	2.1	196	3.9	0.0	0.3	170	0.5	0.0	0.5	148	0.9	0.0	0.4	116	0.7	0.0	24.0	6	34.8	0.0
12/14/09 0:30	4.1	196	7.6	0.1	0.4	170	0.7	0.0	0.3	148	0.5	0.0	0.4	116	0.7	0.0	14.0	6	19.6	0.0
12/14/09 1:00	1.9	193	3.5	0.0	0.4	168	0.7	0.0	0.4	147	0.7	0.0	0.4	116	0.7	0.0	12.0	6	16.6	0.0
12/14/09 1:30	2.0	193	3.7	0.0	0.3	168	0.5	0.0	0.4	147	0.7	0.0	0.4	116	0.7	0.0	11.0	6	15.2	0.0
12/14/09 2:00	2.1	193	3.9	0.0	0.2	168	0.4	0.0	0.6	147	1.1	0.0	0.5	116	0.9	0.0	25.0	6	36.3	0.0
12/14/09 2:30	2.0	193	3.7	0.0	0.2	168	0.4	0.0	0.4	147	0.7	0.0	0.3	116	0.5	0.0	12.0	6	16.6	0.0
12/14/09 3:00	1.9	191	3.5	0.0	0.3	166	0.5	0.0	0.3	146	0.5	0.0	0.4	116	0.7	0.0	14.0	6	19.6	0.0
12/14/09 3:30	2.0	191	3.7	0.0	0.1	166	0.2	0.0	0.4	146	0.7	0.0	0.3	116	0.5	0.0	14.0	6	19.6	0.0
12/14/09 4:00	2.0	191	3.7	0.0	0.2	166	0.4	0.0	0.3	146	0.5	0.0	0.3	116	0.5	0.0	13.0	6	18.1	0.0
12/14/09 4:30	2.0	191	3.7	0.0	0.3	166	0.5	0.0	0.4	145	0.7	0.0	0.4	114	0.7	0.0	14.0	6	19.6	0.0
12/14/09 5:00	2.1	191	3.9	0.0	0.4	166	0.7	0.0	0.3	145	0.5	0.0	0.3	114	0.5	0.0	15.0	6	21.1	0.0
12/14/09 5:30	2.1	191	3.9	0.0	0.5	166	0.9	0.0	0.3	145	0.5	0.0	0.3	114	0.5	0.0	16.0	6	22.6	0.0
12/14/09 6:00	2.2	188	4.0	0.0	0.6	164	1.1	0.0	0.3	144	0.5	0.0	0.4	114	0.7	0.0	16.0	6	22.6	0.0
12/14/09 6:30	2.1	191	3.9	0.0	0.7	166	1.3	0.0	0.4	145	0.7	0.0	0.3	114	0.5	0.0	16.0	6	22.6	0.0
12/14/09 7:00	2.0	188	3.7	0.0	0.4	164	0.7	0.0	0.3	144	0.5	0.0	0.3	114	0.5	0.0	19.0	6	27.1	0.0
12/14/09 7:30	2.0	188	3.7	0.0	0.4	164	0.7	0.0	0.3	144	0.5	0.0	0.5	114	0.9	0.0	14.0	6	19.6	0.0
12/14/09 8:00	2.0	188	3.7	0.0	0.4	164	0.6	0.0	0.3	144	0.5	0.0	0.3	114	0.5	0.0	14.0	6	19.6	0.0
12/14/09 8:30	2.0	188	3.7	0.0	0.3	164	0.6	0.0	0.3	143	0.5	0.0	0.4	112	0.7	0.0	19.0	6	27.1	0.0
12/14/09 9:00	2.0	185	3.7	0.0	0.3	162	0.5	0.0	0.5	142	0.9	0.0	0.4	112	0.7	0.0	13.0	6	18.1	0.0
12/14/09 9:30	1.9	185	3.5	0.0	0.3	162	0.5	0.0	0.3	142	0.5	0.0	0.4	112	0.7	0.0	24.0	6	34.8	0.0
12/14/09 10:00	2.1	185	3.9	0.0	0.3	162	0.5	0.0	0.3	142	0.5	0.0	0.3	112	0.5	0.0	16.0	6	22.6	0.0
12/14/09 10:30	2.0	185	3.7	0.0	0.3	162	0.6	0.0	0.4	142	0.7	0.0	0.3	112	0.5	0.0	23.0	6	33.2	0.0
12/14/09 11:00	2.0	188	3.7	0.0	0.4	164	0.6	0.0	0.3	143	0.5	0.0	0.4	112	0.7	0.0	19.0	6	27.1	0.0
12/14/09 11:30	2.2	185	4.0	0.0	0.4	162	0.7	0.0	0.3	142	0.5	0.0	0.5	112	0.9	0.0	19.0	6	27.1	0.0
12/14/09 12:00	2.0	185	3.7	0.0	0.4	161	0.7	0.0	0.3	141	0.5	0.0	0.3	111	0.5	0.0	26.0	6	37.8	0.0
12/14/09 12:30	2.1	185	3.9	0.0	0.3	161	0.5	0.0	0.3	141	0.5	0.0	0.3	111	0.5	0.0	19.0	6	27.1	0.0
12/14/09 13:00	1.9	185	3.5	0.0	0.3	161	0.5	0.0	0.3	141	0.5	0.0	0.4	111	0.7	0.0	26.0	6	37.8	0.0
12/14/09 13:30	1.9	185	3.5	0.0	0.2	161	0.4	0.0	0.3	141	0.5	0.0	0.4	111	0.7	0.0	17.0	6	24.1	0.0
12/14/09 14:00	2.0	183	3.7	0.0	0.3	159	0.5	0.0	0.6	140	1.1	0.0	0.4	111	0.7	0.0	18.0	6	25.6	0.0
12/14/09 14:30	2.1	183	3.9	0.0	0.3	159	0.5	0.0	0.3	140	0.5	0.0	0.3	111	0.5	0.0	16.0	6	22.6	0.0
12/14/09 15:00	2.2	183	4.0	0.0	0.3	159	0.5	0.0	0.4	140	0.7	0.0	0.3	111	0.5	0.0	14.0	6	19.6	0.0
12/14/09 15:30	2.0	183	3.7	0.0	0.3	159	0.5	0.0	0.4	140	0.7	0.0	0.3	111	0.5	0.0	17.0	6	24.1	0.0
12/14/09 16:00	2.0	183	3.7	0.0	0.3	159	0.5	0.0	0.3	140	0.5	0.0	0.4	111	0.7	0.0	27.0	6	39.4	0.0
12/14/09 16:30	2.0	183	3.7	0.0	0.5	159	0.9	0.0	0.3	140	0.5	0.0	0.3	111	0.5	0.0	20.0	6	28.6	0.0
12/14/09 17:00	1.9	185	3.5	0.0	0.4	161	0.7	0.0	0.3	141	0.5	0.0	0.3	111	0.5	0.0	18.0	6	25.6	0.0
12/14/09 17:30	2.1	183	3.9	0.0	0.4	159	0.7	0.0	0.6	140	1.1	0.0	0.4	111	0.7	0.0	25.0	6	36.3	0.0
12/14/09 18:00	2.1	183	3.9	0.0	0.4	160	0.6	0.0	0.4	141	0.7	0.0	0.4	112	0.7	0.0	20.0	6	28.6	0.0
12/14/09 18:30	2.2	185	4.0	0.0	0.3	162	0.5	0.0	0.5	142	0.9	0.0	0.3	112	0.5	0.0	16.0	6	22.6	0.0
12/14/09 19:00	2.2	185	4.0	0.0	0.4	162	0.7	0.0	0.4	143	0.7	0.0	0.3	114	0.5	0.0	15.0	6	21.1	0.0
12/14/09 19:30	2.2	185	4.0	0.0	0.4	163	0.7	0.0	0.7	144	1.3	0.0	0.3	116	0.5	0.0	16.0	6	22.6	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/14/09 20:00	2.0	185	3.7	0.0	0.3	164	0.5	0.0	0.6	146	1.1	0.0	0.3	119	0.5	0.0	18.0	6	25.6	0.0
12/14/09 20:30	2.2	185	4.0	0.0	0.3	165	0.5	0.0	0.6	148	1.1	0.0	0.4	123	0.7	0.0	16.0	7	22.6	0.0
12/14/09 21:00	2.3	188	4.2	0.0	0.3	169	0.5	0.0	1.0	153	1.8	0.0	0.4	128	0.7	0.0	16.0	7	22.6	0.0
12/14/09 21:30	1.9	185	3.5	0.0	0.6	169	1.1	0.0	1.1	155	2.0	0.0	0.4	134	0.7	0.0	19.0	134	7	27.1
12/14/09 22:00	2.1	188	3.9	0.0	0.4	172	0.7	0.0	1.9	159	3.5	0.0	0.4	140	0.7	0.0	20.0	7	28.6	0.0
12/14/09 22:30	2.3	188	4.2	0.0	0.6	176	1.1	0.0	2.6	165	4.8	0.0	0.4	150	0.7	0.0	23.0	8	33.2	0.0
12/14/09 23:00	2.2	193	4.0	0.0	0.6	183	1.1	0.0	2.8	174	5.2	0.1	0.4	160	0.7	0.0	49.0	9	74.2	0.0
12/14/09 23:30	2.5	196	4.6	0.1	0.6	190	1.1	0.0	2.8	185	5.2	0.1	0.5	178	0.9	0.0	100.0	9	158.2	0.1
12/15/09 0:00	2.1	199	3.9	0.0	0.7	201	1.3	0.0	3.9	202	7.3	0.1	0.6	204	1.1	0.0	170.0	11	278.0	0.2
12/15/09 0:30	5.7	204	10.7	0.1	1.6	215	2.9	0.0	5.0	224	9.3	0.1	0.8	238	1.4	0.0	260.0	12	436.5	0.3
12/15/09 1:00	2.1	216	3.9	0.0	1.0	238	1.8	0.0	4.7	256	8.8	0.1	0.8	283	1.4	0.0	300.0	15	508.2	0.4
12/15/09 1:30	2.1	225	3.9	0.0	1.7	259	3.1	0.0	4.7	288	8.8	0.1	0.8	331	1.4	0.0	500.0	17	874.3	0.8
12/15/09 2:00	2.4	237	4.4	0.1	1.9	285	3.5	0.1	5.4	325	10.1	0.2	1.5	386	2.7	0.1	290.0	19	490.2	0.5
12/15/09 2:30	2.3	259	4.2	0.1	2.1	319	3.9	0.1	5.5	370	10.3	0.2	1.3	447	2.4	0.1	270.0	22	454.4	0.6
12/15/09 3:00	2.7	279	5.0	0.1	3.4	352	6.3	0.1	6.3	415	11.8	0.3	1.0	508	1.8	0.1	280.0	25	472.3	0.7
12/15/09 3:30	2.5	306	4.6	0.1	5.1	394	9.5	0.2	9.2	468	17.4	0.5	1.1	579	2.0	0.1	190.0	29	312.9	0.5
12/15/09 4:00	2.9	335	5.4	0.1	6.3	435	11.8	0.3	17.3	520	33.2	1.0	1.0	646	1.8	0.1	200.0	32	330.4	0.6
12/15/09 4:30	2.9	374	5.4	0.1	6.9	486	13.0	0.4	28.6	581	55.4	1.8	1.4	722	2.6	0.1	210.0	35	347.9	0.7
12/15/09 5:00	3.4	433	6.3	0.2	7.9	555	14.9	0.5	23.6	657	45.5	1.7	1.6	810	2.9	0.1	150.0	39	243.4	0.5
12/15/09 5:30	3.6	531	6.7	0.2	8.1	649	15.3	0.6	24.2	748	46.7	2.0	1.4	897	2.6	0.1	190.0	43	312.9	0.8
12/15/09 6:00	4.4	641	8.2	0.3	14.2	755	27.1	1.2	18.5	852	35.5	1.7	1.4	996	2.6	0.1	170.0	48	278.0	0.7
12/15/09 6:30	6.8	770	12.8	0.6	21.1	870	40.6	2.0	15.9	955	30.4	1.6	1.5	1081	2.7	0.2	160.0	51	260.7	0.8
12/15/09 7:00	8.4	921	15.9	0.8	23.3	1006	44.9	2.5	14.2	1078	27.1	1.6	2.0	1185	3.7	0.2	150.0	56	243.4	0.8
12/15/09 7:30	10.0	1086	19.0	1.2	23.4	1158	45.1	2.9	14.8	1218	28.3	1.9	1.9	1309	3.5	0.3	170.0	62	278.0	1.0
12/15/09 8:00	14.0	1269	26.7	1.9	22.9	1324	44.1	3.3	17.4	1371	33.3	2.6	2.4	1441	4.4	0.4	170.0	67	278.0	1.1
12/15/09 8:30	16.0	1447	30.6	2.5	22.1	1476	42.6	3.5	18.4	1501	35.3	3.0	2.8	1539	5.2	0.4	220.0	72	365.6	1.5
12/15/09 9:00	22.0	1642	42.4	3.9	22.2	1647	42.8	4.0	15.6	1651	29.8	2.8	2.0	1657	3.7	0.3	250.0	77	418.7	1.8
12/15/09 9:30	28.0	1863	54.2	5.7	23.6	1828	45.5	4.7	20.1	1799	38.6	3.9	3.0	1754	5.6	0.5	230.0	81	383.2	1.7
12/15/09 10:00	28.0	2006	54.2	6.1	23.3	1966	44.9	5.0	20.5	1933	39.4	4.3	7.1	1883	13.4	1.4	590.0	87	1042.3	5.1
12/15/09 10:30	29.0	2259	56.1	7.1	24.5	2178	47.2	5.8	19.6	2109	37.7	4.5	4.6	2007	8.6	1.0	460.0	92	800.2	4.1
12/15/09 11:00	27.0	2337	52.2	6.9	25.6	2262	49.4	6.3	19.3	2200	37.1	4.6	5.1	2106	9.5	1.1	380.0	96	653.2	3.5
12/15/09 11:30	28.0	2403	54.2	7.3	26.8	2340	51.7	6.8	25.8	2287	49.8	6.4	3.5	2207	6.5	0.8	295.0	101	499.2	2.8
12/15/09 12:00	30.0	2706	58.1	8.8	27.9	2572	54.0	7.8	28.6	2460	55.4	7.7	3.3	2291	6.1	0.8	320.0	104	544.2	3.2
12/15/09 12:30	31.0	2663	60.1	9.0	29.1	2567	56.2	8.1	25.9	2486	50.0	7.0	3.4	2365	6.3	0.8	260.0	107	436.5	2.6
12/15/09 13:00	31.0	2908	60.1	9.8	30.2	2758	58.5	9.1	24.2	2631	46.7	6.9	4.5	2441	8.4	1.2	190.0	111	312.9	1.9
12/15/09 13:30	33.0	2865	64.1	10.3	31.4	2729	60.8	9.3	23.1	2614	44.5	6.5	3.7	2441	6.9	0.9	450.0	111	781.7	4.9
12/15/09 14:00	35.0	2937	68.0	11.2	32.5	2795	63.1	9.9	23.4	2675	45.1	6.8	3.4	2496	6.3	0.9	330.0	113	562.3	3.6
12/15/09 14:30	36.7	2965	71.3	11.9	31.3	2810	60.7	9.6	19.4	2680	37.3	5.6	4.1	2485	7.6	1.1	180.0	112	295.4	1.9
12/15/09 15:00	38.3	3022	74.6	12.7	29.0	2857	56.1	9.0	21.1	2717	40.6	6.2	4.3	2507	8.0	1.1	180.0	113	295.4	1.9
12/15/09 15:30	40.0	2865	77.9	12.6	27.9	2746	53.9	8.3	19.9	2646	38.2	5.7	2.9	2496	5.4	0.8	140.0	113	226.2	1.4
12/15/09 16:00	32.0	3095	62.1	10.8	26.7	2888	51.6	8.4	17.7	2714	33.9	5.2	3.6	2452	6.7	0.9	130.0	111	209.1	1.3
12/15/09 16:30	34.0	3080	66.0	11.4	25.6	2878	49.4	8.0	16.3	2708	31.2	4.7	3.2	2452	5.9	0.8	110.0	111	175.1	1.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/15/09 17:00	30.0	3080	58.1	10.1	24.4	2871	47.1	7.6	14.2	2695	27.1	4.1	2.7	2430	5.0	0.7	82.0	110	128.2	0.8
12/15/09 17:30	27.0	3051	52.2	9.0	23.3	2837	44.9	7.2	13.8	2657	26.3	3.9	2.6	2387	4.8	0.6	120.0	108	192.0	1.2
12/15/09 18:00	30.0	2979	58.1	9.7	22.2	2792	42.7	6.7	12.7	2634	24.2	3.6	2.6	2397	4.8	0.6	120.0	109	192.0	1.2
12/15/09 18:30	27.0	2979	52.2	8.7	21.0	2785	40.4	6.3	11.5	2621	21.9	3.2	2.5	2376	4.6	0.6	220.0	108	365.6	2.2
12/15/09 19:00	24.0	2951	46.3	7.7	19.9	2755	38.2	5.9	11.5	2591	21.9	3.2	2.3	2344	4.2	0.6	180.0	106	295.4	1.8
12/15/09 19:30	23.0	3008	44.3	7.5	18.7	2801	35.9	5.7	16.1	2627	30.8	4.5	2.3	2365	4.2	0.6	140.0	107	226.2	1.4
12/15/09 20:00	22.0	2880	42.4	6.9	17.6	2718	33.7	5.1	14.3	2581	27.3	4.0	2.2	2376	4.0	0.5	89.0	108	139.8	0.8
12/15/09 20:30	19.0	3008	36.5	6.2	16.4	2798	31.5	4.9	12.1	2620	23.0	3.4	2.2	2354	4.0	0.5	93.0	107	146.5	0.9
12/15/09 21:00	18.0	2706	34.5	5.2	15.3	2593	29.2	4.3	10.9	2497	20.7	2.9	2.9	2333	7.4	1.0	150.0	107	243.4	1.5
12/15/09 21:30	16.0	2865	30.6	4.9	19.3	2694	37.1	5.6	10.7	2550	20.3	2.9	2.5	2333	4.6	0.6	99.0	106	156.5	0.9
12/15/09 22:00	16.0	2865	30.6	4.9	15.9	2701	30.4	4.6	13.2	2562	25.2	3.6	2.1	2354	3.9	0.5	120.0	107	192.0	1.2
12/15/09 22:30	17.0	2937	32.6	5.4	15.6	2756	29.8	4.6	10.1	2604	19.1	2.8	1.8	2376	3.3	0.4	205.0	108	339.1	2.1
12/15/09 23:00	18.0	3051	34.5	5.9	13.6	2848	25.9	4.2	10.1	2676	19.1	2.9	3.0	2419	5.6	0.8	160.0	110	260.7	1.6
12/15/09 23:30	16.0	2880	30.6	5.0	14.8	2764	28.3	4.4	13.4	2665	25.5	3.8	2.3	2518	4.2	0.6	150.0	114	243.4	1.6
12/16/09 0:00	16.0	2836	30.6	4.9	14.8	2770	28.3	4.4	16.6	2715	31.8	4.8	2.3	2631	4.2	0.6	650.0	119	1155.2	7.7
12/16/09 0:30	16.0	2851	30.6	4.9	13.4	2817	25.5	4.0	14.7	2789	28.1	4.4	3.2	2747	5.9	0.9	740.0	124	1325.8	9.2
12/16/09 1:00	16.0	2922	30.6	5.0	16.8	2904	32.2	5.3	19.1	2889	36.7	6.0	4.0	2866	7.4	1.2	300.0	129	508.2	3.7
12/16/09 1:30	15.0	2880	28.7	4.6	16.6	2927	31.8	5.2	33.2	2966	64.5	10.7	7.2	3026	13.6	2.3	190.0	135	312.9	2.4
12/16/09 2:00	15.0	3198	28.7	5.2	18.1	3183	34.7	6.2	32.8	3171	63.7	11.3	4.8	3152	9.0	1.6	180.0	141	295.4	2.3
12/16/09 2:30	18.0	3124	34.5	6.1	25.2	3146	48.7	8.6	28.3	3163	54.8	9.7	5.8	3190	10.9	1.9	120.0	142	192.0	1.5
12/16/09 3:00	23.0	3258	44.3	8.1	38.3	3282	74.6	13.8	27.0	3303	52.2	9.7	5.9	3333	11.1	2.1	100.0	148	158.2	1.3
12/16/09 3:30	26.0	3349	50.2	9.5	36.7	3331	71.4	13.4	23.7	3316	45.7	8.5	6.6	3294	12.4	2.3	99.0	147	156.5	1.3
12/16/09 4:00	31.0	3288	60.1	11.1	35.1	3278	68.3	12.6	22.2	3268	42.8	7.9	8.0	3255	15.1	2.8	86.0	145	134.8	1.1
12/16/09 4:30	40.0	3567	77.9	15.6	33.5	3475	65.1	12.7	18.6	3397	35.7	6.8	7.8	3281	14.7	2.7	78.0	146	121.5	1.0
12/16/09 5:00	39.0	3426	76.0	14.6	32.0	3354	62.0	11.7	20.2	3294	38.8	7.2	6.5	3203	12.2	2.2	72.0	143	111.6	0.9
12/16/09 5:30	38.0	3811	74.0	15.8	30.4	3599	58.8	11.9	19.7	3420	37.8	7.3	4.3	3152	8.0	1.4	62.0	141	95.2	0.8
12/16/09 6:00	39.0	3551	76.0	15.2	28.8	3382	55.7	10.6	15.3	3239	29.2	5.3	3.8	3026	7.1	1.2	69.0	135	106.7	0.8
12/16/09 6:30	37.0	3535	72.0	14.3	27.2	3355	52.6	9.9	13.2	3203	25.2	4.5	9.9	2976	18.8	3.1	56.0	133	85.5	0.6
12/16/09 7:00	34.0	3349	66.0	12.4	25.6	3194	49.4	8.9	12.4	3063	23.6	4.1	4.3	2866	8.0	1.3	54.0	129	82.2	0.6
12/16/09 7:30	29.0	3582	56.1	11.3	19.0	3336	36.5	6.8	10.8	3129	20.5	3.6	3.5	2818	6.5	1.0	53.0	127	80.6	0.6
12/16/09 8:00	27.0	3395	52.2	10.0	19.0	3190	36.5	6.5	11.0	3018	20.9	3.5	2.4	2759	4.4	0.7	54.0	124	82.2	0.6
12/16/09 8:30	27.0	3288	52.2	9.6	19.0	3084	36.5	6.3	10.9	2912	20.7	3.4	2.1	2654	3.9	0.6	62.0	120	95.2	0.6
12/16/09 9:00	23.0	3519	44.3	8.8	16.6	3215	31.7	5.7	9.3	2959	17.6	2.9	2.1	2574	3.9	0.6	47.0	116	71.0	0.5
12/16/09 9:30	22.0	3198	42.4	7.6	14.1	2972	26.9	4.5	9.2	2782	17.4	2.7	1.9	2496	3.5	0.5	49.0	113	74.2	0.5
12/16/09 10:00	21.0	3243	40.4	7.4	13.8	2978	26.3	4.4	8.7	2754	16.4	2.5	1.8	2419	3.3	0.4	40.0	110	59.8	0.4
12/16/09 10:30	20.0	3080	38.4	6.7	12.8	2843	24.4	3.9	8.0	2643	15.1	2.2	1.8	2344	3.3	0.4	46.0	106	69.4	0.4
12/16/09 11:00	18.0	3080	34.5	6.0	11.8	2819	22.4	3.6	9.2	2599	17.4	2.5	1.8	2270	3.3	0.4	47.0	103	71.0	0.4
12/16/09 11:30	15.0	3022	28.7	4.9	12.1	2763	23.0	3.6	6.7	2545	12.6	1.8	1.8	2218	3.3	0.4	41.0	101	61.4	0.3
12/16/09 12:00	14.0	2894	26.7	4.3	11.1	2663	21.1	3.2	6.9	2468	13.0	1.8	4.3	2176	8.0	1.0	36.0	99	53.5	0.3
12/16/09 12:30	14.0	2965	26.7	4.5	12.3	2688	23.4	3.5	7.4	2455	13.9	1.9	3.0	2106	5.6	0.7	36.0	96	53.5	0.3
12/16/09 13:00	13.0	2851	24.8	4.0	10.7	2591	20.3	3.0	6.0	2373	11.3	1.5	1.9	2046	3.5	0.4	33.0	94	48.7	0.3
12/16/09 13:30	12.0	2763	22.8	3.5	11.1	2520	21.1	3.0	6.0	2315	11.3	1.5	2.2	2007	4.0	0.5	31.0	92	45.6	0.2

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/16/09 14:00	13.0	2763	24.8	3.8	8.6	2507	16.3	2.3	7.0	2292	13.2	1.7	1.9	1968	3.5	0.4	34.0	90	50.3	0.3
12/16/09 14:30	12.0	2649	22.8	3.4	9.7	2421	18.4	2.5	5.3	2228	9.9	1.2	1.8	1940	3.3	0.4	34.0	89	50.3	0.3
12/16/09 15:00	11.0	2593	20.9	3.0	8.8	2374	16.6	2.2	6.0	2189	11.3	1.4	1.8	1911	3.3	0.4	42.0	88	63.0	0.3
12/16/09 15:30	10.0	2692	19.0	2.9	8.2	2434	15.5	2.1	5.5	2217	10.3	1.3	1.8	1892	3.3	0.4	74.0	87	114.9	0.6
12/16/09 16:00	11.0	2511	20.9	2.9	8.8	2315	16.6	2.2	5.7	2149	10.7	1.3	1.8	1902	3.3	0.4	46.0	87	69.4	0.3
12/16/09 16:30	11.0	2678	20.9	3.1	8.6	2443	16.3	2.2	6.1	2245	11.4	1.4	1.6	1949	2.9	0.3	83.0	89	129.8	0.7
12/16/09 17:00	9.5	2649	18.0	2.7	7.6	2442	14.3	2.0	6.0	2268	11.3	1.4	1.5	2007	2.7	0.3	120.0	92	192.0	1.0
12/16/09 17:30	10.0	2524	19.0	2.7	7.1	2370	13.4	1.8	5.9	2241	11.1	1.4	1.7	2046	3.1	0.4	37.0	94	55.0	0.3
12/16/09 18:00	8.6	2470	16.3	2.3	7.9	2356	14.9	2.0	7.2	2260	13.6	1.7	1.9	2116	3.5	0.4	34.0	97	50.3	0.3
12/16/09 18:30	8.3	2470	15.7	2.2	8.7	2392	16.4	2.2	6.7	2326	12.6	1.6	1.7	2228	3.1	0.4	44.0	101	66.2	0.4
12/16/09 19:00	8.3	2635	15.7	2.3	9.3	2521	17.6	2.5	5.8	2425	10.9	1.5	1.9	2280	3.5	0.4	44.0	104	66.2	0.4
12/16/09 19:30	9.0	2621	17.0	2.5	7.9	2522	14.9	2.1	6.4	2438	12.0	1.6	1.8	2312	3.3	0.4	100.0	105	158.2	0.9
12/16/09 20:00	9.2	2621	17.4	2.6	8.5	2539	16.1	2.3	6.9	2469	13.0	1.8	1.9	2365	3.5	0.5	78.0	107	121.5	0.7
12/16/09 20:30	10.0	2692	19.0	2.9	8.3	2593	15.7	2.3	8.4	2511	15.9	2.2	1.8	2387	3.3	0.4	32.0	108	47.2	0.3
12/16/09 21:00	10.0	2749	19.0	2.9	9.6	2650	18.2	2.7	10.1	2566	19.1	2.8	1.7	2441	3.1	0.4	32.0	111	47.2	0.3
12/16/09 21:30	9.8	2865	18.6	3.0	9.0	2754	17.0	2.6	7.9	2659	14.9	2.2	4.7	2518	8.8	1.2	100.0	114	158.2	1.0
12/16/09 22:00	9.2	3022	17.4	3.0	9.6	2867	18.2	2.9	7.9	2737	14.9	2.3	2.6	2541	4.8	0.7	31.0	115	45.6	0.3
12/16/09 22:30	9.0	2894	17.0	2.8	12.1	2784	23.0	3.6	8.5	2691	16.1	2.4	2.2	2552	4.0	0.6	29.0	115	42.5	0.3
12/16/09 23:00	11.0	2951	20.9	3.5	9.7	2822	18.4	2.9	8.3	2714	15.7	2.4	3.4	2552	6.3	0.9	32.0	116	47.2	0.3
12/16/09 23:30	11.0	3080	20.9	3.6	9.6	2918	18.2	3.0	7.7	2780	14.5	2.3	2.2	2574	4.0	0.6	32.0	116	47.2	0.3
12/17/09 00:00	12.0	3139	22.8	4.0	11.4	2954	21.7	3.6	7.9	2797	14.9	2.3	3.1	2563	5.7	0.8	26.0	116	37.8	0.2
12/17/09 03:30	12.0	2951	22.8	3.8	10.6	2808	20.1	3.2	7.6	2688	14.3	2.2	2.6	2507	4.8	0.7	36.0	113	53.5	0.3
12/17/09 1:00	11.0	3080	20.9	3.6	9.8	2889	18.6	3.0	6.5	2727	12.2	1.9	2.2	2485	4.0	0.6	26.0	112	37.8	0.2
12/17/09 1:30	12.0	2994	22.8	3.8	9.0	2826	17.0	2.7	6.7	2685	12.6	1.9	2.4	2474	4.4	0.6	24.0	110	33.2	0.2
12/17/09 2:00	12.0	3095	22.8	4.0	10.0	2881	19.0	3.1	7.1	2701	13.4	2.0	2.1	2430	3.9	0.5	23.0	110	33.2	0.2
12/17/09 2:30	11.0	2994	20.9	3.5	8.8	2795	16.6	2.6	6.6	2627	12.4	1.8	2.2	2376	4.0	0.5	25.0	108	36.3	0.2
12/17/09 3:00	11.0	2979	20.9	3.5	8.5	2771	16.1	2.5	6.8	2596	12.8	1.9	1.9	2333	3.5	0.5	24.0	106	34.8	0.2
12/17/09 3:30	11.0	2979	20.9	3.5	8.0	2754	15.1	2.3	5.7	2565	10.7	1.5	1.9	2280	3.5	0.4	24.0	104	34.8	0.2
12/17/09 4:00	10.0	2865	19.0	3.1	8.3	2670	15.7	2.4	5.0	2506	9.3	1.3	1.8	2259	3.3	0.4	23.0	103	33.2	0.2
12/17/09 4:30	10.0	2965	19.0	3.2	8.0	2724	15.1	2.3	5.3	2522	9.9	1.4	1.9	2218	3.5	0.4	22.0	101	31.7	0.2
12/17/09 5:00	9.7	2908	18.4	3.0	7.2	2666	13.6	2.0	5.3	2462	9.9	1.4	1.7	2156	3.1	0.4	21.0	98	30.2	0.2
12/17/09 5:30	8.6	2836	16.3	2.6	6.8	2614	12.8	1.9	5.7	2427	10.7	1.5	1.9	2146	3.5	0.4	22.0	98	31.7	0.2
12/17/09 6:00	8.2	2894	15.5	2.5	6.7	2640	12.6	1.9	5.2	2426	9.7	1.3	1.6	2106	2.9	0.3	22.0	96	31.7	0.2
12/17/09 6:30	7.8	2706	14.7	2.2	6.7	2503	12.6	1.8	4.5	2332	8.4	1.1	1.6	2076	2.9	0.3	22.0	95	31.7	0.2
12/17/09 7:00	8.5	2778	16.1	2.5	6.1	2542	11.4	1.6	4.9	2344	9.2	1.2	1.6	2046	2.9	0.3	32.0	94	47.2	0.2
12/17/09 7:30	7.6	2692	14.3	2.2	6.2	2471	11.6	1.6	4.7	2286	8.8	1.1	1.4	2007	2.6	0.3	42.0	92	63.0	0.3
12/17/09 8:00	7.5	2621	14.1	2.1	6.9	2411	13.0	1.8	4.9	2234	9.2	1.1	1.5	1968	2.7	0.3	47.0	90	71.0	0.4
12/17/09 8:30	7.1	2763	13.4	2.1	6.0	2504	11.3	1.6	4.9	2286	9.2	1.2	1.3	1959	2.4	0.3	63.0	90	96.9	0.5
12/17/09 9:00	7.3	2621	13.7	2.0	5.5	2405	10.3	1.4	5.7	2222	10.7	1.3	1.2	1949	2.2	0.2	70.0	89	108.3	0.5
12/17/09 9:30	6.2	2735	11.6	1.8	5.9	2482	11.1	1.5	5.3	2269	9.9	1.3	1.4	1949	2.6	0.3	57.0	89	87.1	0.4
12/17/09 10:00	8.0	2692	15.1	2.3	5.1	2453	9.5	1.3	4.9	2251	9.2	1.2	1.7	1949	3.1	0.3	48.0	89	72.6	0.4
12/17/09 10:30	6.2	2649	11.6	1.7	6.4	2409	12.0	1.6	5.4	2206	10.1	1.3	1.7	1902	3.1	0.3	56.0	87	85.5	0.4

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/17/09 11:00	6.3	2524	11.8	1.7	6.5	2318	12.2	1.6	5.3	2144	9.9	1.2	1.3	1883	2.4	0.3	65.0	87	100.1	0.5
12/17/09 11:30	8.8	2621	16.6	2.5	6.9	2380	13.0	1.7	5.2	2178	9.7	1.2	1.5	1873	2.7	0.3	38.0	86	56.6	0.3
12/17/09 12:00	6.5	2607	12.2	1.8	6.2	2365	11.6	1.5	5.7	2161	10.7	1.3	1.3	1855	2.4	0.2	32.0	85	47.2	0.2
12/17/09 12:30	7.1	2376	13.4	1.8	5.9	2199	11.1	1.4	5.6	2050	10.5	1.2	1.4	1827	2.6	0.3	27.0	84	39.4	0.2
12/17/09 13:00	6.3	2538	11.8	1.7	5.7	2306	10.7	1.4	3.9	2111	7.3	0.9	1.3	1818	2.4	0.2	56.0	84	85.5	0.4
12/17/09 13:30	7.1	2621	13.4	2.0	5.1	2357	9.5	1.3	4.2	2134	7.8	0.9	1.3	1800	2.4	0.2	61.0	83	93.6	0.4
12/17/09 14:00	6.9	2511	13.0	1.8	6.3	2279	11.8	1.5	3.8	2083	7.1	0.8	1.4	1791	2.6	0.3	39.0	83	58.2	0.3
12/17/09 14:30	6.9	2429	13.0	1.8	6.2	2212	11.6	1.4	4.5	2029	8.4	1.0	1.3	1754	2.4	0.2	31.0	81	45.6	0.2
12/17/09 15:00	6.0	2552	11.3	1.6	4.6	2289	8.6	1.1	4.0	2068	7.4	0.9	1.3	1737	2.4	0.2	30.0	80	44.0	0.2
12/17/09 15:30	6.2	2416	11.6	1.6	4.8	2192	9.0	1.1	3.6	2002	6.7	0.8	1.2	1719	2.2	0.2	29.0	79	42.5	0.2
12/17/09 16:00	6.6	2593	12.4	1.8	4.8	2312	9.0	1.2	4.4	2075	8.2	1.0	1.2	1719	2.2	0.2	27.0	79	39.4	0.2
12/17/09 16:30	6.0	2416	11.3	1.5	4.9	2175	9.2	1.1	3.8	1971	7.1	0.8	1.6	1666	2.9	0.3	27.0	77	39.4	0.2
12/17/09 17:00	5.3	2298	9.9	1.3	5.2	2089	9.7	1.1	3.8	1913	7.1	0.8	1.2	1649	2.2	0.2	25.0	76	36.3	0.2
12/17/09 17:30	7.0	2363	13.2	1.7	4.4	2133	8.2	1.0	2.8	1939	5.2	0.6	1.4	1649	2.6	0.2	31.0	76	45.6	0.2
12/17/09 18:00	6.7	2376	12.6	1.7	4.5	2134	8.4	1.0	3.2	1929	5.9	0.6	1.3	1623	2.4	0.2	29.0	75	42.5	0.2
12/17/09 18:30	6.1	2376	11.4	1.5	4.4	2128	8.3	1.0	3.2	1919	5.9	0.6	1.4	1606	2.6	0.2	35.0	75	51.9	0.2
12/17/09 19:00	5.5	2324	10.3	1.3	4.4	2087	8.1	1.0	3.8	1888	7.1	0.7	1.3	1589	2.4	0.2	34.0	74	50.3	0.2
12/17/09 19:30	5.3	2311	9.9	1.3	4.3	2073	8.0	0.9	3.1	1872	5.7	0.6	1.4	1572	2.6	0.2	27.0	73	39.4	0.2
12/17/09 20:00	5.3	2259	9.9	1.3	4.2	2038	7.9	0.9	3.6	1851	6.7	0.7	1.3	1572	2.4	0.2	26.0	73	37.8	0.2
12/17/09 20:30	5.2	2246	9.7	1.2	4.2	2021	7.8	0.9	3.8	1831	7.1	0.7	1.3	1547	2.4	0.2	28.0	72	40.9	0.2
12/17/09 21:00	4.8	2233	9.0	1.1	4.1	1999	7.6	0.9	3.2	1802	5.9	0.6	1.1	1506	2.0	0.2	25.0	70	36.3	0.1
12/17/09 21:30	5.4	2272	10.1	1.3	4.0	2020	7.5	0.9	2.8	1808	5.2	0.5	1.5	1489	2.7	0.2	25.0	69	36.3	0.1
12/17/09 22:00	5.8	2169	10.9	1.3	4.0	1945	7.4	0.8	2.8	1756	5.2	0.5	1.6	1473	2.9	0.2	26.0	69	37.8	0.1
12/17/09 22:30	5.1	2195	9.5	1.2	3.9	1957	7.3	0.8	2.8	1757	5.2	0.5	1.2	1457	2.2	0.2	26.0	68	37.8	0.1
12/17/09 23:00	5.1	2195	9.5	1.2	3.8	1950	7.1	0.8	4.7	1743	8.8	0.9	1.3	1433	2.4	0.2	27.0	67	39.4	0.1
12/17/09 23:30	5.7	2144	10.7	1.3	3.8	1907	7.0	0.8	2.6	1708	4.8	0.5	1.1	1409	2.0	0.2	27.0	66	39.4	0.1
12/18/09 0:00	4.8	2195	9.0	1.1	3.7	1939	6.9	0.7	2.6	1724	4.8	0.5	1.2	1401	2.2	0.2	25.0	66	36.3	0.1
12/18/09 0:30	4.8	2068	9.0	1.0	3.4	1846	6.2	0.6	3.1	1659	5.7	0.5	0.9	1378	1.6	0.1	26.0	65	37.8	0.1
12/18/09 1:00	4.6	2055	8.6	1.0	3.0	1835	5.6	0.6	2.5	1649	4.6	0.4	1.0	1370	1.8	0.1	26.0	64	37.8	0.1
12/18/09 1:30	4.7	2043	8.8	1.0	2.7	1819	5.0	0.5	2.8	1630	5.2	0.5	1.0	1347	1.8	0.1	24.0	63	34.8	0.1
12/18/09 2:00	4.2	1957	7.8	0.9	3.6	1753	6.7	0.7	3.6	1582	6.7	0.6	1.3	1324	2.4	0.2	25.0	62	36.3	0.1
12/18/09 2:30	11.0	2068	20.9	2.4	2.9	1821	5.4	0.5	2.8	1613	5.2	0.5	1.1	1302	2.0	0.1	24.0	61	34.8	0.1
12/18/09 3:00	4.3	1945	8.0	0.9	3.5	1740	6.5	0.6	2.8	1568	5.2	0.5	1.0	1309	1.8	0.1	26.0	62	37.8	0.1
12/18/09 3:30	4.5	2006	8.4	0.9	3.8	1772	7.1	0.7	2.1	1575	3.9	0.3	1.1	1279	2.0	0.1	25.0	60	36.3	0.1
12/18/09 4:00	3.9	1917	7.3	0.8	3.0	1709	5.6	0.5	2.4	1534	4.4	0.4	1.0	1272	1.8	0.1	24.0	60	34.8	0.1
12/18/09 4:30	4.2	1876	7.8	0.8	3.0	1677	5.5	0.5	2.4	1509	4.4	0.4	1.3	1257	2.4	0.2	24.0	59	34.8	0.1
12/18/09 5:00	4.1	1945	7.6	0.8	2.9	1716	5.4	0.5	2.6	1524	4.8	0.4	1.1	1235	2.0	0.1	26.0	58	37.8	0.1
12/18/09 5:30	4.6	1957	8.6	0.9	2.6	1722	4.8	0.5	2.2	1524	4.0	0.3	1.1	1228	2.0	0.1	25.0	58	36.3	0.1
12/18/09 6:00	4.0	1876	7.4	0.8	3.5	1658	6.5	0.6	2.2	1475	4.0	0.3	1.2	1199	2.2	0.1	24.0	57	34.8	0.1
12/18/09 6:30	3.4	1849	6.3	0.7	3.4	1638	6.3	0.6	2.4	1459	4.4	0.4	1.1	1192	2.0	0.1	24.0	56	34.8	0.1
12/18/09 7:00	3.5	1796	6.5	0.7	3.3	1599	6.2	0.6	1.9	1434	3.5	0.3	1.3	1185	2.4	0.2	28.0	56	40.9	0.1
12/18/09 7:30	4.1	1783	7.6	0.8	3.3	1586	6.0	0.5	1.8	1420	3.3	0.3	1.3	1171	2.4	0.2	27.0	55	39.4	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/18/09 8:00	3.8	1796	7.1	0.7	3.2	1584	5.9	0.5	2.0	1404	3.7	0.3	1.1	1136	2.0	0.1	28.0	54	40.9	0.1
12/18/09 8:30	3.3	1783	6.1	0.6	3.1	1577	5.7	0.5	6.9	1403	13.0	1.0	1.0	1143	1.8	0.1	29.0	54	42.5	0.1
12/18/09 9:00	3.5	1757	6.5	0.6	3.5	1555	6.5	0.6	2.2	1384	4.0	0.3	1.1	1129	2.0	0.1	27.0	54	39.4	0.1
12/18/09 9:30	3.7	1744	6.9	0.7	3.9	1541	7.3	0.6	3.2	1371	5.9	0.3	1.2	1115	2.2	0.1	27.0	53	39.4	0.1
12/18/09 10:00	3.2	1718	5.9	0.6	3.3	1520	6.1	0.5	1.7	1352	3.1	0.2	1.0	1102	1.8	0.1	30.0	52	44.0	0.1
12/18/09 10:30	3.1	1693	5.7	0.5	2.7	1500	5.0	0.4	1.8	1338	3.3	0.2	1.0	1095	1.8	0.1	32.0	52	47.2	0.1
12/18/09 11:00	3.2	1680	5.9	0.6	2.0	1485	3.7	0.3	1.8	1321	3.3	0.2	0.9	1075	1.6	0.1	30.0	51	44.0	0.1
12/18/09 11:30	3.0	1667	5.6	0.5	2.0	1472	3.7	0.3	1.7	1308	3.1	0.2	1.0	1061	1.8	0.1	30.0	50	44.0	0.1
12/18/09 12:00	2.9	1629	5.4	0.5	2.0	1444	3.7	0.3	1.6	1288	2.9	0.2	1.1	1055	2.0	0.1	29.0	50	42.5	0.1
12/18/09 12:30	3.2	1629	5.9	0.5	2.0	1440	3.7	0.3	1.8	1280	3.3	0.2	0.9	1041	1.6	0.1	32.0	50	47.2	0.1
12/18/09 13:00	3.4	1604	6.3	0.6	2.1	1414	3.9	0.3	1.7	1255	3.1	0.2	0.9	1015	1.6	0.1	29.0	48	42.5	0.1
12/18/09 13:30	4.0	1591	7.4	0.7	2.2	1408	4.0	0.3	1.7	1254	3.1	0.2	0.9	1022	1.6	0.1	32.0	49	47.2	0.1
12/18/09 14:00	3.0	1579	5.6	0.5	2.3	1393	4.2	0.3	1.5	1237	2.7	0.2	1.0	1003	1.8	0.1	30.0	48	44.0	0.1
12/18/09 14:30	2.9	1604	5.4	0.5	2.4	1410	4.4	0.4	1.7	1247	3.1	0.2	1.0	1003	1.8	0.1	31.0	48	45.6	0.1
12/18/09 15:00	2.7	1542	5.0	0.4	2.3	1362	4.2	0.3	3.0	1211	5.6	0.4	1.0	983	1.8	0.1	30.0	47	44.0	0.1
12/18/09 15:30	3.1	1530	5.7	0.5	2.2	1350	4.0	0.3	1.5	1198	2.7	0.2	0.9	971	1.6	0.1	32.0	46	47.2	0.1
12/18/09 16:00	3.2	1518	5.9	0.5	2.1	1340	3.9	0.3	1.3	1190	2.4	0.2	1.0	964	1.8	0.1	32.0	46	47.2	0.1
12/18/09 16:30	6.3	1506	11.8	1.0	1.8	1330	3.3	0.2	1.4	1181	2.6	0.2	0.9	958	1.6	0.1	32.0	46	47.2	0.1
12/18/09 17:00	2.7	1482	5.0	0.4	1.7	1311	3.1	0.2	1.5	1168	2.7	0.2	1.0	952	1.8	0.1	33.0	46	48.7	0.1
12/18/09 17:30	2.4	1518	4.4	0.4	1.9	1334	3.5	0.3	1.5	1179	2.7	0.2	1.2	946	2.2	0.1	33.0	45	48.7	0.1
12/18/09 18:00	2.6	1506	4.8	0.4	1.9	1326	3.5	0.3	1.8	1174	3.3	0.2	0.9	946	1.6	0.1	35.0	45	51.9	0.1
12/18/09 18:30	2.4	1482	4.4	0.4	1.9	1305	3.5	0.3	1.7	1157	3.1	0.2	1.5	933	2.7	0.1	33.0	45	48.7	0.1
12/18/09 19:00	3.0	1458	5.6	0.5	2.0	1285	3.7	0.3	1.5	1140	2.7	0.2	1.0	921	1.8	0.1	37.0	44	55.0	0.1
12/18/09 19:30	2.8	1424	5.2	0.4	2.0	1258	3.6	0.3	1.6	1118	2.9	0.2	1.0	909	1.8	0.1	35.0	44	51.9	0.1
12/18/09 20:00	2.6	1458	4.8	0.4	1.9	1280	3.6	0.3	1.5	1129	2.7	0.2	0.9	903	1.6	0.1	33.0	43	48.7	0.1
12/18/09 20:30	2.2	1401	4.0	0.3	1.9	1237	3.5	0.2	1.5	1098	2.7	0.2	0.8	891	1.4	0.1	33.0	43	48.7	0.1
12/18/09 21:00	2.7	1424	5.0	0.4	1.9	1252	3.5	0.2	1.7	1108	3.1	0.2	1.0	891	1.8	0.1	33.0	43	48.7	0.1
12/18/09 21:30	2.6	1401	4.8	0.4	1.9	1233	3.4	0.2	1.7	1091	3.1	0.2	0.9	879	1.6	0.1	31.0	42	45.6	0.1
12/18/09 22:00	3.2	1378	5.9	0.5	1.8	1219	3.3	0.2	1.7	1086	3.1	0.2	0.9	885	1.6	0.1	32.0	43	47.2	0.1
12/18/09 22:30	2.7	1367	5.0	0.4	1.8	1208	3.3	0.2	1.4	1074	2.6	0.2	0.9	873	1.6	0.1	30.0	42	44.0	0.1
12/18/09 23:00	2.3	1356	4.2	0.3	1.8	1199	3.2	0.2	1.7	1066	3.1	0.2	0.9	867	1.6	0.1	35.5	42	52.7	0.1
12/18/09 23:30	2.5	1367	4.6	0.4	1.7	1202	3.2	0.2	1.5	1064	2.7	0.2	0.9	856	1.6	0.1	34.0	41	50.3	0.1
12/19/09 0:00	2.8	1345	5.2	0.4	1.7	1187	3.1	0.2	1.4	1055	2.6	0.2	1.0	856	1.8	0.1	31.0	41	45.6	0.1
12/19/09 0:30	2.4	1345	4.4	0.3	1.7	1185	3.1	0.2	1.8	1051	3.3	0.2	0.9	850	1.6	0.1	31.0	41	45.6	0.1
12/19/09 1:00	2.8	1345	5.2	0.4	1.7	1180	3.0	0.2	1.9	1041	3.5	0.2	1.1	832	2.0	0.1	32.0	40	47.2	0.1
12/19/09 1:30	2.2	1356	4.0	0.3	1.6	1191	3.0	0.2	1.5	1052	2.7	0.2	0.8	844	1.4	0.1	30.0	41	44.0	0.1
12/19/09 2:00	2.7	1323	5.0	0.4	1.6	1167	2.9	0.2	1.5	1035	2.7	0.2	0.8	838	1.4	0.1	35.0	40	51.9	0.1
12/19/09 2:30	2.4	1312	4.4	0.3	1.6	1156	2.9	0.2	2.0	1024	3.7	0.2	0.9	827	1.6	0.1	42.0	40	63.0	0.1
12/19/09 3:00	2.2	1290	4.0	0.3	1.5	1141	2.8	0.2	1.4	1015	2.6	0.1	0.9	827	1.6	0.1	35.0	40	51.9	0.1
12/19/09 3:30	3.2	1290	5.9	0.4	1.5	1141	2.8	0.2	1.9	1015	3.5	0.2	0.9	827	1.6	0.1	39.0	40	58.2	0.1
12/19/09 4:00	2.3	1290	4.2	0.3	1.5	1137	2.7	0.2	1.4	1009	2.6	0.1	0.8	815	1.4	0.1	46.0	39	69.4	0.2
12/19/09 4:30	2.4	1312	4.4	0.3	1.5	1156	2.7	0.2	2.0	1024	3.7	0.2	0.9	827	1.6	0.1	46.0	40	69.4	0.2

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/19/09 5:00	2.3	1334	4.2	0.3	1.4	1170	2.6	0.2	1.7	1033	3.1	0.2	0.8	827	1.4	0.1	40.0	40	59.8	0.1
12/19/09 5:30	2.5	1323	4.6	0.3	1.4	1161	2.6	0.2	1.7	1025	3.1	0.2	1.0	821	1.8	0.1	89.0	40	139.8	0.3
12/19/09 6:00	2.3	1280	4.2	0.3	1.4	1137	2.6	0.2	2.0	1018	3.7	0.2	0.9	838	1.6	0.1	120.0	40	192.0	0.4
12/19/09 6:30	3.2	1290	5.9	0.4	2.5	1143	4.6	0.3	2.3	1019	4.2	0.2	1.0	832	1.8	0.1	100.0	40	158.2	0.4
12/19/09 7:00	2.7	1290	5.0	0.4	1.6	1145	2.9	0.2	1.7	1022	3.1	0.2	0.8	838	1.4	0.1	140.0	40	226.2	0.5
12/19/09 7:30	2.4	1290	4.4	0.3	1.9	1143	3.5	0.2	2.5	1029	4.6	0.3	0.9	832	1.6	0.1	150.0	40	243.4	0.5
12/19/09 8:00	2.3	1290	4.2	0.3	1.9	1148	3.5	0.2	3.9	1029	7.3	0.4	0.9	850	1.6	0.1	99.0	41	156.5	0.4
12/19/09 8:30	2.2	1301	4.0	0.3	2.3	1159	4.2	0.3	4.2	1040	7.8	0.5	0.9	861	1.6	0.1	110.0	41	175.1	0.4
12/19/09 9:00	2.3	1323	4.2	0.3	2.0	1178	3.7	0.2	4.9	1056	9.2	0.5	1.0	873	1.8	0.1	74.0	42	114.9	0.3
12/19/09 9:30	2.9	1312	5.4	0.4	2.8	1169	5.2	0.3	4.7	1048	8.8	0.5	0.9	867	1.6	0.1	62.0	42	95.2	0.2
12/19/09 10:00	2.4	1334	4.4	0.3	4.3	1191	8.0	0.5	3.7	1071	6.9	0.4	0.9	891	1.6	0.1	78.0	43	121.5	0.3
12/19/09 10:30	2.5	1356	4.6	0.4	3.6	1206	6.7	0.5	3.2	1080	5.9	0.4	0.8	891	1.4	0.1	89.0	43	139.8	0.3
12/19/09 11:00	2.3	1345	4.2	0.3	4.1	1203	7.6	0.5	3.5	1083	6.5	0.4	0.8	903	1.4	0.1	81.0	43	126.5	0.3
12/19/09 11:30	2.5	1345	4.6	0.3	3.7	1206	6.9	0.5	3.2	1090	5.9	0.4	0.9	915	1.6	0.1	71.0	44	110.0	0.3
12/19/09 12:00	2.9	1356	5.4	0.4	3.3	1208	6.1	0.4	2.6	1084	4.8	0.3	0.9	897	1.6	0.1	58.0	43	88.7	0.2
12/19/09 12:30	3.1	1378	5.7	0.4	3.1	1231	5.7	0.4	3.0	1107	5.6	0.3	0.8	921	1.4	0.1	54.0	44	82.2	0.2
12/19/09 13:00	3.8	1389	7.1	0.6	2.8	1237	5.2	0.4	2.6	1108	4.8	0.3	0.8	915	1.4	0.1	45.0	44	67.8	0.2
12/19/09 13:30	3.9	1401	7.3	0.6	2.5	1248	4.6	0.3	2.9	1120	5.4	0.3	1.1	927	2.0	0.1	47.0	44	71.0	0.2
12/19/09 14:00	4.7	1401	8.8	0.7	3.1	1248	5.7	0.4	2.3	1120	4.2	0.3	0.8	927	1.4	0.1	50.0	44	75.8	0.2
12/19/09 14:30	4.5	1378	8.4	0.7	3.1	1237	5.7	0.4	1.7	1118	3.1	0.2	0.8	940	1.4	0.1	51.0	45	77.4	0.2
12/19/09 15:00	4.2	1412	7.8	0.6	3.1	1254	5.7	0.4	2.0	1121	3.7	0.2	0.9	921	1.6	0.1	47.0	44	71.0	0.2
12/19/09 15:30	3.2	1435	5.9	0.5	2.5	1275	4.4	0.3	1.6	1141	2.9	0.2	0.8	940	1.4	0.1	42.0	45	63.0	0.2
12/19/09 16:00	2.8	1447	5.2	0.4	2.5	1281	4.6	0.3	2.2	1142	4.0	0.3	0.9	933	1.6	0.1	48.0	45	72.6	0.2
12/19/09 16:30	3.2	1389	5.9	0.5	2.5	1239	4.6	0.3	1.8	1112	3.3	0.2	0.8	921	1.4	0.1	48.0	44	80.6	0.2
12/19/09 17:00	3.0	1424	5.6	0.4	2.4	1262	4.3	0.3	1.7	1126	3.1	0.2	0.8	921	1.4	0.1	44.0	44	72.6	0.2
12/19/09 17:30	2.7	1424	5.0	0.4	2.1	1262	3.8	0.3	1.4	1126	2.6	0.2	0.8	921	1.4	0.1	62.0	44	66.2	0.2
12/19/09 18:00	3.0	1412	5.6	0.4	2.3	1254	4.1	0.3	1.5	1121	2.7	0.2	0.9	921	1.6	0.1	46.0	44	95.2	0.2
12/19/09 18:30	2.3	1424	4.2	0.3	1.9	1266	3.5	0.2	1.5	1133	2.7	0.2	0.8	933	1.4	0.1	46.0	45	69.4	0.2
12/19/09 19:00	2.2	1401	4.0	0.3	2.0	1244	3.6	0.3	1.7	1113	3.1	0.2	1.0	915	1.8	0.1	42.0	44	63.0	0.2
12/19/09 19:30	2.3	1412	4.2	0.3	1.9	1250	3.5	0.2	1.5	1114	2.7	0.2	0.8	909	1.4	0.1	46.0	44	69.4	0.2
12/19/09 20:00	2.0	1389	3.7	0.3	1.9	1235	3.5	0.2	1.8	1104	3.3	0.2	0.8	909	1.4	0.1	53.0	44	80.6	0.2
12/19/09 20:30	2.3	1389	4.2	0.3	2.7	1233	4.9	0.3	3.0	1101	5.6	0.3	1.0	903	1.8	0.1	40.0	43	59.8	0.1
12/19/09 21:00	3.0	1389	5.6	0.4	2.2	1233	4.0	0.3	1.3	1101	2.4	0.1	0.8	903	1.4	0.1	47.0	43	71.0	0.2
12/19/09 21:30	2.1	1378	3.9	0.3	1.8	1223	3.3	0.2	1.5	1093	2.7	0.2	0.8	897	1.4	0.1	46.0	43	69.4	0.2
12/19/09 22:00	2.2	1367	4.0	0.3	2.5	1214	4.6	0.3	2.8	1085	5.2	0.3	0.8	891	1.4	0.1	46.0	43	85.5	0.2
12/19/09 22:30	2.2	1389	4.0	0.3	2.0	1225	3.6	0.2	1.7	1087	3.1	0.2	0.8	879	1.4	0.1	56.0	42	72.6	0.2
12/19/09 23:00	2.2	1334	4.0	0.3	2.4	1189	4.3	0.3	2.5	1068	4.6	0.3	0.8	885	1.4	0.1	48.0	43	67.8	0.2
12/19/09 23:30	2.2	1345	4.0	0.3	1.6	1195	2.9	0.2	1.0	1069	1.8	0.1	0.8	879	1.4	0.1	52.0	42	79.0	0.2
12/20/09 0:00	2.1	1345	3.9	0.3	1.8	1193	3.2	0.2	1.4	1065	2.6	0.2	0.7	873	1.3	0.1	45.0	42	66.2	0.2
12/20/09 0:30	2.3	1356	4.2	0.3	1.9	1200	3.5	0.2	1.5	1070	2.7	0.2	0.8	873	1.4	0.1	44.0	42	66.2	0.2
12/20/09 1:00	2.2	1323	4.0	0.3	1.7	1174	3.1	0.2	1.2	1049	2.2	0.1	0.9	861	1.6	0.1	46.0	41	69.4	0.2
12/20/09 1:30	2.3	1334	4.2	0.3	1.9	1182	3.4	0.2	1.4	1054	2.6	0.2	0.8	861	1.4	0.1	45.0	41	67.8	0.2

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/20/09 2:00	2.0	1312	3.7	0.3	1.6	1165	2.8	0.2	1.1	1041	2.0	0.1	0.8	856	1.4	0.1	48.0	41	72.6	0.2
12/20/09 2:30	2.1	1323	3.9	0.3	1.8	1169	3.3	0.2	1.5	1039	2.7	0.2	0.8	844	1.4	0.1	46.0	41	69.4	0.2
12/20/09 3:00	2.0	1312	3.7	0.3	2.2	1159	4.0	0.3	2.3	1031	4.2	0.2	0.8	838	1.4	0.1	42.0	40	63.0	0.1
12/20/09 3:30	2.1	1312	3.9	0.3	1.7	1161	3.0	0.2	1.2	1034	2.2	0.1	1.0	844	1.8	0.1	40.0	41	59.8	0.1
12/20/09 4:00	1.8	1301	3.3	0.2	1.5	1150	2.7	0.2	1.2	1023	2.2	0.1	0.8	832	1.4	0.1	38.0	40	56.6	0.1
12/20/09 4:30	2.1	1301	3.9	0.3	1.7	1154	3.1	0.2	1.3	1030	2.4	0.1	0.8	844	1.4	0.1	38.0	41	56.6	0.1
12/20/09 5:00	2.2	1301	4.0	0.3	1.7	1150	3.0	0.2	1.1	1023	2.0	0.1	0.9	832	1.6	0.1	37.0	40	55.0	0.1
12/20/09 5:30	1.8	1269	3.3	0.2	1.7	1123	3.0	0.2	1.5	1000	2.7	0.2	0.8	815	1.4	0.1	44.0	39	66.2	0.1
12/20/09 6:00	1.8	1269	3.3	0.2	1.4	1125	2.6	0.2	1.0	1003	1.8	0.1	0.8	821	1.4	0.1	41.0	40	61.4	0.1
12/20/09 6:30	1.7	1280	3.1	0.2	1.5	1132	2.6	0.2	1.2	1008	2.2	0.1	0.8	821	1.4	0.1	42.0	40	63.0	0.1
12/20/09 7:00	2.1	1258	3.9	0.3	1.7	1114	3.0	0.2	1.2	992	2.2	0.1	0.8	810	1.4	0.1	42.0	39	63.0	0.1
12/20/09 7:30	1.8	1248	3.3	0.2	1.6	1108	2.8	0.2	1.3	991	2.4	0.1	0.8	815	1.4	0.1	43.0	39	64.6	0.1
12/20/09 8:00	2.1	1258	3.9	0.3	1.7	1116	3.0	0.2	1.2	996	2.2	0.1	0.8	815	1.4	0.1	41.0	39	61.4	0.1
12/20/09 8:30	1.8	1248	3.3	0.2	1.7	1103	3.1	0.2	1.6	981	2.9	0.2	0.8	798	1.4	0.1	41.0	39	61.4	0.1
12/20/09 9:00	2.3	1258	4.2	0.3	1.7	1114	3.1	0.2	1.1	992	2.0	0.1	0.7	810	1.3	0.1	99.0	39	156.5	0.3
12/20/09 9:30	2.1	1248	3.9	0.3	2.0	1105	3.6	0.2	1.8	985	3.3	0.2	0.9	804	1.6	0.1	56.0	39	85.5	0.2
12/20/09 10:00	1.7	1216	3.1	0.2	1.4	1084	2.5	0.1	1.0	972	1.8	0.1	0.8	804	1.4	0.1	68.0	39	105.0	0.2
12/20/09 10:30	1.9	1216	3.5	0.2	1.4	1080	2.6	0.2	0.9	965	1.6	0.1	0.9	793	1.6	0.1	59.0	38	90.3	0.2
12/20/09 11:00	2.0	1216	3.7	0.3	1.9	1080	3.4	0.2	1.7	965	3.1	0.2	0.7	793	1.3	0.1	47.0	38	71.0	0.2
12/20/09 11:30	2.4	1258	4.4	0.3	2.0	1108	3.7	0.2	1.6	982	2.9	0.2	0.7	793	1.3	0.1	45.0	38	67.8	0.1
12/20/09 12:00	2.1	1206	3.9	0.3	1.9	1075	3.5	0.2	1.7	964	3.1	0.2	0.7	798	1.3	0.1	43.0	39	64.6	0.1
12/20/09 12:30	2.1	1196	3.9	0.3	2.0	1061	3.7	0.2	1.9	947	3.5	0.2	0.7	776	1.3	0.1	46.0	38	69.4	0.1
12/20/09 13:00	2.1	1196	3.9	0.3	1.9	1062	3.5	0.2	1.7	950	3.1	0.2	0.8	782	1.4	0.1	44.0	38	66.2	0.1
12/20/09 13:30	2.0	1206	3.7	0.2	1.6	1069	2.9	0.2	1.2	954	2.2	0.1	0.9	782	1.6	0.1	41.0	38	61.4	0.1
12/20/09 14:00	2.1	1185	3.9	0.3	1.6	1050	2.8	0.2	1.0	956	1.8	0.1	0.9	765	1.6	0.1	43.0	37	64.6	0.1
12/20/09 14:30	2.1	1185	3.9	0.3	1.6	1055	2.9	0.2	1.1	946	2.0	0.1	0.7	782	1.3	0.1	44.0	38	66.2	0.1
12/20/09 15:00	2.3	1165	4.2	0.3	1.8	1038	3.2	0.2	1.2	931	2.2	0.1	1.0	771	1.8	0.1	43.0	37	64.6	0.1
12/20/09 15:30	2.1	1175	3.9	0.3	1.5	1043	2.7	0.2	0.9	932	1.6	0.1	0.8	765	1.4	0.1	38.0	37	56.6	0.1
12/20/09 16:00	2.7	1165	5.0	0.3	1.8	1036	3.3	0.2	1.0	928	1.7	0.1	0.8	765	1.4	0.1	36.0	37	53.5	0.1
12/20/09 16:30	2.2	1165	4.0	0.3	1.6	1040	2.9	0.2	1.0	934	1.8	0.1	0.9	776	1.6	0.1	36.0	38	53.5	0.1
12/20/09 17:00	2.4	1155	4.4	0.3	1.8	1031	3.2	0.2	1.1	927	2.0	0.1	0.8	771	1.4	0.1	37.0	37	55.0	0.1
12/20/09 17:30	3.8	1155	7.1	0.5	2.5	1031	4.5	0.3	1.1	927	2.0	0.1	1.0	771	1.8	0.1	38.0	37	56.6	0.1
12/20/09 18:00	2.4	1175	4.4	0.3	1.8	1049	3.3	0.2	1.2	942	2.2	0.1	0.9	782	1.6	0.1	38.0	38	56.6	0.1
12/20/09 18:30	2.2	1175	4.0	0.3	1.7	1050	3.0	0.2	1.1	945	2.0	0.1	0.8	787	1.4	0.1	46.0	38	69.4	0.1
12/20/09 19:00	2.2	1175	4.0	0.3	1.7	1056	3.0	0.2	1.1	955	2.0	0.1	0.9	804	1.6	0.1	60.0	39	92.0	0.2
12/20/09 19:30	1.9	1185	3.5	0.2	1.4	1066	2.6	0.2	0.9	966	1.6	0.1	0.8	815	1.4	0.1	130.0	39	209.1	0.5
12/20/09 20:00	3.3	1185	6.1	0.4	2.2	1075	4.0	0.2	1.1	983	2.0	0.1	0.8	844	1.4	0.1	130.0	41	209.1	0.5
12/20/09 20:30	2.0	1196	3.7	0.2	1.7	1088	3.0	0.2	1.3	997	2.4	0.1	0.9	861	1.6	0.1	210.0	41	347.9	0.8
12/20/09 21:00	2.1	1227	3.9	0.3	2.1	1122	3.8	0.2	2.0	1035	3.7	0.2	0.7	903	1.3	0.1	150.0	43	243.4	0.6
12/20/09 21:30	3.4	1216	6.3	0.4	3.4	1117	6.3	0.4	3.4	1034	6.3	0.4	0.8	909	1.4	0.1	160.0	44	260.7	0.6
12/20/09 22:00	2.2	1258	4.0	0.3	3.3	1158	6.1	0.4	4.4	1073	8.2	0.5	0.9	946	1.6	0.1	180.0	45	295.4	0.8
12/20/09 22:30	2.1	1280	3.9	0.3	3.9	1180	7.2	0.5	5.6	1096	10.5	0.6	0.9	971	1.6	0.1	120.0	46	192.0	0.5

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/20/09 23:00	4.1	1290	7.6	0.6	4.9	1198	9.2	0.6	5.7	1120	10.7	0.7	0.9	1003	1.6	0.1	76.0	48	118.2	0.3
12/20/09 23:30	2.4	1312	4.4	0.3	4.1	1221	7.6	0.5	5.8	1144	10.9	0.7	0.8	1028	1.4	0.1	76.0	49	118.2	0.3
12/21/09 00:00	2.5	1323	4.6	0.3	3.9	1230	7.2	0.5	5.2	1152	9.7	0.6	1.2	1035	2.2	0.1	83.0	49	129.8	0.4
12/21/09 03:30	4.9	1345	9.2	0.7	4.4	1253	8.1	0.6	3.8	1177	7.1	0.5	1.0	1061	1.8	0.1	66.0	50	101.8	0.3
12/21/09 1:00	2.8	1412	5.2	0.4	2.8	1301	5.1	0.4	2.7	1208	5.0	0.3	1.1	1068	2.0	0.1	57.0	51	87.1	0.2
12/21/09 1:30	2.7	1435	5.0	0.4	2.7	1325	4.9	0.4	2.6	1233	4.8	0.3	1.0	1095	1.8	0.1	52.0	52	79.0	0.2
12/21/09 2:00	3.4	1458	6.3	0.5	3.0	1343	5.5	0.4	2.5	1247	4.6	0.3	1.0	1102	1.8	0.1	58.0	52	88.7	0.3
12/21/09 2:30	3.9	1470	7.3	0.6	3.2	1356	5.9	0.5	2.5	1260	4.6	0.3	1.6	1115	2.9	0.2	50.0	53	75.8	0.2
12/21/09 3:00	5.6	1482	10.5	0.9	3.9	1368	7.2	0.6	2.1	1273	3.9	0.3	1.1	1129	2.0	0.1	53.0	54	80.6	0.2
12/21/09 3:30	5.3	1506	9.9	0.8	3.8	1396	7.0	0.5	2.2	1303	4.0	0.3	1.2	1164	2.2	0.1	130.0	55	209.1	0.6
12/21/09 4:00	5.3	1530	9.9	0.9	3.8	1430	7.1	0.6	2.3	1346	4.2	0.3	2.2	1221	4.0	0.3	260.0	58	436.5	1.4
12/21/09 4:30	5.1	1542	9.5	0.8	4.0	1455	7.3	0.6	2.8	1382	5.2	0.4	1.4	1272	2.6	0.2	140.0	60	226.2	0.8
12/21/09 5:00	5.1	1604	9.5	0.9	4.3	1526	8.0	0.7	3.5	1461	6.5	0.5	1.3	1362	2.4	0.2	680.0	64	1211.9	4.3
12/21/09 5:30	3.9	1667	7.3	0.7	5.0	1623	9.3	0.9	6.1	1586	11.4	1.0	1.2	1530	2.2	0.2	570.0	71	1004.8	4.0
12/21/09 6:00	3.9	1705	7.3	0.7	6.2	1701	11.5	1.1	8.4	1698	15.9	1.5	1.5	1692	2.7	0.3	250.0	78	418.7	1.8
12/21/09 6:30	4.3	1744	8.0	0.8	11.2	1810	21.2	2.2	18.0	1866	34.5	3.6	1.5	1949	2.7	0.3	150.0	89	243.4	1.2
12/21/09 7:00	4.2	1770	7.8	0.8	15.5	1921	29.5	3.2	26.7	2048	51.6	5.9	2.2	2238	4.0	0.5	430.0	102	744.9	4.3
12/21/09 7:30	4.5	1957	8.4	0.9	8.9	2116	16.8	2.0	13.3	2251	25.4	3.2	2.1	2452	3.9	0.5	230.0	111	383.2	2.4
12/21/09 8:00	5.9	2131	11.1	1.3	10.0	2303	19.0	2.5	14.1	2448	26.9	3.7	2.9	2666	5.4	0.8	120.0	120	192.0	1.3
12/21/09 8:30	8.3	2350	15.7	2.1	13.8	2508	26.3	3.7	19.3	2642	37.1	5.5	2.8	2842	5.2	0.8	96.0	128	151.5	1.1
12/21/09 9:00	10.0	2552	19.0	2.7	12.6	2665	23.9	3.6	15.1	2760	28.9	4.5	3.1	2903	5.7	0.9	96.0	130	151.5	1.1
12/21/09 9:30	15.0	2735	28.7	4.4	14.0	2797	26.6	4.2	12.9	2849	24.6	3.9	3.4	2927	6.3	1.0	93.0	131	146.5	1.1
12/21/09 10:00	24.0	3124	46.3	8.1	17.8	3057	34.1	5.9	11.6	3000	22.1	3.7	2.8	2915	5.2	0.8	77.0	131	119.9	0.9
12/21/09 10:30	25.0	3066	48.3	8.3	18.2	3006	34.8	5.9	11.3	2955	21.5	3.6	2.6	2878	4.8	0.8	78.0	129	121.5	0.9
12/21/09 11:00	22.0	3504	42.4	8.3	15.9	3302	30.4	5.6	9.8	3133	18.6	3.3	2.5	2878	4.6	0.7	270.0	129	454.4	3.3
12/21/09 11:30	25.0	3154	48.3	8.6	16.6	3050	31.7	5.4	8.1	2962	15.3	2.5	2.7	2830	5.0	0.8	220.0	127	365.6	2.6
12/21/09 12:00	23.0	3472	44.3	8.6	16.5	3266	31.6	5.8	10.0	3092	19.0	3.3	2.2	2830	4.0	0.6	260.0	127	436.5	3.1
12/21/09 12:30	20.0	3380	38.4	7.3	15.6	3199	29.7	5.3	11.1	3047	21.1	3.6	1.9	2818	3.5	0.6	320.0	127	544.2	3.9
12/21/09 13:00	19.0	3426	36.5	7.0	15.7	3238	30.0	5.5	12.4	3080	23.6	4.1	2.7	2842	5.0	0.8	190.0	128	312.9	2.2
12/21/09 13:30	20.0	3258	38.4	7.0	18.1	3128	34.6	6.1	16.1	3019	30.8	5.2	1.9	2854	3.5	0.6	130.0	128	209.1	1.5
12/21/09 14:00	21.0	3410	40.4	7.7	15.8	3227	30.1	5.5	10.5	3073	19.9	3.4	2.3	2842	4.2	0.7	170.0	128	278.0	2.0
12/21/09 14:30	18.0	3410	34.5	6.6	13.5	3224	25.7	4.7	9.0	3066	17.0	2.9	1.9	2830	3.5	0.6	120.0	127	192.0	1.4
12/21/09 15:00	16.0	3380	30.6	5.8	13.3	3187	25.4	4.5	10.6	3026	20.1	3.4	3.0	2783	5.6	0.9	140.0	125	226.2	1.6
12/21/09 15:30	18.0	3426	34.5	6.6	13.8	3204	26.2	4.7	9.5	3016	18.0	3.0	2.4	2736	4.4	0.7	84.0	123	131.5	0.9
12/21/09 16:00	20.0	3567	38.4	7.7	14.1	3306	26.8	5.0	8.1	3088	15.3	2.7	2.7	2759	5.0	0.8	93.0	124	146.5	1.0
12/21/09 16:30	20.0	3349	38.4	7.2	14.1	3122	26.9	4.7	8.2	2930	15.5	2.5	2.3	2643	4.2	0.6	140.0	119	226.2	1.5
12/21/09 17:00	16.0	3198	30.6	5.5	12.1	3001	22.9	3.9	8.1	2835	15.3	2.4	2.0	2586	3.7	0.5	80.0	117	124.8	0.8
12/21/09 17:30	16.0	3535	30.6	6.1	12.6	3215	24.0	4.3	9.2	2945	17.4	2.9	2.2	2541	4.0	0.6	76.0	115	118.2	0.8
12/21/09 18:00	15.0	3334	28.7	5.4	11.4	3053	21.7	3.7	7.8	2817	14.7	2.3	1.7	2463	3.1	0.4	85.0	112	133.1	0.8
12/21/09 18:30	14.0	3110	26.7	4.7	10.3	2884	19.5	3.2	6.6	2694	12.4	1.9	1.8	2408	3.3	0.4	67.0	109	103.4	0.6
12/21/09 19:00	16.0	3124	30.6	5.4	11.2	2873	21.2	3.4	6.3	2661	11.8	1.8	1.8	2344	3.3	0.4	68.0	106	105.0	0.6
12/21/09 19:30	13.0	3258	24.8	4.5	9.6	2953	18.1	3.0	6.1	2697	11.4	1.7	1.7	2312	3.1	0.4	47.0	105	71.0	0.4

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/21/09 20:00	14.0	3198	26.7	4.8	10.8	2889	20.5	3.3	7.6	2629	14.3	2.1	1.9	2238	3.5	0.4	41.0	102	61.4	0.4
12/21/09 20:30	12.0	3110	22.8	4.0	8.8	2822	16.5	2.6	5.5	2580	10.3	1.5	1.6	2218	2.9	0.4	54.0	101	82.2	0.5
12/21/09 21:00	12.0	2994	22.8	3.8	9.1	2714	17.1	2.6	6.1	2479	11.4	1.6	1.4	2126	2.6	0.3	51.0	97	77.4	0.4
12/21/09 21:30	10.0	3066	19.0	3.3	6.8	2760	12.8	2.0	5.0	2502	9.3	1.3	1.4	2116	2.6	0.3	36.0	97	53.5	0.3
12/21/09 22:00	11.0	2979	20.9	3.5	8.3	2692	15.7	2.4	4.6	2449	8.6	1.2	1.5	2086	2.7	0.3	33.0	95	48.7	0.3
12/21/09 22:30	11.0	2894	20.9	3.4	7.1	2615	13.4	2.0	4.9	2379	9.2	1.2	1.7	2026	3.1	0.4	34.0	93	50.3	0.3
12/21/09 23:00	10.0	2836	19.0	3.0	6.0	2560	11.3	1.6	4.9	2327	9.2	1.2	1.6	1978	2.9	0.3	28.0	91	40.9	0.2
12/21/09 23:30	9.1	2865	17.2	2.8	6.3	2564	11.8	1.7	3.9	2310	7.3	0.9	1.4	1930	2.6	0.3	22.0	89	31.7	0.2
12/22/09 00:00	8.1	2951	15.3	2.5	6.5	2613	12.2	1.8	3.9	2328	7.3	0.9	1.1	1902	2.0	0.2	23.0	87	33.2	0.2
12/22/09 00:30	8.3	2706	15.7	2.4	5.6	2432	10.4	1.4	3.3	2201	6.1	0.8	1.2	1855	2.2	0.2	23.0	85	33.2	0.2
12/22/09 1:00	7.4	2865	13.9	2.2	4.6	2528	8.6	1.2	3.3	2244	6.1	0.8	1.6	1818	2.9	0.3	21.0	84	30.2	0.1
12/22/09 1:30	7.8	2566	14.7	2.1	5.0	2316	9.3	1.2	3.3	2106	6.1	0.7	1.6	1791	2.9	0.3	22.0	83	31.7	0.1
12/22/09 2:00	6.9	2607	13.0	1.9	4.7	2333	8.8	1.2	3.5	2101	6.5	0.8	1.2	1754	2.2	0.2	20.0	81	28.6	0.1
12/22/09 2:30	6.6	2566	12.4	1.8	4.1	2290	7.6	1.0	3.3	2058	6.1	0.7	1.1	1710	2.0	0.2	20.0	79	28.6	0.1
12/22/09 3:00	7.2	2483	13.6	1.9	5.1	2220	9.5	1.2	3.0	1999	5.6	0.6	1.1	1666	2.0	0.2	23.0	77	33.2	0.1
12/22/09 3:30	5.8	2497	10.9	1.5	4.8	2224	9.0	1.1	2.8	1994	5.2	0.6	1.1	1649	2.0	0.2	24.0	76	34.8	0.1
12/22/09 4:00	5.4	2524	10.1	1.4	3.5	2231	6.5	0.8	2.6	1984	4.8	0.5	1.0	1614	1.8	0.2	31.0	75	45.6	0.2
12/22/09 4:30	5.8	2649	10.9	1.6	3.5	2308	6.6	0.9	3.3	2020	6.1	0.7	1.0	1589	1.8	0.2	23.0	74	33.2	0.1
12/22/09 5:00	5.5	2350	10.3	1.4	3.6	2097	6.6	0.8	2.6	1883	4.8	0.5	1.0	1564	1.8	0.2	21.0	73	30.2	0.1
12/22/09 5:30	5.5	2363	10.3	1.4	3.6	2095	6.7	0.8	2.7	1869	5.0	0.5	1.0	1530	1.8	0.2	18.0	71	25.6	0.1
12/22/09 6:00	4.8	2470	9.0	1.2	3.6	2162	6.7	0.8	2.6	1903	4.8	0.5	1.0	1514	1.8	0.2	21.0	71	30.2	0.1
12/22/09 6:30	4.6	2285	8.6	1.1	3.7	2028	6.8	0.8	2.7	1813	5.0	0.5	1.0	1489	1.8	0.2	18.0	69	25.6	0.1
12/22/09 7:00	4.7	2272	8.8	1.1	3.7	2012	6.9	0.8	2.5	1793	4.6	0.5	1.1	1465	2.0	0.2	17.0	68	24.1	0.1
12/22/09 7:30	4.6	2208	8.6	1.1	3.7	1951	6.9	0.8	3.4	1734	6.3	0.6	1.0	1409	1.8	0.1	18.0	66	25.6	0.1
12/22/09 8:00	4.8	2363	9.0	1.2	3.8	2058	7.0	0.8	2.3	1802	4.2	0.4	1.0	1417	1.8	0.1	17.0	66	24.1	0.1
12/22/09 8:30	4.4	2233	8.2	1.0	3.8	1960	7.1	0.8	2.6	1730	4.8	0.5	2.9	1386	5.4	0.4	17.0	65	24.1	0.1
12/22/09 9:00	4.9	2233	9.2	1.1	3.8	1948	7.1	0.8	2.3	1708	4.2	0.4	1.2	1347	2.2	0.2	17.0	63	24.1	0.1
12/22/09 9:30	4.8	2195	9.0	1.1	3.9	1917	7.2	0.8	2.5	1683	4.6	0.4	0.9	1332	1.6	0.1	17.0	63	24.1	0.1
12/22/09 10:00	3.7	2118	6.9	0.8	3.9	1865	7.3	0.8	2.0	1652	3.7	0.3	0.9	1332	1.6	0.1	17.0	63	24.1	0.1
12/22/09 10:30	3.7	2131	6.9	0.8	3.9	1861	7.3	0.8	2.5	1634	4.6	0.4	1.1	1294	2.0	0.1	16.0	61	22.6	0.1
12/22/09 11:00	3.9	2118	7.3	0.9	4.0	1850	7.4	0.8	2.1	1625	3.9	0.4	0.9	1287	1.6	0.1	16.0	61	22.6	0.1
12/22/09 11:30	3.9	1994	7.3	0.8	4.0	1759	7.4	0.7	4.7	1561	8.8	0.8	0.8	1264	1.4	0.1	19.0	60	27.1	0.1
12/22/09 12:00	3.7	1981	6.9	0.8	4.0	1743	7.5	0.7	2.1	1543	3.9	0.3	0.9	1242	1.6	0.1	21.0	59	30.2	0.1
12/22/09 12:30	3.4	2055	6.3	0.7	4.1	1784	7.6	0.8	1.8	1556	3.3	0.3	0.9	1213	1.6	0.1	20.0	57	28.6	0.1
12/22/09 13:00	3.7	1945	6.9	0.8	4.1	1709	7.6	0.7	2.1	1511	3.9	0.3	0.9	1213	1.6	0.1	33.3	57	49.3	0.2
12/22/09 13:30	3.6	1917	6.7	0.7	4.1	1684	7.7	0.7	2.0	1487	3.7	0.3	1.0	1192	1.8	0.1	41.0	56	61.4	0.2
12/22/09 14:00	3.1	1945	5.7	0.6	4.2	1702	7.8	0.7	2.0	1498	3.7	0.3	0.8	1192	1.4	0.1	250.0	56	418.7	1.3
12/22/09 14:30	3.9	1981	7.3	0.8	4.2	1718	7.8	0.8	2.0	1496	3.7	0.3	0.8	1164	1.4	0.1	200.0	55	330.4	1.0
12/22/09 15:00	3.4	1917	6.3	0.7	4.2	1668	7.9	0.7	2.3	1458	4.2	0.3	0.9	1143	1.6	0.1	170.0	54	278.0	0.8
12/22/09 15:30	3.5	1863	6.5	0.7	4.3	1631	8.0	0.7	5.1	1436	9.5	0.8	0.9	1143	1.6	0.1	190.0	54	312.9	1.0
12/22/09 16:00	3.0	1796	5.6	0.6	4.3	1579	8.0	0.7	5.5	1396	10.3	0.8	1.0	1122	1.8	0.1	180.0	53	295.4	0.9
12/22/09 16:30	3.0	1823	5.6	0.6	4.3	1593	8.1	0.7	5.2	1399	9.7	0.8	0.8	1108	1.4	0.1	120.0	53	192.0	0.6

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/22/09 17:00	2.9	1836	5.4	0.6	4.4	1597	8.1	0.7	5.0	1396	9.3	0.7	0.8	1095	1.4	0.1	57.0	52	87.1	0.3
12/22/09 17:30	4.5	1770	8.4	0.8	4.4	1550	8.2	0.7	4.1	1365	7.6	0.6	0.9	1088	1.6	0.1	48.0	52	72.6	0.2
12/22/09 18:00	3.1	1823	5.7	0.6	4.4	1578	8.3	0.7	3.5	1371	6.5	0.5	0.8	1061	1.4	0.1	84.0	50	131.5	0.4
12/22/09 18:30	3.3	1731	6.1	0.6	4.5	1511	8.3	0.7	3.1	1326	5.7	0.4	0.9	1048	1.6	0.1	76.0	50	118.2	0.3
12/22/09 19:00	3.7	1744	6.9	0.7	4.5	1514	8.4	0.7	3.1	1319	5.7	0.4	0.8	1028	1.4	0.1	57.0	49	87.1	0.2
12/22/09 19:30	4.4	1667	8.2	0.8	4.5	1461	8.5	0.7	3.1	1288	5.7	0.4	1.1	1028	2.0	0.1	130.0	49	209.1	0.6
12/22/09 20:00	4.7	1680	8.8	0.8	4.6	1464	8.5	0.7	2.8	1282	5.2	0.4	0.7	1009	48	0.1	22.0	1009	31.7	0.1
12/22/09 20:30	5.3	1693	9.9	0.9	4.6	1466	8.6	0.7	2.6	1276	4.8	0.3	1.1	990	2.0	0.1	20.0	47	28.6	0.1
12/22/09 21:00	6.0	1642	11.3	1.0	4.6	1430	8.6	0.7	1.9	1251	3.5	0.2	0.7	983	1.3	0.1	16.0	47	22.6	0.1
12/22/09 21:30	4.7	1604	8.8	0.8	4.7	1400	8.7	0.7	1.8	1228	3.3	0.2	0.7	971	1.3	0.1	13.0	46	18.1	0.0
12/22/09 22:00	4.2	1616	7.8	0.7	4.7	1406	8.8	0.7	1.5	1230	2.7	0.2	0.7	964	1.3	0.1	13.0	46	18.1	0.0
12/22/09 22:30	4.4	1616	8.2	0.7	4.7	1404	8.8	0.7	1.9	1226	3.5	0.2	1.1	958	2.0	0.1	12.0	46	16.6	0.0
12/22/09 23:00	4.4	1579	8.2	0.7	4.8	1373	8.9	0.7	4.0	1200	7.4	0.5	0.8	940	1.4	0.1	12.0	45	16.6	0.0
12/22/09 23:30	4.2	1591	7.8	0.7	4.8	1378	9.0	0.7	1.8	1197	3.3	0.2	0.6	927	1.1	0.1	25.0	44	36.3	0.1
12/23/09 0:00	3.5	1554	6.5	0.6	4.8	1351	9.0	0.7	1.3	1179	2.4	0.2	0.7	921	1.3	0.1	24.0	44	34.8	0.1
12/23/09 0:30	3.5	1518	6.5	0.6	4.9	1324	9.1	0.7	4.1	1160	7.6	0.5	0.6	915	1.1	0.1	20.0	44	28.6	0.1
12/23/09 1:00	3.1	1506	5.7	0.5	4.9	1310	9.2	0.7	1.3	1145	2.4	0.2	0.6	897	1.1	0.1	12.0	43	16.6	0.0
12/23/09 1:30	3.1	1506	5.7	0.5	4.9	1312	9.2	0.7	1.2	1148	2.2	0.1	0.7	903	1.3	0.1	11.0	43	15.2	0.0
12/23/09 2:00	2.8	1482	5.2	0.4	5.0	1290	9.3	0.7	1.1	1128	2.0	0.1	0.6	885	1.1	0.1	9.4	43	12.8	0.0
12/23/09 2:30	3.1	1494	5.7	0.5	5.0	1296	9.3	0.7	1.3	1129	2.4	0.2	0.6	879	1.1	0.1	85.0	42	133.1	0.3
12/23/09 3:00	2.9	1447	5.4	0.4	5.0	1258	9.4	0.7	1.5	1100	2.7	0.2	0.6	861	1.1	0.1	52.0	41	79.0	0.2
12/23/09 3:30	2.4	1435	4.4	0.4	5.1	1250	9.5	0.7	1.2	1095	2.2	0.1	0.6	861	1.1	0.1	33.0	41	48.7	0.1
12/23/09 4:00	3.7	1458	6.9	0.6	5.1	1262	9.5	0.7	1.1	1097	2.0	0.1	0.7	850	1.3	0.1	19.0	41	27.1	0.1
12/23/09 4:30	2.7	1435	5.0	0.4	5.1	1239	9.6	0.7	1.4	1074	2.6	0.2	0.7	827	1.3	0.1	28.0	40	40.9	0.1
12/23/09 5:00	2.3	1389	4.2	0.3	5.2	1212	9.7	0.7	1.0	1062	1.8	0.1	0.6	838	1.1	0.1	68.0	40	105.0	0.2
12/23/09 5:30	2.9	1412	5.4	0.4	5.2	1222	9.7	0.7	1.3	1061	2.4	0.1	0.6	821	1.1	0.0	59.0	40	90.3	0.2
12/23/09 6:00	2.5	1389	4.6	0.4	5.2	1205	9.8	0.7	1.2	1049	2.2	0.1	0.6	815	1.1	0.0	29.0	39	42.5	0.1
12/23/09 6:30	2.5	1378	4.6	0.4	5.3	1193	9.9	0.7	2.5	1038	4.6	0.3	1.6	804	2.9	0.1	16.0	39	22.6	0.0
12/23/09 7:00	2.7	1367	5.0	0.4	5.3	1186	9.9	0.7	1.0	1033	1.8	0.1	0.7	804	1.3	0.1	12.0	39	16.6	0.0
12/23/09 7:30	2.4	1356	4.4	0.3	5.3	1176	10.0	0.7	1.4	1025	2.6	0.1	0.7	798	1.3	0.1	9.8	39	13.4	0.0
12/23/09 8:00	2.7	1345	5.0	0.4	5.4	1163	10.0	0.7	1.3	1011	2.4	0.1	0.7	782	1.3	0.1	55.0	38	83.9	0.2
12/23/09 8:30	2.4	1334	4.4	0.3	5.4	1154	10.1	0.7	1.0	1003	1.8	0.1	0.8	776	1.4	0.1	71.0	38	110.0	0.2
12/23/09 9:00	2.2	1356	4.0	0.3	5.4	1166	10.2	0.7	1.0	1006	1.8	0.1	0.6	765	1.1	0.0	14.0	37	19.6	0.0
12/23/09 9:30	2.2	1301	4.0	0.3	5.5	1127	10.2	0.6	1.0	980	1.8	0.1	0.6	760	1.1	0.0	12.0	37	16.6	0.0
12/23/09 10:00	2.3	1312	4.2	0.3	5.5	1136	10.3	0.7	1.2	988	2.2	0.1	1.3	765	2.4	0.1	11.0	37	15.2	0.0
12/23/09 10:30	2.0	1290	3.7	0.3	5.5	1118	10.4	0.7	0.9	972	1.6	0.1	0.6	754	1.1	0.0	8.1	37	11.0	0.0
12/23/09 11:00	2.2	1258	4.0	0.3	5.6	1091	10.4	0.6	1.4	950	2.6	0.1	0.6	738	1.1	0.0	60.0	36	92.0	0.2
12/23/09 11:30	2.1	1258	3.9	0.3	5.6	1091	10.5	0.6	1.5	950	2.7	0.1	0.5	738	0.9	0.0	41.0	36	61.4	0.1
12/23/09 12:00	2.2	1248	4.0	0.3	5.6	1082	10.6	0.6	2.2	942	4.0	0.2	0.5	733	0.9	0.0	22.0	36	31.7	0.1
12/23/09 12:30	2.2	1258	4.0	0.3	5.7	1086	10.6	0.6	1.2	940	2.2	0.1	0.6	722	1.1	0.0	29.0	35	42.5	0.1
12/23/09 13:00	2.4	1237	4.4	0.3	5.7	1070	10.7	0.6	1.1	929	2.0	0.1	0.6	717	1.1	0.0	14.0	35	19.6	0.0
12/23/09 13:30	2.0	1227	3.7	0.3	1.0	1063	1.8	0.1	0.9	924	1.6	0.1	0.5	717	0.9	0.0	56.0	35	85.5	0.2

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/23/09 14:00	2.0	1216	3.7	0.3	0.9	1054	1.6	0.1	0.9	917	1.6	0.1	0.6	712	1.1	0.0	41.0	35	61.4	0.1
12/23/09 14:30	2.2	1206	4.0	0.3	1.5	1044	2.7	0.2	1.0	907	1.8	0.1	0.7	702	1.3	0.0	120.0	34	192.0	0.4
12/23/09 15:00	2.2	1216	4.0	0.3	0.7	1049	1.3	0.1	0.9	908	1.6	0.1	0.4	696	0.7	0.0	66.0	34	101.8	0.2
12/23/09 15:30	2.1	1206	3.9	0.3	0.7	1044	1.3	0.1	1.0	907	1.8	0.1	0.5	702	0.9	0.0	50.0	34	75.8	0.1
12/23/09 16:00	2.1	1196	3.9	0.3	1.0	1032	1.8	0.1	3.8	893	7.1	0.4	0.5	686	0.9	0.0	87.0	33	136.5	0.3
12/23/09 16:30	3.2	1175	5.9	0.4	0.7	1016	1.3	0.1	1.0	882	1.8	0.1	0.5	681	0.9	0.0	76.0	33	118.2	0.2
12/23/09 17:00	1.9	1175	3.5	0.2	0.7	1013	1.3	0.1	1.3	876	2.4	0.1	0.6	671	1.1	0.0	68.0	33	105.0	0.2
12/23/09 17:30	2.3	1155	4.2	0.3	1.8	999	3.3	0.2	1.9	868	3.5	0.2	0.6	671	1.1	0.0	53.0	33	80.6	0.1
12/23/09 18:00	3.0	1175	5.6	0.4	0.7	1011	1.3	0.1	1.8	873	3.3	0.2	0.5	666	0.9	0.0	47.0	33	71.0	0.1
12/23/09 18:30	1.9	1135	3.5	0.2	1.4	986	2.6	0.1	1.4	860	2.6	0.1	0.6	671	1.1	0.0	42.0	33	63.0	0.1
12/23/09 19:00	2.0	1155	3.7	0.2	1.4	996	2.6	0.1	1.6	862	2.9	0.1	0.5	661	0.9	0.0	41.0	32	61.4	0.1
12/23/09 19:30	1.9	1135	3.5	0.2	1.3	979	2.4	0.1	1.6	848	2.9	0.1	0.5	651	0.9	0.0	23.0	32	33.2	0.1
12/23/09 20:00	2.8	1125	5.2	0.3	1.2	972	2.2	0.1	1.7	844	3.1	0.1	0.5	651	0.9	0.0	110.0	32	175.1	0.3
12/23/09 20:30	1.9	1115	3.5	0.2	1.4	963	2.6	0.1	2.5	834	4.6	0.2	0.6	641	1.1	0.0	62.0	31	95.2	0.2
12/23/09 21:00	1.9	1106	3.5	0.2	1.5	958	2.7	0.1	1.5	833	2.7	0.1	0.5	646	0.9	0.0	44.0	32	66.2	0.1
12/23/09 21:30	2.3	1096	4.2	0.3	1.4	948	2.6	0.1	2.0	823	3.7	0.2	0.5	636	0.9	0.0	37.0	31	55.0	0.1
12/23/09 22:00	1.7	1106	3.1	0.2	1.1	953	2.0	0.1	1.2	824	2.2	0.1	0.5	631	0.9	0.0	34.0	31	50.3	0.1
12/23/09 22:30	2.1	1096	3.9	0.2	1.3	946	2.4	0.1	1.4	820	2.6	0.1	0.5	631	0.9	0.0	44.0	31	66.2	0.1
12/23/09 23:00	1.8	1096	3.3	0.2	1.2	943	2.2	0.1	1.7	815	3.1	0.1	0.6	622	1.1	0.0	46.0	31	69.4	0.1
12/23/09 23:30	1.9	1067	3.5	0.2	1.4	924	2.6	0.1	1.5	803	2.6	0.1	0.6	622	1.1	0.0	38.0	31	56.6	0.1
12/24/09 00:00	1.9	1067	3.5	0.2	1.1	920	2.0	0.1	1.2	797	2.2	0.1	0.4	612	0.7	0.0	51.0	30	77.4	0.1
12/24/09 03:30	2.3	1058	4.2	0.3	1.5	914	2.7	0.1	1.0	793	1.8	0.1	0.7	612	1.3	0.0	49.0	30	74.2	0.1
12/24/09 1:00	2.5	1058	4.6	0.3	0.9	913	1.6	0.1	1.5	790	2.7	0.1	0.5	607	0.9	0.0	23.0	30	33.2	0.1
12/24/09 1:30	2.2	1058	4.0	0.2	1.1	913	2.0	0.1	1.6	790	2.9	0.1	0.4	607	0.7	0.0	19.0	30	27.1	0.0
12/24/09 2:00	2.0	1039	3.7	0.2	1.0	898	1.8	0.1	1.4	780	2.6	0.1	0.6	602	1.1	0.0	21.0	30	30.2	0.1
12/24/09 2:30	2.0	1039	3.7	0.2	1.2	897	2.2	0.1	1.2	777	2.2	0.1	0.6	598	1.1	0.0	16.0	29	22.6	0.0
12/24/09 3:00	2.0	1039	3.7	0.2	1.0	895	1.8	0.1	1.2	774	2.2	0.1	0.4	593	0.7	0.0	20.0	29	28.6	0.0
12/24/09 3:30	1.9	1048	3.5	0.2	1.4	900	2.6	0.1	0.9	775	1.6	0.1	0.5	588	0.9	0.0	20.0	29	28.6	0.0
12/24/09 4:00	2.0	1039	3.7	0.2	0.6	894	1.1	0.1	0.9	772	1.6	0.1	0.5	588	0.9	0.0	14.0	29	19.6	0.0
12/24/09 4:30	2.2	1020	4.0	0.2	1.0	880	1.8	0.1	1.4	761	2.6	0.1	0.6	584	1.1	0.0	12.0	29	16.6	0.0
12/24/09 5:00	2.0	1012	3.7	0.2	0.6	872	1.1	0.1	0.9	755	1.6	0.1	0.4	579	0.7	0.0	21.0	29	30.2	0.0
12/24/09 5:30	2.0	1012	3.7	0.2	0.8	871	1.4	0.1	1.0	752	1.8	0.1	0.5	575	0.9	0.0	13.0	28	18.1	0.0
12/24/09 6:00	1.9	1003	3.5	0.2	0.8	864	1.4	0.1	1.8	746	3.3	0.1	0.5	570	0.9	0.0	170.0	28	278.0	0.4
12/24/09 6:30	2.1	1012	3.9	0.2	0.8	869	1.4	0.1	1.0	750	13.2	0.6	0.5	570	0.9	0.0	59.0	28	90.3	0.1
12/24/09 7:00	1.9	995	3.5	0.2	0.7	856	1.3	0.1	0.9	740	1.6	0.1	0.5	565	0.9	0.0	44.0	28	66.2	0.1
12/24/09 7:30	1.8	995	3.3	0.2	0.6	856	1.1	0.1	1.8	740	3.3	0.1	0.5	565	0.9	0.0	9.6	28	13.1	0.0
12/24/09 8:00	1.9	986	3.5	0.2	0.9	848	1.6	0.1	1.9	731	1.6	0.1	0.5	556	0.9	0.0	10.0	27	13.7	0.0
12/24/09 8:30	1.5	978	2.7	0.2	0.7	844	1.3	0.1	1.0	731	1.8	0.1	0.5	561	0.9	0.0	21.0	28	30.2	0.0
12/24/09 9:00	1.8	986	3.3	0.2	0.7	848	1.3	0.1	0.9	731	1.6	0.1	0.4	556	0.7	0.0	62.0	27	95.2	0.1
12/24/09 9:30	2.2	978	4.0	0.2	0.8	841	1.4	0.1	0.9	725	1.6	0.1	0.5	552	0.9	0.0	45.0	27	67.8	0.1
12/24/09 10:00	2.0	978	3.7	0.2	0.5	841	0.9	0.0	0.8	725	1.4	0.1	0.5	552	0.9	0.0	160.0	27	260.7	0.4
12/24/09 10:30	2.2	978	4.0	0.2	0.7	838	1.3	0.1	1.0	720	1.8	0.1	0.5	543	0.9	0.0	53.0	27	80.6	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/24/09 11:00	2.3	962	4.2	0.2	1.0	825	1.8	0.1	1.0	711	1.8	0.1	0.5	539	0.9	0.0	27.0	27	39.4	0.1
12/24/09 11:30	2.1	962	3.9	0.2	0.7	825	1.3	0.1	2.6	711	4.8	0.2	0.4	539	0.7	0.0	24.0	27	34.8	0.1
12/24/09 12:00	1.9	953	3.5	0.2	0.8	820	1.4	0.1	2.3	707	4.2	0.2	0.4	539	0.7	0.0	18.0	27	25.6	0.0
12/24/09 12:30	1.8	953	3.3	0.2	0.7	817	1.3	0.1	3.0	702	5.6	0.2	0.5	530	0.9	0.0	18.0	26	25.6	0.0
12/24/09 13:00	2.2	929	4.0	0.2	1.5	802	2.7	0.1	3.1	695	5.7	0.2	0.4	534	0.7	0.0	26.0	26	37.8	0.1
12/24/09 13:30	1.8	945	3.3	0.2	1.6	811	2.9	0.1	2.1	699	3.9	0.2	0.5	530	0.9	0.0	28.0	26	40.9	0.1
12/24/09 14:00	3.8	937	7.1	0.4	2.5	805	4.6	0.2	1.4	693	2.6	0.1	0.5	525	0.9	0.0	27.0	26	39.4	0.1
12/24/09 14:30	1.8	937	3.3	0.2	2.2	806	4.0	0.2	1.1	695	2.0	0.1	0.4	530	0.7	0.0	22.0	26	31.7	0.0
12/24/09 15:00	2.0	929	3.7	0.2	1.8	801	3.3	0.1	1.2	692	2.2	0.1	0.4	530	0.7	0.0	41.0	26	61.4	0.1
12/24/09 15:30	1.8	913	3.3	0.2	1.0	788	1.8	0.1	1.4	683	2.6	0.1	0.4	525	0.7	0.0	64.0	26	98.5	0.1
12/24/09 16:00	1.8	929	3.3	0.2	1.2	798	2.2	0.1	1.3	687	2.4	0.1	0.6	521	1.1	0.0	140.0	26	226.2	0.3
12/24/09 16:30	2.2	929	4.0	0.2	1.0	801	1.8	0.1	1.3	692	2.4	0.1	0.4	530	0.7	0.0	58.0	26	88.7	0.1
12/24/09 17:00	2.0	921	3.7	0.2	0.8	795	1.4	0.1	1.4	689	2.6	0.1	0.4	530	0.7	0.0	83.0	26	129.8	0.2
12/24/09 17:30	2.9	921	5.4	0.3	0.9	794	1.6	0.1	1.5	686	2.7	0.1	0.5	525	0.9	0.0	64.0	26	98.5	0.1
12/24/09 18:00	3.0	905	5.6	0.3	1.0	782	1.8	0.1	1.9	677	3.5	0.1	0.5	521	0.9	0.0	48.0	26	72.6	0.1
12/24/09 18:30	3.1	921	5.7	0.3	1.3	795	2.4	0.1	3.0	689	5.6	0.2	0.4	530	0.7	0.0	33.0	26	48.7	0.1
12/24/09 19:00	3.0	921	5.6	0.3	1.5	794	2.7	0.1	3.3	686	6.1	0.2	0.4	525	0.7	0.0	28.0	26	40.9	0.1
12/24/09 19:30	3.0	897	5.6	0.3	1.9	776	3.5	0.2	2.5	674	4.6	0.2	0.4	521	0.7	0.0	34.0	26	50.3	0.1
12/24/09 20:00	2.3	905	4.2	0.2	2.1	782	3.9	0.2	2.0	677	3.7	0.1	0.4	521	0.7	0.0	19.0	26	27.1	0.0
12/24/09 20:30	2.0	905	3.7	0.2	2.1	783	3.9	0.2	1.8	680	3.3	0.1	0.5	525	0.9	0.0	19.0	26	27.1	0.0
12/24/09 21:00	1.8	897	3.3	0.2	2.1	776	3.9	0.2	1.5	674	2.7	0.1	0.4	521	0.7	0.0	17.0	26	24.1	0.0
12/24/09 21:30	2.7	890	5.0	0.2	1.4	769	2.6	0.1	1.4	668	2.6	0.1	0.4	517	0.7	0.0	17.0	26	24.1	0.0
12/24/09 22:00	2.3	897	4.2	0.2	1.0	773	1.8	0.1	1.6	669	2.9	0.1	0.4	512	0.7	0.0	17.0	25	24.1	0.0
12/24/09 22:30	2.3	897	4.2	0.2	1.2	772	2.2	0.1	1.2	666	2.2	0.1	0.5	508	0.9	0.0	13.0	25	18.1	0.0
12/24/09 23:00	2.8	890	5.2	0.3	0.9	767	1.6	0.1	1.1	663	2.0	0.1	0.4	508	0.7	0.0	13.0	25	18.1	0.0
12/24/09 23:30	2.4	890	4.4	0.2	0.9	768	1.6	0.1	1.5	666	2.7	0.1	0.4	512	0.7	0.0	11.0	25	15.2	0.0
12/25/09 0:00	2.8	905	5.2	0.3	1.2	779	2.2	0.1	1.1	672	2.0	0.1	0.5	512	0.9	0.0	11.0	25	15.2	0.0
12/25/09 0:30	3.3	890	6.1	0.3	0.8	767	1.4	0.1	0.9	663	1.6	0.1	0.5	508	0.9	0.0	11.0	25	15.2	0.0
12/25/09 1:00	3.5	874	6.5	0.3	0.9	758	1.6	0.1	0.9	659	1.6	0.1	0.4	512	0.7	0.0	12.0	25	16.6	0.0
12/25/09 1:30	3.4	882	6.3	0.3	0.7	760	1.3	0.1	0.8	658	1.4	0.1	0.4	504	0.7	0.0	11.0	25	15.2	0.0
12/25/09 2:00	3.1	890	5.7	0.3	0.7	765	1.3	0.1	0.9	661	1.6	0.1	0.4	504	0.7	0.0	32.0	25	47.2	0.1
12/25/09 2:30	2.7	890	5.0	0.2	0.9	767	1.6	0.1	0.7	663	1.3	0.0	0.4	508	0.7	0.0	25.0	25	36.3	0.1
12/25/09 3:00	2.6	882	4.8	0.2	0.4	759	0.7	0.0	0.8	655	1.4	0.1	0.4	500	0.7	0.0	18.0	25	25.6	0.0
12/25/09 3:30	2.6	874	4.8	0.2	0.6	753	1.1	0.0	1.0	652	1.8	0.1	0.4	500	0.7	0.0	15.0	25	21.1	0.0
12/25/09 4:00	2.9	882	5.4	0.3	0.8	757	1.4	0.1	1.2	653	2.2	0.1	0.4	495	0.7	0.0	12.0	25	16.6	0.0
12/25/09 4:30	3.5	866	6.5	0.3	0.4	748	0.7	0.0	0.9	649	1.6	0.1	0.5	500	0.9	0.0	8.8	25	12.0	0.0
12/25/09 5:00	3.4	866	6.3	0.3	0.7	747	1.3	0.1	0.8	646	1.4	0.1	0.4	495	0.7	0.0	6.8	25	9.1	0.0
12/25/09 5:30	2.4	874	4.4	0.2	0.7	752	1.3	0.1	0.7	649	1.3	0.0	0.5	495	0.9	0.0	6.5	25	8.7	0.0
12/25/09 6:00	2.8	866	5.2	0.3	0.6	745	1.1	0.0	0.7	644	1.3	0.0	0.4	491	0.7	0.0	6.6	24	8.8	0.0
12/25/09 6:30	2.4	859	4.4	0.2	0.4	739	0.7	0.0	0.7	638	1.3	0.0	0.4	487	0.7	0.0	7.1	24	9.5	0.0
12/25/09 7:00	2.7	859	5.0	0.2	1.7	739	3.1	0.1	1.3	638	2.4	0.1	0.4	487	0.7	0.0	7.4	24	10.0	0.0
12/25/09 7:30	2.5	843	4.6	0.2	0.6	729	1.1	0.0	0.7	632	1.3	0.0	0.4	487	0.7	0.0	8.7	24	11.8	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/25/09 8:00	2.6	851	4.8	0.2	0.3	731	0.5	0.0	0.7	630	1.3	0.0	0.4	479	0.7	0.0	16.0	24	22.6	0.0
12/25/09 8:30	2.1	843	3.9	0.2	0.6	727	1.1	0.0	0.6	630	1.1	0.0	0.6	483	1.1	0.0	20.0	24	28.6	0.0
12/25/09 9:00	2.6	859	4.8	0.2	0.6	738	1.1	0.0	0.7	636	1.3	0.0	0.4	483	0.7	0.0	28.0	24	40.9	0.1
12/25/09 9:30	2.5	843	4.6	0.2	0.6	726	1.1	0.0	0.7	627	1.3	0.0	0.5	479	0.9	0.0	52.0	24	79.0	0.1
12/25/09 10:00	2.6	836	4.8	0.2	0.5	720	0.9	0.0	0.7	622	1.3	0.0	0.4	475	0.7	0.0	16.0	24	22.6	0.0
12/25/09 10:30	2.3	836	4.2	0.2	0.3	721	0.5	0.0	0.5	624	0.9	0.0	0.7	479	1.3	0.0	25.0	24	36.3	0.0
12/25/09 11:00	2.6	843	4.8	0.2	0.5	725	0.9	0.0	0.7	625	1.3	0.0	0.6	475	1.1	0.0	16.0	24	22.6	0.0
12/25/09 11:30	2.3	836	4.2	0.2	0.6	720	1.1	0.0	0.6	622	1.1	0.0	0.4	475	0.7	0.0	35.0	24	51.9	0.1
12/25/09 12:00	2.5	828	4.6	0.2	0.4	714	0.7	0.0	0.7	619	1.3	0.0	0.4	475	0.7	0.0	18.0	24	25.6	0.0
12/25/09 12:30	2.7	821	5.0	0.2	0.8	707	1.4	0.1	0.6	611	1.1	0.0	0.4	467	0.7	0.0	9.2	23	12.6	0.0
12/25/09 13:00	2.1	828	3.9	0.2	0.5	712	0.9	0.0	0.5	614	0.9	0.0	0.4	467	0.7	0.0	8.4	23	11.4	0.0
12/25/09 13:30	2.9	821	5.4	0.2	0.5	707	0.9	0.0	0.7	611	1.3	0.0	0.5	467	0.9	0.0	6.1	23	8.1	0.0
12/25/09 14:00	2.1	813	3.9	0.2	0.4	700	0.7	0.0	0.6	605	1.1	0.0	0.4	462	0.7	0.0	9.8	23	13.4	0.0
12/25/09 14:30	2.2	806	4.0	0.2	0.2	694	0.4	0.0	0.7	600	1.3	0.0	0.6	458	1.1	0.0	6.0	23	8.0	0.0
12/25/09 15:00	2.2	821	4.0	0.2	0.5	705	0.9	0.0	0.6	608	1.1	0.0	0.5	462	0.9	0.0	6.2	23	8.3	0.0
12/25/09 15:30	2.3	813	4.2	0.2	0.4	699	0.7	0.0	0.5	603	0.9	0.0	0.4	458	0.7	0.0	5.1	23	6.7	0.0
12/25/09 16:00	1.9	806	3.5	0.2	0.4	695	0.7	0.0	0.7	602	1.3	0.0	0.4	462	0.7	0.0	13.0	23	18.1	0.0
12/25/09 16:30	2.3	799	4.2	0.2	0.3	688	0.5	0.0	0.5	594	0.9	0.0	0.4	454	0.7	0.0	6.1	23	8.1	0.0
12/25/09 17:00	1.9	806	3.5	0.2	0.3	693	0.5	0.0	0.5	597	0.9	0.0	0.4	454	0.7	0.0	5.1	23	6.7	0.0
12/25/09 17:30	1.9	806	3.5	0.2	0.3	694	0.5	0.0	0.6	600	1.1	0.0	0.4	458	0.7	0.0	11.0	23	15.2	0.0
12/25/09 18:00	2.0	806	3.7	0.2	0.4	693	0.7	0.0	0.6	597	1.1	0.0	0.4	454	0.7	0.0	5.4	23	7.1	0.0
12/25/09 18:30	2.1	806	3.9	0.2	0.4	692	0.7	0.0	0.8	595	1.4	0.0	0.4	450	0.7	0.0	7.5	23	10.1	0.0
12/25/09 19:00	1.9	799	3.5	0.2	0.3	687	0.5	0.0	0.7	592	1.3	0.0	0.5	450	0.9	0.0	4.7	23	6.2	0.0
12/25/09 19:30	1.9	791	3.5	0.2	0.3	680	0.5	0.0	0.9	587	1.6	0.1	0.4	447	0.7	0.0	4.7	22	6.2	0.0
12/25/09 20:00	2.1	791	3.9	0.2	0.6	679	1.1	0.0	0.6	584	1.1	0.0	0.5	443	0.9	0.0	6.0	22	8.0	0.0
12/25/09 20:30	2.0	791	3.7	0.2	0.4	680	0.7	0.0	0.6	587	1.1	0.0	0.5	447	0.9	0.0	4.5	22	5.9	0.0
12/25/09 21:00	2.0	791	3.7	0.2	0.3	679	0.5	0.0	1.4	584	2.6	0.1	0.4	443	0.7	0.0	5.3	22	7.0	0.0
12/25/09 21:30	2.1	784	3.9	0.2	0.6	674	1.1	0.0	0.6	581	1.1	0.0	0.4	443	0.7	0.0	4.6	22	6.0	0.0
12/25/09 22:00	2.3	784	4.2	0.2	0.3	673	0.5	0.0	1.6	579	2.9	0.1	0.4	439	0.7	0.0	11.0	22	15.2	0.0
12/25/09 22:30	2.3	784	4.2	0.2	0.4	674	0.7	0.0	0.7	581	1.3	0.0	0.5	443	0.9	0.0	4.6	22	6.0	0.0
12/25/09 23:00	2.2	777	4.0	0.2	0.3	667	0.5	0.0	0.5	574	0.9	0.0	0.5	435	0.9	0.0	5.3	22	7.0	0.0
12/25/09 23:30	2.5	770	4.6	0.2	0.3	661	0.5	0.0	0.7	569	1.3	0.0	0.5	431	0.9	0.0	4.6	22	6.0	0.0
12/26/09 0:00	2.6	777	4.8	0.2	0.6	667	1.1	0.0	0.6	574	1.1	0.0	0.6	435	1.1	0.0	4.6	22	6.0	0.0
12/26/09 0:30	2.0	770	3.7	0.2	0.4	662	0.7	0.0	0.6	571	1.1	0.0	0.4	435	0.7	0.0	5.1	22	6.7	0.0
12/26/09 1:00	2.4	762	4.4	0.2	0.3	656	0.5	0.0	0.7	566	1.3	0.0	0.4	431	0.7	0.0	5.1	22	6.7	0.0
12/26/09 1:30	2.2	762	4.0	0.2	0.6	657	1.1	0.0	0.6	568	1.1	0.0	0.4	435	0.7	0.0	5.2	22	6.8	0.0
12/26/09 2:00	1.9	762	3.5	0.1	0.4	654	0.7	0.0	0.8	563	1.4	0.0	0.4	427	0.7	0.0	5.1	21	6.7	0.0
12/26/09 2:30	2.3	755	4.2	0.2	0.3	650	0.5	0.0	0.5	561	0.9	0.0	0.4	427	0.7	0.0	5.6	21	7.4	0.0
12/26/09 3:00	2.4	762	4.4	0.2	0.3	654	0.5	0.0	0.6	563	1.1	0.0	0.4	427	0.7	0.0	9.2	21	12.6	0.0
12/26/09 3:30	2.2	770	4.0	0.2	0.5	658	0.9	0.0	0.8	564	1.4	0.0	0.4	423	0.7	0.0	7.6	21	10.2	0.0
12/26/09 4:00	2.3	755	4.2	0.2	0.3	648	0.5	0.0	0.6	558	1.1	0.0	0.4	423	0.7	0.0	6.6	21	8.8	0.0
12/26/09 4:30	1.9	748	3.5	0.1	0.5	642	0.9	0.0	0.6	553	1.1	0.0	0.4	419	0.7	0.0	8.5	21	11.5	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/26/09 5:00	2.2	741	4.0	0.2	0.2	639	0.4	0.0	0.6	553	1.1	0.0	0.4	423	0.7	0.0	8.1	21	11.0	0.0
12/26/09 5:30	2.6	755	4.8	0.2	0.3	646	0.5	0.0	0.6	554	1.1	0.0	0.4	416	0.7	0.0	8.3	21	11.3	0.0
12/26/09 6:00	2.6	748	4.8	0.2	0.5	642	0.9	0.0	0.7	553	1.3	0.0	0.5	419	0.9	0.0	5.3	21	7.0	0.0
12/26/09 6:30	2.7	734	5.0	0.2	0.4	630	0.7	0.0	0.7	543	1.3	0.0	0.3	412	0.5	0.0	16.0	21	22.6	0.0
12/26/09 7:00	1.8	748	3.3	0.1	0.3	640	0.5	0.0	0.7	549	1.3	0.0	0.7	412	1.3	0.0	6.5	21	8.7	0.0
12/26/09 7:30	2.5	741	4.6	0.2	0.3	634	0.5	0.0	0.7	544	1.3	0.0	0.4	408	0.7	0.0	7.6	21	10.2	0.0
12/26/09 8:00	2.5	741	4.6	0.2	0.6	634	1.1	0.0	0.8	544	1.4	0.0	0.4	408	0.7	0.0	6.6	21	8.8	0.0
12/26/09 8:30	2.7	727	5.0	0.2	0.4	625	0.7	0.0	0.7	538	1.3	0.0	0.4	408	0.7	0.0	6.9	21	9.2	0.0
12/26/09 9:00	2.6	720	4.8	0.2	0.4	619	0.7	0.0	0.6	533	1.1	0.0	0.3	404	0.5	0.0	7.1	20	9.5	0.0
12/26/09 9:30	2.2	727	4.0	0.2	0.5	622	0.9	0.0	0.7	534	1.3	0.0	0.4	401	0.7	0.0	5.2	20	6.8	0.0
12/26/09 10:00	2.8	734	5.2	0.2	0.4	628	0.7	0.0	0.6	539	1.1	0.0	0.4	404	0.7	0.0	11.0	20	15.2	0.0
12/26/09 10:30	2.6	714	4.8	0.2	0.3	613	0.5	0.0	0.6	528	1.1	0.0	0.4	401	0.7	0.0	6.3	20	8.4	0.0
12/26/09 11:00	2.3	727	4.2	0.2	0.3	623	0.5	0.0	0.6	536	1.1	0.0	0.3	404	0.5	0.0	8.0	20	10.8	0.0
12/26/09 11:30	2.3	720	4.2	0.2	0.4	616	0.7	0.0	0.7	529	1.3	0.0	0.4	397	0.7	0.0	8.9	20	12.1	0.0
12/26/09 12:00	2.4	720	4.4	0.2	0.3	617	0.5	0.0	0.6	531	1.1	0.0	0.5	401	0.9	0.0	13.0	20	18.1	0.0
12/26/09 12:30	2.5	714	4.6	0.2	0.3	612	0.5	0.0	0.6	526	1.1	0.0	0.4	397	0.7	0.0	7.5	20	10.1	0.0
12/26/09 13:00	1.8	707	3.3	0.1	0.2	607	0.4	0.0	0.7	523	1.3	0.0	0.4	397	0.7	0.0	5.8	20	7.7	0.0
12/26/09 13:30	2.0	707	3.7	0.1	0.6	606	1.1	0.0	1.4	521	2.6	0.1	0.4	393	0.7	0.0	8.0	20	10.8	0.0
12/26/09 14:00	1.7	700	3.1	0.1	0.3	601	0.5	0.0	0.6	518	1.1	0.0	0.4	393	0.7	0.0	7.5	20	10.1	0.0
12/26/09 14:30	1.7	707	3.1	0.1	0.3	605	0.5	0.0	0.7	519	1.3	0.0	0.4	390	0.7	0.0	9.8	20	13.4	0.0
12/26/09 15:00	1.7	707	3.1	0.1	0.6	605	1.1	0.0	0.7	519	1.3	0.0	0.4	390	0.7	0.0	9.5	20	13.0	0.0
12/26/09 15:30	1.7	707	3.1	0.1	0.3	603	0.5	0.0	0.6	516	1.1	0.0	0.4	386	0.7	0.0	14.0	19	19.6	0.0
12/26/09 16:00	1.8	693	3.3	0.1	0.3	595	0.5	0.0	1.1	513	2.0	0.1	0.5	390	0.9	0.0	9.4	20	12.8	0.0
12/26/09 16:30	1.7	700	3.1	0.1	0.4	599	0.7	0.0	0.6	514	1.1	0.0	0.4	386	0.7	0.0	11.0	19	15.2	0.0
12/26/09 17:00	1.8	686	3.3	0.1	0.3	590	0.5	0.0	0.6	508	1.1	0.0	0.4	386	0.7	0.0	10.0	19	13.7	0.0
12/26/09 17:30	1.5	693	2.7	0.1	0.6	593	1.1	0.0	0.6	509	1.1	0.0	0.4	382	0.7	0.0	9.0	19	12.3	0.0
12/26/09 18:00	2.2	693	4.0	0.2	0.5	593	0.9	0.0	0.7	509	1.3	0.0	0.4	382	0.7	0.0	7.2	19	9.7	0.0
12/26/09 18:30	1.9	686	3.5	0.1	0.3	587	0.5	0.0	0.7	504	1.3	0.0	0.5	379	0.9	0.0	8.5	19	11.5	0.0
12/26/09 19:00	1.8	686	3.3	0.1	0.4	587	0.7	0.0	0.8	504	1.4	0.0	0.6	379	1.1	0.0	6.0	19	8.0	0.0
12/26/09 19:30	2.0	673	3.7	0.1	0.5	577	0.9	0.0	0.8	496	1.4	0.0	0.5	375	0.9	0.0	5.9	19	7.8	0.0
12/26/09 20:00	1.8	680	3.3	0.1	0.5	582	0.9	0.0	0.6	499	1.1	0.0	0.7	375	1.3	0.0	8.7	19	11.8	0.0
12/26/09 20:30	2.0	680	3.7	0.1	0.4	582	0.7	0.0	0.7	499	1.3	0.0	0.4	375	0.7	0.0	10.0	19	13.7	0.0
12/26/09 21:00	1.8	673	3.3	0.1	0.4	576	0.7	0.0	0.6	494	1.1	0.0	0.4	372	0.7	0.0	6.5	19	8.7	0.0
12/26/09 21:30	1.8	673	3.3	0.1	0.4	576	0.7	0.0	0.6	494	1.1	0.0	0.5	372	0.9	0.0	6.8	19	9.1	0.0
12/26/09 22:00	1.8	673	3.3	0.1	0.3	576	0.5	0.0	0.9	494	1.6	0.0	0.4	372	0.7	0.0	8.7	19	11.8	0.0
12/26/09 22:30	1.7	673	3.1	0.1	1.0	575	1.8	0.1	0.6	492	1.1	0.0	0.4	368	0.7	0.0	8.3	19	11.3	0.0
12/26/09 23:00	1.7	667	3.1	0.1	0.7	570	1.3	0.0	0.6	490	1.1	0.0	0.4	368	0.7	0.0	7.2	19	9.7	0.0
12/26/09 23:30	1.7	667	3.1	0.1	0.9	570	1.6	0.1	0.6	490	1.1	0.0	0.5	368	0.9	0.0	6.2	19	8.3	0.0
12/27/09 0:00	1.7	660	3.1	0.1	0.7	565	1.3	0.0	0.6	485	1.1	0.0	0.4	365	0.7	0.0	8.5	18	11.5	0.0
12/27/09 0:30	2.0	660	3.7	0.1	0.4	565	0.7	0.0	0.5	485	0.9	0.0	0.5	365	0.9	0.0	6.8	18	9.1	0.0
12/27/09 1:00	1.7	660	3.1	0.1	2.8	565	5.2	0.2	0.5	485	0.9	0.0	0.4	365	0.7	0.0	4.9	18	6.4	0.0
12/27/09 1:30	1.9	660	3.5	0.1	0.3	564	0.5	0.0	0.6	483	1.1	0.0	0.4	361	0.7	0.0	5.0	18	6.6	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/27/09 2:00	3.1	660	5.7	0.2	0.3	564	0.5	0.0	0.6	483	1.1	0.0	0.4	361	0.7	0.0	6.3	18	8.4	0.0
12/27/09 2:30	1.8	653	3.3	0.1	0.4	559	0.7	0.0	0.6	480	1.1	0.0	0.6	361	1.1	0.0	7.8	18	10.5	0.0
12/27/09 3:00	1.6	647	2.9	0.1	0.4	554	0.7	0.0	0.6	475	1.1	0.0	0.4	358	0.7	0.0	7.0	18	9.4	0.0
12/27/09 3:30	2.0	647	3.7	0.1	0.4	554	0.7	0.0	0.5	475	0.9	0.0	0.4	358	0.7	0.0	6.3	18	8.4	0.0
12/27/09 4:00	2.5	641	4.6	0.2	0.4	549	0.7	0.0	0.5	471	0.9	0.0	0.7	354	1.3	0.0	5.7	18	7.5	0.0
12/27/09 4:30	1.7	647	3.1	0.1	0.3	553	0.5	0.0	0.4	473	0.7	0.0	0.5	354	0.9	0.0	5.5	18	7.3	0.0
12/27/09 5:00	2.0	647	3.7	0.1	0.3	553	0.5	0.0	0.5	473	0.9	0.0	0.4	354	0.7	0.0	6.0	18	8.0	0.0
12/27/09 5:30	2.1	635	3.9	0.1	0.3	543	0.5	0.0	0.6	466	1.1	0.0	0.4	351	0.7	0.0	11.0	18	15.2	0.0
12/27/09 6:00	1.7	635	3.1	0.1	0.4	543	0.7	0.0	0.6	466	1.1	0.0	0.7	351	1.3	0.0	6.3	18	8.4	0.0
12/27/09 6:30	1.7	629	3.1	0.1	0.4	539	0.7	0.0	0.6	464	1.1	0.0	0.4	351	0.7	0.0	5.2	18	6.8	0.0
12/27/09 7:00	1.8	635	3.3	0.1	0.3	542	0.5	0.0	0.6	464	1.1	0.0	0.4	347	0.7	0.0	5.4	18	7.1	0.0
12/27/09 7:30	1.5	623	2.7	0.1	0.3	534	0.5	0.0	0.6	459	1.1	0.0	0.4	347	0.7	0.0	7.4	18	10.0	0.0
12/27/09 8:00	1.7	629	3.1	0.1	0.3	538	0.5	0.0	0.6	462	1.1	0.0	0.4	347	0.7	0.0	5.6	18	7.4	0.0
12/27/09 8:30	1.9	617	3.5	0.1	0.6	529	1.1	0.0	0.6	455	1.1	0.0	0.4	344	0.7	0.0	8.3	17	11.3	0.0
12/27/09 9:00	1.8	623	3.3	0.1	0.9	533	1.6	0.0	1.2	457	2.2	0.1	0.6	344	1.1	0.0	12.0	17	16.6	0.0
12/27/09 9:30	1.6	623	2.9	0.1	0.3	532	0.5	0.0	0.6	455	1.1	0.0	0.4	341	0.7	0.0	7.5	17	10.1	0.0
12/27/09 10:00	1.8	629	3.3	0.1	0.2	536	0.4	0.0	0.6	458	1.1	0.0	0.4	341	0.7	0.0	7.7	17	10.4	0.0
12/27/09 10:30	1.8	617	3.3	0.1	0.3	527	0.5	0.0	0.5	451	0.9	0.0	0.4	337	0.7	0.0	5.5	17	7.3	0.0
12/27/09 11:00	1.6	611	2.9	0.1	0.3	524	0.5	0.0	0.4	451	0.7	0.0	0.4	341	0.7	0.0	4.9	17	6.4	0.0
12/27/09 11:30	1.7	611	3.1	0.1	0.3	524	0.5	0.0	0.4	451	0.7	0.0	0.4	341	0.7	0.0	5.7	17	7.5	0.0
12/27/09 12:00	1.4	611	2.6	0.1	0.1	523	0.2	0.0	0.5	449	0.9	0.0	0.4	337	0.7	0.0	6.5	17	8.7	0.0
12/27/09 12:30	1.6	605	2.9	0.1	0.1	518	0.2	0.0	0.6	444	1.1	0.0	0.4	334	0.7	0.0	6.4	17	8.5	0.0
12/27/09 13:00	1.8	611	3.3	0.1	0.2	522	0.4	0.0	0.6	447	1.1	0.0	0.6	334	1.1	0.0	10.0	17	13.7	0.0
12/27/09 13:30	1.8	605	3.3	0.1	0.5	517	0.9	0.0	0.6	442	1.1	0.0	0.4	331	0.7	0.0	9.0	17	12.3	0.0
12/27/09 14:00	1.7	611	3.1	0.1	0.2	521	0.4	0.0	0.5	445	0.9	0.0	0.4	331	0.7	0.0	6.5	17	8.7	0.0
12/27/09 14:30	1.6	605	2.9	0.1	0.3	517	0.5	0.0	0.5	442	0.9	0.0	0.5	331	0.9	0.0	5.2	17	6.8	0.0
12/27/09 15:00	1.7	599	3.1	0.1	0.4	513	0.7	0.0	0.6	440	1.1	0.0	0.6	331	1.1	0.0	4.4	17	5.7	0.0
12/27/09 15:30	1.6	599	2.9	0.1	0.6	513	1.1	0.0	0.5	440	0.9	0.0	1.0	331	1.8	0.0	4.6	17	6.0	0.0
12/27/09 16:00	1.6	599	2.9	0.1	0.3	512	0.5	0.0	0.6	438	1.1	0.0	0.4	327	0.7	0.0	5.4	17	7.1	0.0
12/27/09 16:30	1.6	593	2.9	0.1	0.2	508	0.4	0.0	0.6	436	1.1	0.0	0.4	327	0.7	0.0	5.9	17	7.8	0.0
12/27/09 17:00	1.6	593	2.9	0.1	0.4	507	0.7	0.0	0.6	434	1.1	0.0	0.6	324	1.1	0.0	7.5	17	10.1	0.0
12/27/09 17:30	1.6	599	2.9	0.1	0.3	511	0.5	0.0	0.7	436	1.3	0.0	0.4	324	0.7	0.0	5.5	17	7.3	0.0
12/27/09 18:00	1.6	593	2.9	0.1	0.2	507	0.4	0.0	0.5	434	0.9	0.0	0.3	324	0.5	0.0	5.8	17	7.7	0.0
12/27/09 18:30	1.6	588	2.9	0.1	0.2	503	0.4	0.0	0.4	431	0.7	0.0	0.5	324	0.9	0.0	4.9	17	6.4	0.0
12/27/09 19:00	1.6	588	2.9	0.1	0.1	502	0.2	0.0	0.5	429	0.9	0.0	0.4	321	0.7	0.0	16.0	16	22.6	0.0
12/27/09 19:30	1.5	582	2.7	0.1	0.2	498	0.4	0.0	0.7	427	1.3	0.0	0.5	321	0.9	0.0	7.6	16	10.2	0.0
12/27/09 20:00	1.8	582	3.3	0.1	0.3	498	0.5	0.0	0.6	427	1.1	0.0	0.3	321	0.5	0.0	6.2	16	8.3	0.0
12/27/09 20:30	1.6	588	2.9	0.1	0.1	501	0.2	0.0	0.5	427	0.9	0.0	0.4	318	0.7	0.0	7.2	16	9.7	0.0
12/27/09 21:00	1.6	582	2.9	0.1	0.3	497	0.5	0.0	0.4	425	0.7	0.0	0.5	318	0.9	0.0	6.8	16	9.1	0.0
12/27/09 21:30	1.6	576	2.9	0.1	0.2	493	0.4	0.0	0.6	423	1.1	0.0	0.4	318	0.7	0.0	6.5	16	8.7	0.0
12/27/09 22:00	2.3	582	4.2	0.1	0.2	496	0.4	0.0	0.7	423	1.3	0.0	0.4	314	0.7	0.0	7.6	16	10.2	0.0
12/27/09 22:30	1.8	576	3.3	0.1	0.3	492	0.5	0.0	0.6	421	1.1	0.0	0.4	314	0.7	0.0	8.9	16	12.1	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/27/09 23:00	1.6	576	2.9	0.1	0.2	492	0.4	0.0	0.6	421	1.1	0.0	0.4	314	0.7	0.0	6.3	16	8.4	0.0
12/27/09 23:30	1.7	576	3.1	0.1	0.2	492	0.4	0.0	0.6	421	1.1	0.0	0.9	314	1.6	0.0	6.4	16	8.5	0.0
12/28/09 0:00	1.6	570	2.9	0.1	0.1	487	0.2	0.0	0.8	417	1.4	0.0	0.3	311	0.5	0.0	7.6	16	10.2	0.0
12/28/09 0:30	1.6	576	2.9	0.1	0.7	491	1.3	0.0	0.6	419	1.1	0.0	0.3	311	0.5	0.0	9.9	16	13.6	0.0
12/28/09 1:00	1.7	570	3.1	0.1	0.3	487	0.5	0.0	0.6	417	1.1	0.0	0.4	311	0.7	0.0	9.2	16	12.6	0.0
12/28/09 1:30	1.6	565	2.9	0.1	0.3	482	0.5	0.0	0.6	412	1.1	0.0	0.4	308	0.7	0.0	13.0	16	18.1	0.0
12/28/09 2:00	1.6	570	2.9	0.1	0.2	486	0.4	0.0	0.5	415	0.9	0.0	1.0	308	1.8	0.0	7.1	16	9.5	0.0
12/28/09 2:30	1.6	565	2.9	0.1	0.2	482	0.4	0.0	0.5	412	0.9	0.0	0.4	308	0.7	0.0	6.9	16	9.2	0.0
12/28/09 3:00	1.5	565	2.7	0.1	0.1	481	0.2	0.0	0.6	411	1.1	0.0	0.4	305	0.7	0.0	8.8	16	12.0	0.0
12/28/09 3:30	1.5	565	2.7	0.1	0.3	481	0.5	0.0	0.5	411	0.9	0.0	0.5	305	0.9	0.0	8.5	16	11.5	0.0
12/28/09 4:00	1.7	565	3.1	0.1	0.3	481	0.5	0.0	0.5	411	0.9	0.0	0.4	305	0.7	0.0	5.3	16	7.0	0.0
12/28/09 4:30	1.6	559	2.9	0.1	0.3	477	0.5	0.0	0.6	408	1.1	0.0	0.4	305	0.7	0.0	36.0	16	53.5	0.0
12/28/09 5:00	1.6	559	2.9	0.1	0.2	476	0.4	0.0	0.6	406	1.1	0.0	0.4	302	0.7	0.0	33.0	15	48.7	0.0
12/28/09 5:30	1.7	559	3.1	0.1	0.4	476	0.7	0.0	0.5	406	0.9	0.0	0.4	302	0.7	0.0	24.0	15	34.8	0.0
12/28/09 6:00	1.6	553	2.9	0.1	0.2	472	0.4	0.0	0.6	404	1.1	0.0	0.4	302	0.7	0.0	19.0	15	27.1	0.0
12/28/09 6:30	1.7	553	3.1	0.1	0.4	472	0.7	0.0	0.6	404	1.1	0.0	0.4	302	0.7	0.0	12.0	15	16.6	0.0
12/28/09 7:00	1.7	548	3.1	0.1	0.4	468	0.7	0.0	0.6	400	1.1	0.0	0.4	299	0.7	0.0	13.0	15	18.1	0.0
12/28/09 7:30	1.6	548	2.9	0.1	0.2	468	0.4	0.0	0.9	400	1.6	0.0	0.3	299	0.5	0.0	27.0	15	39.4	0.0
12/28/09 8:00	1.7	542	3.1	0.1	0.3	463	0.5	0.0	0.6	396	1.1	0.0	0.4	296	0.7	0.0	6.6	15	8.8	0.0
12/28/09 8:30	1.7	537	3.1	0.1	0.3	459	0.5	0.0	0.6	394	1.1	0.0	0.4	296	0.7	0.0	7.9	15	10.7	0.0
12/28/09 9:00	2.3	542	4.2	0.1	0.4	463	0.7	0.0	1.0	396	1.8	0.0	0.4	296	0.7	0.0	10.0	15	13.7	0.0
12/28/09 9:30	1.6	537	2.9	0.1	0.3	458	0.5	0.0	0.5	392	0.9	0.0	0.3	293	0.5	0.0	14.0	15	19.6	0.0
12/28/09 10:00	1.8	537	3.3	0.1	0.2	458	0.4	0.0	0.6	392	1.1	0.0	0.4	293	0.7	0.0	5.6	15	7.4	0.0
12/28/09 10:30	1.7	542	3.1	0.1	0.3	462	0.5	0.0	0.6	394	1.1	0.0	0.4	293	0.7	0.0	5.6	15	7.4	0.0
12/28/09 11:00	1.6	537	2.9	0.1	0.4	458	0.7	0.0	0.6	392	1.1	0.0	0.4	293	0.7	0.0	6.7	15	9.0	0.0
12/28/09 11:30	2.1	531	3.9	0.1	0.7	453	1.3	0.0	0.4	388	0.7	0.0	0.4	290	0.7	0.0	6.5	15	8.7	0.0
12/28/09 12:00	1.9	531	3.5	0.1	0.2	453	0.4	0.0	0.4	388	0.7	0.0	0.3	290	0.5	0.0	11.0	15	15.2	0.0
12/28/09 12:30	1.7	531	3.1	0.1	0.3	453	0.5	0.0	0.4	388	0.7	0.0	0.3	290	0.5	0.0	18.0	15	25.6	0.0
12/28/09 13:00	1.6	531	2.9	0.1	0.3	453	0.5	0.0	0.6	388	1.1	0.0	1.2	290	2.2	0.0	7.8	15	10.5	0.0
12/28/09 13:30	2.0	531	3.7	0.1	0.3	453	0.5	0.0	0.4	388	0.7	0.0	0.3	290	0.5	0.0	12.0	15	16.6	0.0
12/28/09 14:00	2.0	526	3.7	0.1	0.2	448	0.4	0.0	0.6	382	1.1	0.0	1.0	283	1.8	0.0	5.7	15	7.5	0.0
12/28/09 14:30	2.1	531	3.9	0.1	0.3	453	0.5	0.0	0.6	386	1.1	0.0	0.3	286	0.5	0.0	10.0	15	13.7	0.0
12/28/09 15:00	2.3	526	4.2	0.1	0.1	448	0.2	0.0	0.6	382	1.1	0.0	0.3	283	0.5	0.0	4.8	15	6.3	0.0
12/28/09 15:30	1.6	521	2.9	0.1	0.2	444	0.4	0.0	0.5	380	0.9	0.0	0.5	283	0.9	0.0	6.4	15	8.5	0.0
12/28/09 16:00	1.7	521	3.1	0.1	0.2	444	0.4	0.0	0.4	380	0.7	0.0	0.3	283	0.5	0.0	6.1	15	8.1	0.0
12/28/09 16:30	2.1	515	3.9	0.1	0.3	441	0.5	0.0	0.4	378	0.7	0.0	0.3	283	0.5	0.0	5.4	15	7.1	0.0
12/28/09 17:00	2.0	521	3.7	0.1	0.3	443	0.5	0.0	0.6	378	1.1	0.0	0.4	280	0.7	0.0	5.9	14	7.8	0.0
12/28/09 17:30	1.9	521	3.5	0.1	0.2	443	0.4	0.0	0.6	378	1.1	0.0	0.3	280	0.5	0.0	7.3	14	9.8	0.0
12/28/09 18:00	2.0	510	3.7	0.1	0.4	436	0.7	0.0	0.5	374	0.9	0.0	0.3	280	0.5	0.0	5.6	14	7.4	0.0
12/28/09 18:30	2.0	515	3.7	0.1	0.4	440	0.7	0.0	0.5	376	0.9	0.0	0.3	280	0.5	0.0	4.4	14	5.7	0.0
12/28/09 19:00	2.1	515	3.9	0.1	0.2	440	0.4	0.0	0.4	376	0.7	0.0	0.5	280	0.9	0.0	4.2	14	5.5	0.0
12/28/09 19:30	2.1	515	3.9	0.1	0.2	439	0.4	0.0	0.6	374	1.1	0.0	0.3	277	0.5	0.0	7.1	14	9.5	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/28/09 20:00	2.1	510	3.9	0.1	0.3	435	0.5	0.0	0.4	372	0.7	0.0	0.4	277	0.7	0.0	4.4	14	5.7	0.0
12/28/09 20:30	1.3	510	2.4	0.1	0.2	435	0.4	0.0	0.5	372	0.9	0.0	0.3	277	0.5	0.0	9.8	14	13.4	0.0
12/28/09 21:00	1.9	504	3.5	0.1	0.2	431	0.4	0.0	0.5	370	0.9	0.0	0.3	277	0.5	0.0	4.1	14	5.3	0.0
12/28/09 21:30	2.2	510	4.0	0.1	0.3	434	0.5	0.0	0.6	370	1.1	0.0	0.3	275	0.5	0.0	4.3	14	5.6	0.0
12/28/09 22:00	2.4	504	4.4	0.1	0.3	430	0.5	0.0	0.4	368	0.7	0.0	0.3	275	0.5	0.0	4.7	14	6.2	0.0
12/28/09 22:30	2.1	504	3.9	0.1	0.4	429	0.7	0.0	0.4	366	0.7	0.0	0.5	272	0.9	0.0	5.0	14	6.6	0.0
12/28/09 23:00	2.3	504	4.2	0.1	0.2	429	0.4	0.0	0.5	366	0.9	0.0	0.4	272	0.7	0.0	4.6	14	6.0	0.0
12/28/09 23:30	2.3	499	4.2	0.1	0.1	426	0.2	0.0	0.4	364	0.7	0.0	0.5	272	0.9	0.0	7.1	14	9.5	0.0
12/29/09 00:00	1.9	499	3.5	0.1	0.3	426	0.5	0.0	0.5	364	0.9	0.0	0.3	272	0.5	0.0	14.0	14	19.6	0.0
12/29/09 03:00	2.4	499	4.4	0.1	0.2	426	0.4	0.0	0.5	364	0.9	0.0	0.3	272	0.5	0.0	4.5	14	5.9	0.0
12/29/09 1:00	2.0	499	3.7	0.1	0.3	425	0.5	0.0	0.4	362	0.7	0.0	0.4	269	0.7	0.0	5.0	14	6.6	0.0
12/29/09 1:30	2.4	504	4.4	0.1	0.3	429	0.5	0.0	0.5	365	0.9	0.0	0.8	269	1.4	0.0	5.1	14	6.7	0.0
12/29/09 2:00	2.5	494	4.6	0.1	0.6	421	1.1	0.0	0.4	360	0.7	0.0	0.5	269	0.9	0.0	11.0	14	15.2	0.0
12/29/09 2:30	2.4	494	4.4	0.1	0.3	421	0.5	0.0	0.4	360	0.7	0.0	0.4	269	0.7	0.0	5.9	14	7.8	0.0
12/29/09 3:00	2.2	494	4.0	0.1	0.1	420	0.2	0.0	0.5	359	0.9	0.0	0.4	266	0.7	0.0	6.7	14	9.0	0.0
12/29/09 3:30	2.4	489	4.4	0.1	0.3	417	0.5	0.0	0.5	356	0.9	0.0	0.9	266	1.6	0.0	4.2	14	5.5	0.0
12/29/09 4:00	2.2	489	4.0	0.1	1.2	417	2.2	0.1	0.4	356	0.7	0.0	0.6	266	1.1	0.0	7.5	14	10.1	0.0
12/29/09 4:30	3.2	484	5.9	0.2	0.3	413	0.5	0.0	0.4	353	0.7	0.0	0.3	263	0.5	0.0	7.3	14	9.8	0.0
12/29/09 5:00	2.4	489	4.4	0.1	0.1	416	0.2	0.0	0.6	355	1.1	0.0	0.3	263	0.5	0.0	6.7	14	9.0	0.0
12/29/09 5:30	2.9	484	5.4	0.1	0.3	413	0.5	0.0	0.5	353	0.9	0.0	0.4	263	0.7	0.0	6.2	14	8.3	0.0
12/29/09 6:00	2.9	484	5.4	0.1	0.1	413	0.2	0.0	0.5	353	0.9	0.0	0.4	263	0.7	0.0	8.0	14	10.8	0.0
12/29/09 6:30	2.3	484	4.2	0.1	0.1	413	0.2	0.0	0.6	353	1.1	0.0	0.3	263	0.5	0.0	6.5	14	8.7	0.0
12/29/09 7:00	2.1	478	3.9	0.1	0.1	408	0.2	0.0	0.6	349	1.1	0.0	0.3	260	0.5	0.0	6.2	13	8.3	0.0
12/29/09 7:30	1.9	478	3.5	0.1	0.1	408	0.2	0.0	1.1	349	2.0	0.0	0.3	260	0.5	0.0	4.5	13	5.9	0.0
12/29/09 8:00	2.3	484	4.2	0.1	0.2	412	0.4	0.0	0.5	351	0.9	0.0	0.3	260	0.5	0.0	4.1	13	5.3	0.0
12/29/09 8:30	2.3	473	4.2	0.1	0.3	405	0.5	0.0	0.4	347	0.7	0.0	0.3	260	0.5	0.0	4.9	13	6.4	0.0
12/29/09 9:00	1.8	473	3.3	0.1	0.4	404	0.7	0.0	0.5	345	0.9	0.0	0.3	257	0.5	0.0	5.4	13	7.1	0.0
12/29/09 9:30	2.2	478	4.0	0.1	0.3	407	0.5	0.0	0.5	347	0.9	0.0	0.4	257	0.7	0.0	6.3	13	8.4	0.0
12/29/09 10:00	2.4	473	4.4	0.1	0.1	404	0.2	0.0	0.5	345	0.9	0.0	0.3	257	0.5	0.0	5.3	13	7.0	0.0
12/29/09 10:30	2.2	468	4.0	0.1	0.1	400	0.2	0.0	0.5	343	0.9	0.0	0.4	257	0.7	0.0	12.0	13	16.6	0.0
12/29/09 11:00	2.2	468	4.0	0.1	0.1	400	0.2	0.0	0.5	343	0.9	0.0	0.3	257	0.5	0.0	6.1	13	8.1	0.0
12/29/09 11:30	2.1	468	3.9	0.1	0.2	399	0.4	0.0	0.4	341	0.7	0.0	0.3	254	0.5	0.0	14.0	13	19.6	0.0
12/29/09 12:00	2.3	468	4.2	0.1	0.3	399	0.5	0.0	0.4	341	0.7	0.0	0.3	254	0.5	0.0	6.7	13	9.0	0.0
12/29/09 12:30	2.3	468	4.2	0.1	0.2	399	0.4	0.0	0.4	341	0.7	0.0	0.4	254	0.7	0.0	5.9	13	7.8	0.0
12/29/09 13:00	2.3	468	4.2	0.1	0.3	399	0.5	0.0	0.5	341	0.9	0.0	0.4	254	0.7	0.0	6.2	13	8.3	0.0
12/29/09 13:30	2.2	463	4.0	0.1	0.1	396	0.2	0.0	0.4	339	0.7	0.0	0.4	254	0.7	0.0	8.2	13	11.1	0.0
12/29/09 14:00	2.4	468	4.4	0.1	0.1	398	0.2	0.0	0.5	340	0.9	0.0	0.3	252	0.5	0.0	6.9	13	9.2	0.0
12/29/09 14:30	1.1	463	2.0	0.1	0.1	395	0.2	0.0	0.4	338	0.7	0.0	0.3	252	0.5	0.0	7.5	13	10.1	0.0
12/29/09 15:00	1.3	463	2.4	0.1	0.1	395	0.2	0.0	0.4	338	0.7	0.0	0.3	252	0.5	0.0	8.5	13	11.5	0.0
12/29/09 15:30	1.0	463	1.8	0.0	0.2	395	0.4	0.0	0.4	338	0.7	0.0	0.4	252	0.7	0.0	8.8	13	12.0	0.0
12/29/09 16:00	1.0	463	1.8	0.0	0.1	395	0.2	0.0	0.4	338	0.7	0.0	0.4	252	0.7	0.0	9.4	13	12.8	0.0
12/29/09 16:30	1.0	468	1.8	0.0	0.2	399	0.4	0.0	0.6	341	1.1	0.0	0.3	254	0.5	0.0	9.7	13	13.3	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/29/09 17:00	1.1	463	2.0	0.1	0.1	396	0.2	0.0	0.6	339	1.1	0.0	0.4	254	0.7	0.0	5.8	13	7.7	0.0
12/29/09 17:30	1.8	468	3.3	0.1	0.4	399	0.7	0.0	0.5	341	0.9	0.0	0.4	254	0.7	0.0	8.5	13	11.5	0.0
12/29/09 18:00	1.0	463	1.8	0.0	0.1	396	0.2	0.0	0.6	339	1.1	0.0	0.3	254	0.5	0.0	9.1	13	12.4	0.0
12/29/09 18:30	0.9	463	1.6	0.0	0.1	396	0.2	0.0	0.6	339	1.1	0.0	0.3	254	0.5	0.0	27.0	13	39.4	0.0
12/29/09 19:00	1.0	463	1.8	0.0	0.3	396	0.5	0.0	0.6	339	1.1	0.0	0.3	254	0.5	0.0	21.0	13	30.2	0.0
12/29/09 19:30	1.1	463	2.0	0.1	0.4	396	0.7	0.0	0.7	339	1.3	0.0	0.3	254	0.5	0.0	30.0	13	44.0	0.0
12/29/09 20:00	1.2	468	2.2	0.1	0.3	399	0.5	0.0	0.6	341	1.1	0.0	0.3	254	0.5	0.0	51.0	13	77.4	0.1
12/29/09 20:30	1.5	468	2.7	0.1	0.3	400	0.5	0.0	0.6	343	1.1	0.0	0.3	257	0.5	0.0	51.0	13	77.4	0.1
12/29/09 21:00	1.0	473	1.8	0.0	0.3	405	0.5	0.0	0.7	347	1.3	0.0	0.3	260	0.5	0.0	56.0	13	88.5	0.1
12/29/09 21:30	1.1	478	2.0	0.1	0.4	409	0.7	0.0	0.8	351	1.4	0.0	0.4	263	0.7	0.0	39.0	14	58.2	0.0
12/29/09 22:00	1.3	473	2.4	0.1	0.4	406	0.7	0.0	1.2	348	2.2	0.0	0.6	263	1.1	0.0	36.0	14	53.5	0.0
12/29/09 22:30	1.1	489	2.0	0.1	0.3	417	0.5	0.0	0.8	356	1.4	0.0	0.4	266	0.7	0.0	47.0	14	71.0	0.1
12/29/09 23:00	2.3	484	4.2	0.1	0.5	413	0.9	0.0	0.9	353	1.6	0.0	0.4	263	0.7	0.0	58.0	14	88.7	0.1
12/29/09 23:30	2.5	494	4.6	0.1	0.4	420	0.7	0.0	1.2	357	2.2	0.0	0.3	257	0.5	0.0	19.0	14	27.1	0.0
12/30/09 0:00	2.1	489	3.9	0.1	0.6	415	1.1	0.0	1.4	353	2.6	0.1	0.4	260	0.7	0.0	14.0	13	19.6	0.0
12/30/09 0:30	3.2	489	5.9	0.2	0.6	414	1.1	0.0	1.9	351	3.5	0.1	0.4	257	0.7	0.0	18.0	13	25.6	0.0
12/30/09 1:00	2.5	494	4.6	0.1	0.6	418	1.1	0.0	1.9	354	3.5	0.1	0.3	257	0.5	0.0	18.0	13	25.6	0.0
12/30/09 1:30	2.8	489	5.2	0.1	0.7	414	1.3	0.0	1.9	351	3.5	0.1	0.4	257	0.7	0.0	15.0	13	21.1	0.0
12/30/09 2:00	2.5	494	4.6	0.1	1.1	417	2.0	0.0	1.8	352	3.3	0.1	0.3	254	0.5	0.0	9.4	13	12.8	0.0
12/30/09 2:30	2.0	499	3.7	0.1	1.0	420	1.8	0.0	1.8	354	3.3	0.1	0.4	254	0.7	0.0	9.3	13	12.7	0.0
12/30/09 3:00	2.2	494	4.0	0.1	1.5	417	2.7	0.1	1.7	352	3.1	0.1	0.3	254	0.5	0.0	10.0	13	13.7	0.0
12/30/09 3:30	2.3	489	4.2	0.1	1.2	413	2.2	0.1	1.4	350	2.6	0.1	0.3	254	0.5	0.0	13.0	13	18.1	0.0
12/30/09 4:00	2.2	489	4.0	0.1	1.4	413	2.6	0.1	1.1	350	2.0	0.0	0.4	254	0.7	0.0	14.0	13	19.6	0.0
12/30/09 4:30	2.3	489	4.2	0.1	1.3	414	2.4	0.1	1.0	351	1.8	0.0	0.4	257	0.7	0.0	11.0	13	15.2	0.0
12/30/09 5:00	2.5	494	4.6	0.1	1.1	418	2.0	0.0	1.0	354	1.8	0.0	0.3	257	0.5	0.0	9.2	13	12.6	0.0
12/30/09 5:30	2.3	494	4.2	0.1	1.1	418	2.0	0.0	0.9	354	1.6	0.0	0.3	257	0.5	0.0	9.8	13	13.4	0.0
12/30/09 6:00	2.4	494	4.4	0.1	0.7	418	1.3	0.0	0.9	354	1.6	0.0	0.3	257	0.5	0.0	19.0	13	27.1	0.0
12/30/09 6:30	2.3	499	4.2	0.1	0.7	421	1.3	0.0	0.7	356	1.3	0.0	0.3	257	0.5	0.0	8.7	13	11.8	0.0
12/30/09 7:00	2.4	499	4.4	0.1	0.6	422	1.1	0.0	0.9	357	1.6	0.0	0.4	260	0.7	0.0	7.4	13	10.0	0.0
12/30/09 7:30	2.2	510	4.0	0.1	3.0	429	5.6	0.1	0.8	362	1.4	0.0	0.3	260	0.5	0.0	6.3	13	8.4	0.0
12/30/09 8:00	2.4	515	4.4	0.1	0.6	433	1.1	0.0	1.3	364	2.4	0.0	0.4	260	0.7	0.0	18.0	13	25.6	0.0
12/30/09 8:30	2.9	515	5.4	0.2	0.7	433	1.3	0.0	1.2	364	2.2	0.0	0.4	260	0.7	0.0	18.0	13	25.6	0.0
12/30/09 9:00	2.6	521	4.8	0.1	0.7	437	1.3	0.0	0.8	366	1.4	0.0	0.4	260	0.7	0.0	12.0	13	16.6	0.0
12/30/09 9:30	2.9	526	5.4	0.2	0.6	439	1.1	0.0	0.7	367	1.3	0.0	0.4	257	0.7	0.0	11.0	13	15.2	0.0
12/30/09 10:00	2.7	526	5.0	0.1	0.5	439	0.9	0.0	1.0	367	1.8	0.0	0.3	257	0.5	0.0	9.1	13	12.4	0.0
12/30/09 10:30	2.7	531	5.0	0.1	0.6	443	1.1	0.0	0.9	369	1.6	0.0	0.3	257	0.5	0.0	7.3	13	9.8	0.0
12/30/09 11:00	4.0	537	7.4	0.2	0.5	447	0.9	0.0	1.0	371	1.8	0.0	0.3	257	0.5	0.0	7.4	13	10.0	0.0
12/30/09 11:30	3.1	537	5.7	0.2	0.6	447	1.1	0.0	0.7	371	1.3	0.0	0.3	257	0.5	0.0	6.9	13	9.2	0.0
12/30/09 12:00	2.3	526	4.2	0.1	1.0	439	1.8	0.0	0.7	367	1.3	0.0	0.5	257	0.9	0.0	7.8	13	10.5	0.0
12/30/09 12:30	2.9	531	5.4	0.2	0.6	442	1.1	0.0	0.9	367	1.6	0.0	0.3	254	0.5	0.0	15.0	13	21.1	0.0
12/30/09 13:00	2.8	526	5.2	0.2	0.6	438	1.1	0.0	0.8	365	1.4	0.0	0.3	254	0.5	0.0	10.0	13	13.7	0.0
12/30/09 13:30	2.5	526	4.6	0.1	0.7	439	1.3	0.0	0.7	367	1.3	0.0	0.3	257	0.5	0.0	7.8	13	10.5	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/30/09 14:00	3.3	526	6.1	0.2	0.4	439	0.7	0.0	0.8	367	1.4	0.0	0.3	257	0.5	0.0	6.4	13	8.5	0.0
12/30/09 14:30	2.5	521	4.6	0.1	0.7	436	1.3	0.0	0.7	364	1.3	0.0	0.3	257	0.5	0.0	8.7	13	11.8	0.0
12/30/09 15:00	2.5	526	4.6	0.1	0.9	440	1.6	0.0	0.6	368	1.1	0.0	0.3	260	0.5	0.0	8.4	13	11.4	0.0
12/30/09 15:30	2.3	521	4.2	0.1	0.9	437	1.6	0.0	0.6	366	1.1	0.0	0.4	260	0.7	0.0	11.0	260	13	15.2
12/30/09 16:00	2.3	526	4.2	0.1	0.6	440	1.1	0.0	0.6	368	1.1	0.0	0.3	260	0.5	0.0	9.5	13	13.0	0.0
12/30/09 16:30	2.2	521	4.0	0.1	0.4	436	0.7	0.0	0.7	364	1.3	0.0	0.3	257	0.5	0.0	13.0	13	18.1	0.0
12/30/09 17:00	2.7	521	5.0	0.1	0.7	437	1.3	0.0	0.7	366	1.3	0.0	0.3	260	0.5	0.0	12.0	260	13	16.6
12/30/09 17:30	2.2	521	4.0	0.1	0.7	437	1.3	0.0	0.6	366	1.1	0.0	0.4	260	0.7	0.0	18.0	13	25.6	0.0
12/30/09 18:00	2.2	521	4.0	0.1	0.5	437	0.9	0.0	0.7	366	1.3	0.0	0.8	260	1.4	0.0	9.9	260	13	13.6
12/30/09 18:30	3.9	521	7.3	0.2	0.5	437	0.9	0.0	0.7	366	1.3	0.0	0.4	260	0.7	0.0	10.0	13	13.7	0.0
12/30/09 19:00	2.0	526	3.7	0.1	0.4	441	0.7	0.0	0.6	370	1.1	0.0	0.5	263	0.9	0.0	10.0	14	13.7	0.0
12/30/09 19:30	2.6	526	4.8	0.1	0.4	441	0.7	0.0	0.6	370	1.1	0.0	0.4	263	0.7	0.0	24.0	14	34.8	0.0
12/30/09 20:00	2.3	521	4.2	0.1	0.6	438	1.1	0.0	0.7	368	1.3	0.0	0.5	263	0.9	0.0	31.0	14	45.6	0.0
12/30/09 20:30	2.2	521	4.0	0.1	0.4	438	0.7	0.0	0.7	368	1.3	0.0	0.4	263	0.7	0.0	26.0	14	37.8	0.0
12/30/09 21:00	3.0	521	5.6	0.2	0.5	438	0.9	0.0	0.8	368	1.4	0.0	0.3	263	0.5	0.0	12.0	14	16.6	0.0
12/30/09 21:30	3.3	521	6.1	0.2	0.6	441	1.1	0.0	0.7	370	1.3	0.0	0.3	263	0.5	0.0	8.7	14	11.8	0.0
12/30/09 22:00	2.1	526	3.9	0.1	0.4	440	0.7	0.0	0.7	368	1.3	0.0	0.3	260	0.5	0.0	7.7	13	10.4	0.0
12/30/09 22:30	3.0	526	5.6	0.2	0.6	440	1.1	0.0	0.7	368	1.3	0.0	0.3	260	0.5	0.0	10.0	13	13.7	0.0
12/30/09 23:00	2.4	526	4.4	0.1	0.6	439	1.1	0.0	1.0	367	1.8	0.0	0.3	257	0.5	0.0	9.5	260	13	13.0
12/30/09 23:30	2.5	526	4.6	0.1	0.4	440	0.7	0.0	1.0	368	1.8	0.0	0.4	260	0.7	0.0	10.0	13	13.7	0.0
12/31/09 00:00	2.6	521	4.8	0.1	0.8	436	1.4	0.0	1.0	364	1.8	0.0	0.6	257	1.1	0.0	7.5	13	10.1	0.0
12/31/09 00:30	2.2	526	4.0	0.1	0.4	439	0.7	0.0	1.2	367	2.2	0.0	0.3	257	0.5	0.0	9.0	13	12.3	0.0
12/31/09 1:00	3.5	521	6.5	0.2	0.6	436	1.1	0.0	1.0	364	1.8	0.0	0.3	257	0.5	0.0	9.7	13	13.3	0.0
12/31/09 1:30	3.4	526	6.3	0.2	0.8	438	1.4	0.0	0.9	365	1.6	0.0	0.4	254	0.7	0.0	9.3	13	12.7	0.0
12/31/09 2:00	2.5	515	4.6	0.1	1.1	431	2.0	0.0	0.7	360	1.3	0.0	0.5	254	0.9	0.0	12.0	13	16.6	0.0
12/31/09 2:30	1.6	515	2.9	0.1	0.5	431	0.9	0.0	0.9	360	1.6	0.0	0.3	254	0.5	0.0	14.0	13	19.6	0.0
12/31/09 3:00	2.1	515	3.9	0.1	0.8	430	1.4	0.0	0.7	359	1.3	0.0	0.4	252	0.7	0.0	12.0	13	16.6	0.0
12/31/09 3:30	2.8	510	5.2	0.1	0.4	427	0.7	0.0	0.6	357	1.1	0.0	0.4	252	0.7	0.0	12.0	13	16.6	0.0
12/31/09 4:00	2.4	510	4.4	0.1	0.4	427	0.7	0.0	0.6	357	1.1	0.0	0.4	252	0.7	0.0	13.0	13	18.1	0.0
12/31/09 4:30	2.0	504	3.7	0.1	0.4	423	0.7	0.0	0.6	354	1.1	0.0	0.3	252	0.5	0.0	12.0	13	16.6	0.0
12/31/09 5:00	2.2	504	4.0	0.1	0.3	422	0.5	0.0	0.7	353	1.3	0.0	0.4	249	0.7	0.0	9.9	13	13.6	0.0
12/31/09 5:30	2.1	510	3.9	0.1	0.4	426	0.7	0.0	0.6	355	1.3	0.0	0.4	249	0.5	0.0	21.0	13	30.2	0.0
12/31/09 6:00	2.5	510	4.6	0.1	0.4	426	0.7	0.0	0.7	355	1.3	0.0	0.4	249	0.7	0.0	17.0	13	24.1	0.0
12/31/09 6:30	2.2	510	4.0	0.1	0.4	427	0.7	0.0	0.6	357	1.1	0.0	0.3	252	0.5	0.0	11.0	13	15.2	0.0
12/31/09 7:00	2.2	510	4.0	0.1	0.4	427	0.7	0.0	0.6	357	1.1	0.0	0.3	252	0.5	0.0	14.0	13	19.6	0.0
12/31/09 7:30	2.0	515	3.7	0.1	0.4	430	0.7	0.0	0.8	359	1.4	0.0	0.3	252	0.5	0.0	14.0	13	19.6	0.0
12/31/09 8:00	2.2	515	4.0	0.1	0.5	431	0.9	0.0	0.9	360	1.6	0.0	0.4	254	0.7	0.0	17.0	13	24.1	0.0
12/31/09 8:30	3.0	521	5.6	0.2	0.5	436	0.9	0.0	0.7	364	1.3	0.0	0.4	257	0.7	0.0	15.0	13	21.1	0.0
12/31/09 9:00	2.4	526	4.4	0.1	0.6	440	1.1	0.0	1.0	368	1.8	0.0	0.3	260	0.5	0.0	15.0	13	21.1	0.0
12/31/09 9:30	3.5	537	6.5	0.2	0.6	450	1.1	0.0	1.2	378	2.2	0.0	0.3	269	0.5	0.0	26.0	14	37.8	0.0
12/31/09 10:00	2.3	548	4.2	0.1	0.7	459	1.3	0.0	1.0	384	1.8	0.0	0.4	272	0.7	0.0	46.0	14	69.4	0.1
12/31/09 10:30	2.7	559	5.0	0.2	1.2	470	2.2	0.1	1.2	396	2.2	0.0	0.4	283	0.7	0.0	57.0	15	87.1	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
12/31/09 11:00	2.6	576	4.8	0.2	1.8	488	3.3	0.1	1.5	413	2.7	0.1	0.6	302	1.1	0.0	1300	15	209.1	0.2
12/31/09 11:30	3.0	593	5.6	0.2	2.5	508	4.6	0.1	2.0	436	3.7	0.1	0.5	327	0.9	0.0	320.0	17	544.2	0.5
12/31/09 12:00	3.6	611	6.7	0.2	2.6	533	4.8	0.1	2.4	467	4.4	0.1	0.5	368	0.9	0.0	750.0	19	1344.9	1.4
12/31/09 12:30	3.0	641	5.6	0.2	3.6	571	6.7	0.2	2.7	512	5.0	0.1	0.8	423	1.4	0.0	1060.0	21	1942.0	2.3
12/31/09 13:00	4.3	680	8.0	0.3	4.8	626	9.0	0.3	3.6	580	6.7	0.2	0.9	512	1.6	0.0	1060.0	25	1942.0	2.8
12/31/09 13:30	4.8	727	9.0	0.4	6.5	690	12.2	0.5	4.8	659	9.0	0.3	0.8	612	1.4	0.0	1060.0	30	1942.0	3.3
12/31/09 14:00	7.6	791	14.3	0.6	6.9	785	13.0	0.6	7.6	779	14.3	0.6	1.4	771	2.6	0.1	1060.0	37	1942.0	4.1
12/31/09 14:30	9.2	843	17.4	0.8	10.1	876	19.1	0.9	34.1	904	66.2	3.4	1.4	946	2.6	0.1	1060.0	45	1942.0	4.9
12/31/09 15:00	10.0	953	19.0	1.0	13.6	1028	25.9	1.5	73.1	1091	144.2	8.8	1.7	1185	3.1	0.2	910.0	56	1651.5	5.2
12/31/09 15:30	11.0	1067	20.9	1.3	27.7	1208	53.6	3.6	82.8	1327	163.7	12.2	1.3	1506	2.4	0.2	1060.0	70	1942.0	7.7
12/31/09 16:00	17.0	1258	32.6	2.3	67.7	1459	133.3	10.9	74.5	1629	147.0	13.5	2.4	1883	4.4	0.5	860.0	87	1555.3	7.6
12/31/09 16:30	18.0	1506	34.5	2.9	83.0	1748	164.1	16.1	76.7	1953	151.4	16.6	3.1	2259	5.7	0.7	800.0	103	1440.3	8.3
12/31/09 17:00	23.0	1917	44.3	4.8	80.1	2144	158.3	19.1	88.2	2334	174.6	22.9	3.9	2620	7.3	1.1	610.0	118	1079.9	7.2
12/31/09 17:30	29.0	2311	56.1	7.3	79.6	2513	157.3	22.2	53.9	2683	105.7	15.9	4.2	2939	7.8	1.3	510.0	132	892.9	6.6
12/31/09 18:00	33.0	2649	64.1	9.5	66.8	2799	131.5	20.7	41.0	2925	79.9	13.1	5.5	3114	10.3	1.8	480.0	139	837.2	6.5
12/31/09 18:30	56.0	3154	109.9	19.5	54.4	3195	106.7	19.1	36.6	3229	71.2	12.9	6.3	3281	11.8	2.2	320.0	146	544.2	4.5
12/31/09 19:00	74.0	3551	146.0	29.1	46.8	3502	91.5	18.0	61.7	3461	121.3	23.6	6.9	3400	13.0	2.5	270.0	151	454.4	3.9
12/31/09 19:30	71.0	3728	139.9	29.3	52.6	3618	103.1	21.0	31.2	3525	60.5	12.0	4.1	3386	7.6	1.5	240.0	150	401.0	3.4
12/31/09 20:00	76.0	4065	150.0	34.3	39.6	3847	77.1	16.7	30.7	3672	39.8	8.2	4.4	3294	8.2	1.6	240.0	150	401.0	3.4
12/31/09 20:30	61.0	4223	119.9	28.4	47.6	3924	93.1	20.5	20.7	3672	39.8	8.2	4.4	3294	8.2	1.5	160.0	147	260.7	2.1
12/31/09 21:00	57.0	4276	111.9	26.9	33.4	3939	64.8	14.4	21.9	3655	42.2	8.7	3.2	3229	5.9	1.1	130.0	144	209.1	1.7
12/31/09 21:30	56.0	4048	109.9	25.0	29.7	3764	57.5	12.2	20.4	3524	39.2	7.8	2.9	3164	5.4	1.0	120.0	141	192.0	1.5
12/31/09 22:00	51.0	4014	99.9	22.5	25.7	3732	49.6	10.4	14.2	3495	27.1	5.3	3.1	3139	5.7	1.0	130.0	140	209.1	1.6
12/31/09 22:30	46.0	4152	89.9	21.0	23.6	3802	45.5	9.7	12.8	3506	24.4	4.8	2.8	3063	5.2	0.9	140.0	137	226.2	1.7
12/31/09 23:00	42.0	3861	81.9	17.8	18.9	3588	36.3	7.3	14.2	3358	27.1	5.1	3.0	3013	5.6	0.9	110.0	135	175.1	1.3
12/31/09 23:30	39.0	3895	76.0	16.6	20.9	3599	40.2	8.1	13.2	3350	25.2	4.7	2.4	2976	4.4	0.7	97.0	133	153.2	1.1
1/1/10 00:00	32.0	3535	62.1	12.3	18.8	3351	36.1	6.8	12.0	3196	22.8	4.1	1.9	2964	3.5	0.6	100.0	133	158.2	1.2
1/1/10 03:00	28.0	3794	54.2	11.6	17.8	3515	34.1	6.7	11.0	3280	20.9	3.9	2.3	2927	4.2	0.7	95.0	131	149.8	1.1
1/1/10 1:00	27.0	4065	52.2	11.9	18.5	3695	35.5	7.4	11.9	3383	22.6	4.3	3.4	2915	6.3	1.0	120.0	131	192.0	1.4
1/1/10 1:30	26.0	3663	50.2	10.3	14.4	3426	27.5	5.3	11.8	3226	22.4	4.1	1.6	2927	2.9	0.5	84.0	131	131.5	1.0
1/1/10 2:00	24.0	3861	46.3	10.0	14.8	3552	28.3	5.6	11.8	3293	22.4	4.2	1.8	2903	3.3	0.5	80.0	130	124.8	0.9
1/1/10 2:30	26.0	3895	50.2	11.0	13.5	3591	25.7	5.2	11.1	3335	21.1	4.0	2.1	2951	3.9	0.6	74.0	132	114.9	0.9
1/1/10 3:00	22.0	3980	42.4	9.5	17.5	3656	33.5	6.9	9.2	3384	17.4	3.3	2.0	2976	3.7	0.6	180.0	133	295.4	2.2
1/1/10 3:30	22.0	3844	42.4	9.2	14.3	3545	27.3	5.4	9.2	3293	17.4	3.2	1.8	2915	3.3	0.5	320.0	131	544.2	4.0
1/1/10 4:00	21.0	3728	40.4	8.5	14.0	3458	26.7	5.2	30.2	3231	58.5	10.6	2.1	2891	3.9	0.6	220.0	130	365.6	2.7
1/1/10 4:30	22.0	3828	42.4	9.1	21.6	3530	41.6	8.2	26.9	3279	52.0	9.6	1.8	2903	3.3	0.5	130.0	130	209.1	1.5
1/1/10 5:00	21.0	3488	40.4	7.9	40.4	3296	78.7	14.6	16.3	3134	31.2	5.5	1.8	2891	3.3	0.5	97.0	130	153.2	1.1
1/1/10 5:30	20.0	3980	38.4	8.6	19.6	3617	37.7	7.7	13.7	3312	26.1	4.9	2.3	2854	4.2	0.7	110.0	128	175.1	1.3
1/1/10 6:00	23.0	3929	44.3	9.8	17.2	3586	33.0	6.6	11.7	3298	22.2	4.1	1.7	2866	3.1	0.5	80.0	129	124.8	0.9
1/1/10 6:30	21.0	3551	40.4	8.1	16.6	3326	31.8	5.9	13.2	3138	25.2	4.4	2.3	2854	4.2	0.7	71.0	128	110.0	0.8
1/1/10 7:00	35.0	3811	68.0	14.6	13.3	3499	25.4	5.0	8.9	3236	16.8	3.1	2.0	2842	3.7	0.6	76.0	128	118.2	0.8
1/1/10 7:30	26.0	3646	50.2	10.3	13.5	3395	25.7	4.9	9.4	3184	17.8	3.2	1.7	2866	3.1	0.5	66.0	129	101.8	0.7

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/1/10 8:00	21.0	3695	40.4	8.4	12.6	3421	24.0	4.6	8.9	3189	16.8	3.0	1.6	2842	2.9	0.5	110.0	128	175.1	1.3
1/1/10 8:30	19.0	3614	36.5	7.4	12.1	3373	23.0	4.4	8.7	3171	16.4	2.9	1.7	2866	3.1	0.5	88.0	129	138.1	1.0
1/1/10 9:00	18.0	3745	34.5	7.3	11.5	3458	21.9	4.2	10.2	3216	19.3	3.5	2.1	2854	3.9	0.6	55.0	128	83.9	0.6
1/1/10 9:30	16.0	3712	30.6	6.4	10.0	3436	19.0	3.7	9.5	3203	18.0	3.2	1.8	2854	3.3	0.5	57.0	128	87.1	0.6
1/1/10 10:00	18.0	3630	34.5	7.0	11.2	3365	21.3	4.0	9.7	3141	18.4	3.2	1.6	2806	2.9	0.5	51.0	126	77.4	0.5
1/1/10 10:30	16.0	3551	30.6	6.1	10.1	3307	19.1	3.6	8.1	3102	15.3	2.7	1.8	2795	3.3	0.5	53.0	126	80.6	0.6
1/1/10 11:00	15.0	3761	28.7	6.1	10.3	3450	19.5	3.8	7.8	3188	14.7	2.6	2.1	2795	3.9	0.6	53.0	126	80.6	0.6
1/1/10 11:30	18.0	3663	34.5	7.1	9.5	3372	18.0	3.4	8.1	3127	15.3	2.7	1.5	2759	2.7	0.4	47.0	124	71.0	0.5
1/1/10 12:00	16.0	3614	30.6	6.2	9.8	3335	18.6	3.5	8.6	3100	16.3	2.8	2.0	2747	3.7	0.6	50.0	124	75.8	0.5
1/1/10 12:30	14.0	3364	26.7	5.1	9.5	3143	18.0	3.2	7.0	2957	13.2	2.2	2.2	2677	4.0	0.6	47.0	121	71.0	0.5
1/1/10 13:00	13.0	3519	24.8	4.9	10.6	3241	20.1	3.7	8.7	3006	16.4	2.8	1.7	2654	3.1	0.5	42.0	120	63.0	0.4
1/1/10 13:30	14.0	3472	26.7	5.2	8.9	3202	16.8	3.0	8.4	2973	15.9	2.7	1.8	2631	3.3	0.5	42.0	119	63.0	0.4
1/1/10 14:00	12.0	3441	22.8	4.4	12.1	3181	23.0	4.1	9.0	2961	17.0	2.8	1.5	2631	2.7	0.4	43.0	119	64.6	0.4
1/1/10 14:30	13.0	3472	24.8	4.8	8.1	3194	15.3	2.7	13.9	2960	26.5	4.4	1.6	2608	2.9	0.4	51.0	118	77.4	0.5
1/1/10 15:00	12.0	3551	22.8	4.6	7.6	3244	14.3	2.6	5.9	2985	11.1	1.9	4.8	2597	9.0	1.3	46.0	117	69.4	0.5
1/1/10 15:30	11.0	3519	20.9	4.1	10.0	3204	19.0	3.4	6.8	2939	12.8	2.1	1.5	2541	2.7	0.4	43.0	115	64.6	0.4
1/1/10 16:00	12.0	3519	22.8	4.5	9.4	3211	17.8	3.2	8.0	2952	15.1	2.5	2.1	2563	3.9	0.6	49.0	116	74.2	0.5
1/1/10 16:30	11.0	3457	20.9	4.1	8.0	3155	15.1	2.7	9.2	2900	17.4	2.8	1.4	2518	2.6	0.4	59.0	114	90.3	0.6
1/1/10 17:00	11.0	3426	20.9	4.0	7.9	3134	14.9	2.6	6.3	2888	11.8	1.9	1.5	2518	2.7	0.4	58.0	114	88.7	0.6
1/1/10 17:30	11.0	3441	20.9	4.0	8.1	3148	15.3	2.7	7.2	2900	13.6	2.2	1.6	2529	2.9	0.4	42.0	114	63.0	0.4
1/1/10 18:00	10.0	3349	19.0	3.6	7.4	3085	13.9	2.4	6.6	2863	12.4	2.0	1.2	2529	2.2	0.3	39.0	114	58.2	0.4
1/1/10 18:30	10.0	3334	19.0	3.6	7.8	3075	14.7	2.5	6.9	2857	13.0	2.1	1.3	2529	2.4	0.3	34.0	114	50.3	0.3
1/1/10 19:00	10.0	3184	19.0	3.4	7.3	2973	13.7	2.3	5.7	2796	10.7	1.7	1.3	2529	2.4	0.3	37.0	114	55.0	0.4
1/1/10 19:30	11.0	3243	20.9	3.8	7.3	3010	13.7	2.3	5.3	2813	9.9	1.6	1.7	2518	3.1	0.4	47.0	114	71.0	0.5
1/1/10 20:00	10.0	3426	19.0	3.6	6.8	3134	12.8	2.3	6.6	2888	12.4	2.0	1.6	2518	2.9	0.4	92.0	114	144.8	0.9
1/1/10 20:30	9.9	3243	18.8	3.4	8.3	3024	15.7	2.7	14.7	2840	28.1	4.5	1.8	2563	3.3	0.5	96.0	116	151.5	1.0
1/1/10 21:00	9.6	3410	18.2	3.5	6.7	3152	12.6	2.2	7.9	2935	14.9	2.5	1.5	2608	2.7	0.4	56.0	118	85.5	0.6
1/1/10 21:30	9.1	3319	17.2	3.2	7.2	3108	13.6	2.4	15.0	2931	28.7	4.7	1.5	2666	2.7	0.4	51.0	120	77.4	0.5
1/1/10 22:00	9.8	3273	18.6	3.4	9.0	3100	17.0	3.0	9.6	2954	18.2	3.0	1.4	2736	2.6	0.4	89.0	123	139.8	1.0
1/1/10 22:30	8.6	3303	16.3	3.0	8.3	3128	15.7	2.8	6.3	2981	11.8	2.0	1.9	2759	3.5	0.5	42.0	124	63.0	0.4
1/1/10 23:00	8.7	3273	16.4	3.0	7.8	3123	14.7	2.6	8.1	2996	15.3	2.6	1.9	2806	3.5	0.5	36.0	126	53.5	0.4
1/2/10 0:00	9.7	3303	18.4	3.4	8.5	3143	16.1	2.8	10.8	3009	20.5	3.5	2.2	2806	4.0	0.6	33.0	126	48.7	0.3
1/2/10 0:30	11.0	3334	20.9	3.9	8.2	3137	15.5	2.7	6.2	2972	11.6	1.9	1.7	2724	3.1	0.5	47.0	123	71.0	0.5
1/2/10 1:00	12.0	3457	22.8	4.4	7.9	3228	14.9	2.7	6.5	3036	12.2	2.1	1.9	2747	3.5	0.5	40.0	124	59.8	0.4
1/2/10 1:30	14.0	3426	26.7	5.1	7.2	3204	13.6	2.4	6.2	3016	11.6	2.0	1.9	2736	3.5	0.5	47.0	123	71.0	0.5
1/2/10 2:00	10.0	3426	19.0	3.6	9.5	3200	18.0	3.2	6.9	3009	13.0	2.2	1.9	2724	3.5	0.5	50.0	123	75.8	0.5
1/2/10 2:30	11.0	3551	20.9	4.2	7.3	3266	13.7	2.5	10.2	3026	19.3	3.3	3.1	2666	3.1	0.5	41.0	120	61.4	0.4
1/2/10 3:00	9.2	3457	17.4	3.4	6.9	3198	13.0	2.3	13.5	2981	25.7	4.3	2.1	2654	3.9	0.6	32.0	120	47.2	0.3
1/2/10 3:30	13.0	3395	24.8	4.7	7.5	3138	14.1	2.5	6.3	2922	11.8	1.9	1.7	2597	3.1	0.5	42.0	117	63.0	0.4
1/2/10 4:00	9.4	3288	17.8	3.3	8.1	3055	15.3	2.6	5.9	2858	11.1	1.8	1.5	2563	2.7	0.4	66.0	116	101.8	0.7
1/2/10 4:30	10.0	3364	19.0	3.6	7.5	3092	14.1	2.5	21.6	2862	41.6	6.7	2.5	2518	4.6	0.7	30.0	114	44.0	0.3
1/2/10 4:30	9.9	3334	18.8	3.5	7.2	3057	13.6	2.3	6.0	2824	11.3	1.8	1.3	2474	2.4	0.3	28.0	112	40.9	0.3

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/2/10 5:00	9.1	3410	17.2	3.3	6.2	3095	11.6	2.0	8.8	2829	16.6	2.6	1.6	2430	2.9	0.4	32.0	110	47.2	0.3
1/2/10 5:30	9.6	3319	18.2	3.4	6.2	3022	11.6	2.0	6.8	2772	12.8	2.0	1.4	2397	2.6	0.3	31.0	109	45.6	0.3
1/2/10 6:00	9.3	3273	17.6	3.2	5.7	2974	10.7	1.8	4.8	2722	9.0	1.4	1.7	2344	3.1	0.4	29.0	106	42.5	0.3
1/2/10 6:30	11.0	3243	20.9	3.8	5.7	2936	10.7	1.8	6.2	2678	11.6	1.8	1.2	2291	2.2	0.3	41.0	104	61.4	0.4
1/2/10 7:00	8.4	3124	15.9	2.8	5.3	2853	9.9	1.6	6.0	2624	11.3	1.7	1.1	2280	2.0	0.3	65.0	104	100.1	0.6
1/2/10 7:30	8.5	2994	16.1	2.7	6.1	2750	11.4	1.8	6.0	2546	11.3	1.6	1.2	2238	2.2	0.3	32.0	102	47.2	0.3
1/2/10 8:00	8.0	3154	15.1	2.7	5.7	2846	10.7	1.7	6.3	2586	11.8	1.7	1.3	2197	2.4	0.3	30.0	100	44.0	0.2
1/2/10 8:30	9.7	3095	18.4	3.2	5.5	2796	10.3	1.6	5.4	2544	10.1	1.4	1.0	2166	1.8	0.2	28.0	99	40.9	0.2
1/2/10 9:00	7.8	2965	14.7	2.5	6.4	2692	12.0	1.8	5.1	2461	9.5	1.3	1.2	2116	2.2	0.3	25.0	97	36.3	0.2
1/2/10 9:30	7.9	2994	14.9	2.5	5.7	2698	10.7	1.6	4.5	2449	8.4	1.2	1.2	2076	2.2	0.3	28.0	95	40.9	0.2
1/2/10 10:00	8.3	2994	15.7	2.6	5.5	2682	10.3	1.6	5.4	2420	10.1	1.4	1.3	2026	2.4	0.3	26.0	93	37.8	0.2
1/2/10 10:30	8.5	2937	16.1	2.7	7.7	2643	14.5	2.2	4.8	2397	9.0	1.2	1.2	2026	2.2	0.2	24.0	93	34.8	0.2
1/2/10 11:00	8.7	2937	16.4	2.7	5.1	2628	9.5	1.4	4.5	2368	8.4	1.1	1.0	1978	1.8	0.2	28.0	91	40.9	0.2
1/2/10 11:30	7.5	2763	14.1	2.2	5.5	2498	10.3	1.4	4.1	2275	7.6	1.0	0.9	1940	1.6	0.2	31.0	89	45.6	0.2
1/2/10 12:00	7.3	2821	13.7	2.2	4.2	2531	7.8	1.1	5.7	2287	10.7	1.4	0.9	1920	1.6	0.2	150.0	88	243.4	1.2
1/2/10 12:30	10.0	2706	19.0	2.9	4.6	2438	8.6	1.2	4.3	2212	8.0	1.0	0.9	1873	1.6	0.2	46.0	86	69.4	0.3
1/2/10 13:00	6.9	2851	13.0	2.1	5.6	2527	10.5	1.5	4.5	2254	8.4	1.1	1.0	1846	1.8	0.2	33.0	85	48.7	0.2
1/2/10 13:30	7.1	2593	13.4	1.9	4.3	2347	8.0	1.1	6.4	2139	12.0	1.4	0.9	1827	1.6	0.2	25.0	84	36.3	0.2
1/2/10 14:00	6.5	2635	12.2	1.8	5.2	2363	9.7	1.3	5.1	2134	9.5	1.1	1.1	1791	2.0	0.2	22.0	83	31.7	0.1
1/2/10 14:30	6.2	2593	11.6	1.7	5.8	2326	10.9	1.4	4.3	2101	8.0	0.9	0.9	1763	1.6	0.2	22.0	81	31.7	0.1
1/2/10 15:00	6.5	2749	12.2	1.9	4.5	2429	8.4	1.1	4.0	2159	7.4	0.9	0.8	1754	1.4	0.1	21.0	81	30.2	0.1
1/2/10 15:30	5.5	2663	10.3	1.5	4.2	2362	7.8	1.0	3.7	2108	6.9	0.8	0.7	1728	1.3	0.1	52.0	80	79.0	0.4
1/2/10 16:00	5.9	2607	11.1	1.6	3.3	2310	6.1	0.8	3.6	2059	6.7	0.8	0.7	1683	1.3	0.1	24.0	78	34.8	0.2
1/2/10 16:30	6.2	2607	11.6	1.7	3.9	2299	7.3	0.9	3.9	2039	7.3	0.8	0.8	1649	1.4	0.1	36.0	76	53.5	0.2
1/2/10 17:00	7.3	2593	13.7	2.0	3.4	2286	6.3	0.8	4.0	2028	7.4	0.8	0.7	1640	1.3	0.1	26.0	76	37.8	0.2
1/2/10 17:30	6.0	2416	11.3	1.5	4.1	2163	7.6	0.9	4.2	1951	7.8	0.9	0.8	1631	1.4	0.1	29.0	76	42.5	0.2
1/2/10 18:30	4.7	2416	8.8	1.2	4.2	2144	7.8	0.9	3.5	1946	6.5	0.7	1.0	1606	1.8	0.2	140.0	75	226.2	0.9
1/2/10 19:00	5.6	2376	10.5	1.4	3.4	2112	6.3	0.7	3.5	1889	6.5	0.7	0.8	1572	1.4	0.1	65.0	73	100.1	0.4
1/2/10 19:30	5.5	2376	10.3	1.4	4.6	2106	8.6	1.0	6.0	1879	11.3	1.2	1.0	1539	1.8	0.2	50.0	72	75.8	0.3
1/2/10 20:00	4.9	2337	9.2	1.2	3.9	2069	7.3	0.8	5.2	1844	9.7	1.0	0.7	1506	1.3	0.1	26.0	72	37.8	0.2
1/2/10 20:30	5.1	2298	9.5	1.2	5.1	2035	9.5	1.1	4.0	1813	7.4	0.8	1.1	1481	2.0	0.2	41.0	70	61.4	0.2
1/2/10 21:00	4.7	2298	8.8	1.1	4.5	2029	8.4	1.0	3.5	1804	6.5	0.7	0.7	1465	1.3	0.1	37.0	69	55.0	0.2
1/2/10 21:30	4.8	2337	9.0	1.2	3.2	2048	5.9	0.7	3.7	1805	6.9	0.7	0.6	1441	1.1	0.1	29.0	68	42.5	0.2
1/2/10 22:00	4.9	2259	9.2	1.2	3.9	1988	7.3	0.8	3.5	1759	6.5	0.6	0.7	1417	1.3	0.1	21.0	67	30.2	0.1
1/2/10 22:30	5.1	2324	9.5	1.2	4.3	2024	8.0	0.9	4.0	1772	7.4	0.7	0.6	1394	1.1	0.1	31.0	66	45.6	0.2
1/2/10 23:00	6.4	2324	12.0	1.6	3.4	2022	6.3	0.7	3.0	1767	5.6	0.6	1.3	1386	2.4	0.2	42.0	65	63.0	0.2
1/2/10 23:30	5.5	2208	10.3	1.3	2.9	1933	5.4	0.6	3.2	1702	5.9	0.6	0.7	1355	1.3	0.1	32.0	65	47.2	0.2
1/3/10 0:00	5.3	2220	9.9	1.2	2.6	1939	4.8	0.5	3.6	1702	6.7	0.6	0.8	1347	1.4	0.1	23.0	64	33.2	0.1
1/3/10 0:30	5.8	2195	10.9	1.3	3.2	1912	5.9	0.6	3.3	1674	6.1	0.6	0.6	1317	1.1	0.1	26.0	63	37.8	0.1
1/3/10 1:00	4.8	2106	9.0	1.1	3.2	1851	5.9	0.6	3.5	1638	6.5	0.6	0.6	1317	1.1	0.1	20.0	62	28.6	0.1
1/3/10 1:30	5.0	2169	9.3	1.1	2.6	1885	4.8	0.5	3.0	1646	5.6	0.5	0.6	1287	1.1	0.1	22.0	61	31.7	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/3/10 2:00	3.8	2131	7.1	0.8	2.8	1857	5.2	0.5	3.1	1626	5.7	0.5	0.5	1279	0.9	0.1	23.0	60	33.2	0.1
1/3/10 2:30	4.4	2106	8.2	1.0	2.5	1832	4.6	0.5	3.0	1602	5.6	0.5	0.5	0.9	1.6	0.1	28.0	59	40.9	0.1
1/3/10 3:00	4.1	2031	7.6	0.9	2.6	1781	4.8	0.5	2.7	1572	5.0	0.4	0.1	0.5	1257	0.9	28.0	59	40.9	0.1
1/3/10 3:30	4.4	2043	8.2	0.9	2.4	1783	4.4	0.4	2.7	1564	5.0	0.4	0.4	0.7	1235	1.3	24.0	58	34.8	0.1
1/3/10 4:00	4.3	2018	8.0	0.9	2.9	1759	5.4	0.5	3.2	1541	5.9	0.5	0.5	0.6	1213	1.1	24.0	57	34.8	0.1
1/3/10 4:30	3.8	1981	7.1	0.8	3.0	1732	5.6	0.5	3.6	1522	6.7	0.6	0.6	0.6	1206	1.1	34.0	57	50.3	0.2
1/3/10 5:00	3.8	1969	7.1	0.8	2.6	1719	4.8	0.5	3.0	1508	5.6	0.5	0.5	0.6	1192	1.1	25.0	56	36.3	0.1
1/3/10 5:30	3.5	1931	6.5	0.7	2.4	1684	4.4	0.4	2.9	1476	5.4	0.4	0.4	0.6	1164	1.1	17.0	55	24.1	0.1
1/3/10 6:00	3.8	2006	7.1	0.8	2.5	1730	4.6	0.4	2.7	1498	5.0	0.4	0.4	0.6	1150	1.1	16.0	54	22.6	0.1
1/3/10 6:30	3.6	1890	6.7	0.7	2.5	1652	4.6	0.4	4.1	1451	7.6	0.6	0.6	0.7	1150	1.3	18.0	54	25.6	0.1
1/3/10 7:00	4.0	1876	7.4	0.8	2.7	1638	5.0	0.5	2.8	1437	5.2	0.4	0.4	0.5	1136	0.9	21.0	54	30.2	0.1
1/3/10 7:30	3.7	1904	6.9	0.7	2.8	1645	5.2	0.5	2.7	1428	5.0	0.4	0.4	0.6	1102	1.1	20.0	52	28.6	0.1
1/3/10 8:00	3.5	1836	6.5	0.7	2.1	1600	3.9	0.3	2.7	1400	5.0	0.4	0.4	0.6	1102	1.1	16.0	52	22.6	0.1
1/3/10 8:30	3.7	1823	6.9	0.7	2.3	1588	4.2	0.4	2.5	1391	4.6	0.4	0.4	0.6	1095	1.1	18.0	52	25.6	0.1
1/3/10 9:00	3.5	1783	6.5	0.7	2.0	1553	3.7	0.3	2.4	1359	4.4	0.3	0.5	0.5	1068	0.9	20.0	51	28.6	0.1
1/3/10 9:30	3.3	1757	6.1	0.6	2.8	1533	5.2	0.4	2.9	1344	5.4	0.4	0.4	0.6	1061	1.1	20.0	50	28.6	0.1
1/3/10 10:00	3.3	1783	6.1	0.6	2.1	1551	3.9	0.3	2.5	1355	4.6	0.4	0.4	0.7	1061	1.3	26.0	50	37.8	0.1
1/3/10 10:30	3.5	1693	6.5	0.6	1.8	1481	3.3	0.3	2.3	1302	4.2	0.3	0.6	0.6	1035	1.1	19.0	49	27.1	0.1
1/3/10 11:00	3.7	1757	6.9	0.7	2.1	1524	3.9	0.3	2.3	1329	4.2	0.3	0.6	0.6	1035	1.1	13.0	49	18.1	0.1
1/3/10 11:30	3.2	1705	5.9	0.6	1.7	1485	3.1	0.3	2.5	1300	4.6	0.3	0.6	0.6	1022	1.1	15.0	49	21.1	0.1
1/3/10 12:00	4.3	1693	8.0	0.8	2.1	1472	3.9	0.3	2.7	1287	5.0	0.4	0.4	0.7	1009	1.3	17.0	48	24.1	0.1
1/3/10 12:30	3.2	1718	5.9	0.6	2.0	1486	3.7	0.3	2.5	1290	4.6	0.3	0.6	0.6	996	1.1	15.0	48	21.1	0.1
1/3/10 13:00	3.0	1654	5.6	0.5	2.3	1438	4.2	0.3	2.4	1256	4.4	0.3	0.6	0.6	983	1.1	20.0	47	28.6	0.1
1/3/10 13:30	3.0	1667	5.6	0.5	1.6	1443	2.9	0.2	3.2	1254	5.9	0.4	0.4	0.4	971	0.7	23.0	46	33.2	0.1
1/3/10 14:00	2.9	1629	5.4	0.5	1.7	1413	3.1	0.2	2.2	1231	4.0	0.3	0.6	0.6	958	1.1	19.0	46	27.1	0.1
1/3/10 14:30	3.0	1654	5.6	0.5	1.6	1432	2.9	0.2	3.0	1245	5.6	0.4	0.5	0.5	964	0.9	19.0	46	27.1	0.1
1/3/10 15:00	2.6	1629	4.8	0.4	1.8	1411	3.3	0.3	3.2	1227	5.9	0.4	0.6	0.6	952	1.1	23.0	46	33.2	0.1
1/3/10 15:30	2.9	1591	5.4	0.5	1.8	1382	3.3	0.3	3.0	1205	5.6	0.4	0.5	0.5	940	0.9	26.0	45	37.8	0.1
1/3/10 16:00	3.9	1591	7.3	0.6	2.3	1378	4.2	0.3	2.2	1197	4.0	0.3	0.4	0.4	927	0.7	17.0	44	24.1	0.1
1/3/10 16:30	2.6	1591	4.8	0.4	2.2	1374	4.0	0.3	3.6	1190	6.7	0.4	0.4	0.4	915	0.7	14.0	44	19.6	0.0
1/3/10 17:00	2.8	1567	5.2	0.5	1.7	1359	3.1	0.2	2.4	1184	4.4	0.3	0.5	0.5	921	0.9	16.0	44	22.6	0.1
1/3/10 17:30	3.4	1579	6.3	0.6	1.7	1363	3.1	0.2	2.2	1182	4.0	0.3	1.0	0.909	1.8	0.1	21.0	44	30.2	0.1
1/3/10 18:00	2.9	1530	5.4	0.5	2.0	1324	3.7	0.3	2.0	1151	3.7	0.2	0.5	0.91	0.7	0.0	21.0	43	30.2	0.1
1/3/10 18:30	2.8	1506	5.2	0.4	1.5	1308	2.7	0.2	2.1	1141	3.9	0.2	0.4	0.891	0.7	0.0	29.0	43	42.5	0.1
1/3/10 19:00	2.8	1530	5.2	0.4	2.6	1320	4.8	0.4	2.0	1144	3.7	0.2	0.5	0.879	0.9	0.0	36.0	42	53.5	0.1
1/3/10 19:30	2.7	1506	5.0	0.4	1.7	1302	3.1	0.2	1.9	1131	3.5	0.2	0.5	0.873	0.9	0.0	28.0	42	40.9	0.1
1/3/10 20:00	2.8	1506	5.2	0.4	1.8	1302	3.3	0.2	2.1	1131	3.9	0.2	0.4	0.873	0.7	0.0	29.0	42	42.5	0.1
1/3/10 20:30	2.6	1470	4.8	0.4	1.7	1278	3.1	0.2	2.5	1116	4.6	0.3	0.5	0.873	0.9	0.0	29.0	42	42.5	0.1
1/3/10 21:00	2.7	1494	5.0	0.4	1.8	1287	3.3	0.2	2.7	1112	5.0	0.3	0.6	0.850	1.1	0.1	19.0	41	27.1	0.1
1/3/10 21:30	2.7	1458	5.0	0.4	2.0	1259	3.7	0.3	2.8	1090	5.2	0.3	0.5	0.838	0.7	0.0	18.0	40	25.6	0.1
1/3/10 22:00	2.8	1447	5.2	0.4	2.0	1254	3.7	0.3	2.7	1093	5.0	0.3	0.5	0.850	0.9	0.0	15.0	41	21.1	0.0
1/3/10 22:30	3.2	1435	5.9	0.5	1.9	1241	3.5	0.2	2.6	1078	4.8	0.3	0.5	0.832	0.9	0.0	14.0	40	19.6	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/3/10 23:00	4.4	1412	8.2	0.7	1.9	1225	3.5	0.2	2.3	1068	4.2	0.3	0.4	832	0.7	0.0	12.0	40	16.6	0.0
1/3/10 23:30	3.4	1412	6.3	0.5	1.8	1224	3.3	0.2	2.2	1065	4.0	0.2	0.4	827	0.7	0.0	17.0	40	24.1	0.1
1/4/10 0:00	2.3	1412	4.2	0.3	1.5	1220	2.7	0.2	2.1	1058	3.9	0.2	0.5	815	0.9	0.0	12.0	39	16.6	0.0
1/4/10 0:30	2.9	1378	5.4	0.4	1.6	1195	2.9	0.2	2.0	1041	3.7	0.2	0.5	810	0.9	0.0	16.0	39	22.6	0.0
1/4/10 1:00	3.1	1412	5.7	0.5	1.5	1214	2.7	0.2	2.0	1048	3.7	0.2	2.9	798	5.4	0.2	48.0	39	72.6	0.2
1/4/10 1:30	2.7	1401	5.0	0.4	1.9	1209	3.5	0.2	2.3	1047	4.2	0.2	0.5	804	0.9	0.0	45.0	39	67.8	0.1
1/4/10 2:00	3.5	1345	6.5	0.5	1.3	1171	2.4	0.2	2.1	1024	3.9	0.2	0.4	804	0.7	0.0	21.0	39	30.2	0.1
1/4/10 2:30	2.9	1367	5.4	0.4	1.4	1179	2.6	0.2	2.4	1020	4.4	0.3	0.6	782	1.1	0.0	15.0	38	21.1	0.0
1/4/10 3:00	3.0	1345	5.6	0.4	1.7	1165	3.1	0.2	1.9	1014	3.5	0.2	0.4	787	0.7	0.0	12.0	38	16.6	0.0
1/4/10 3:30	2.5	1345	4.6	0.3	1.7	1163	3.1	0.2	1.9	1011	3.5	0.2	0.5	782	0.9	0.0	13.0	38	18.1	0.0
1/4/10 4:00	2.5	1312	4.6	0.3	1.4	1139	2.6	0.2	2.0	994	3.7	0.2	0.4	776	0.7	0.0	11.0	38	15.2	0.0
1/4/10 4:30	3.7	1334	6.9	0.5	1.8	1154	3.3	0.2	1.9	1003	3.5	0.2	0.4	776	0.7	0.0	14.0	38	19.6	0.0
1/4/10 5:00	2.1	1290	3.9	0.3	1.0	1125	1.8	0.1	1.9	985	3.5	0.2	0.4	776	0.7	0.0	25.0	38	36.3	0.1
1/4/10 5:30	2.6	1301	4.8	0.4	1.6	1127	2.9	0.2	2.0	980	3.7	0.2	0.6	760	1.1	0.0	12.0	37	16.6	0.0
1/4/10 6:00	2.2	1290	4.0	0.3	1.7	1118	3.1	0.2	1.8	972	3.3	0.2	0.5	754	0.9	0.0	19.0	37	27.1	0.1
1/4/10 6:30	2.7	1301	5.0	0.4	0.9	1125	1.6	0.1	2.3	977	4.2	0.2	0.4	754	0.7	0.0	14.0	37	19.6	0.0
1/4/10 7:00	2.0	1280	3.7	0.3	1.0	1112	1.8	0.1	2.3	971	4.2	0.2	0.4	760	0.7	0.0	11.0	37	15.2	0.0
1/4/10 7:30	2.2	1269	4.0	0.3	1.3	1100	2.4	0.1	2.0	957	3.7	0.2	0.4	744	0.7	0.0	11.0	36	15.2	0.0
1/4/10 8:00	2.7	1290	5.0	0.4	1.4	1114	2.6	0.2	1.6	966	2.9	0.2	0.5	744	0.9	0.0	18.0	36	25.6	0.1
1/4/10 8:30	2.6	1269	4.8	0.3	1.1	1098	2.0	0.1	1.7	954	3.1	0.2	0.4	738	0.7	0.0	21.0	36	30.2	0.1
1/4/10 9:00	2.7	1227	5.0	0.3	1.2	1064	2.2	0.1	1.6	928	2.9	0.2	0.5	722	0.9	0.0	19.0	35	27.1	0.1
1/4/10 9:30	4.8	1248	9.0	0.6	1.1	1082	2.0	0.1	1.6	942	2.9	0.2	0.4	733	0.7	0.0	21.0	36	30.2	0.1
1/4/10 10:00	2.0	1269	3.7	0.3	1.3	1098	2.4	0.1	1.9	954	3.5	0.2	0.4	738	0.7	0.0	46.0	36	69.4	0.1
1/4/10 10:30	2.1	1237	3.9	0.3	0.7	1073	1.3	0.1	2.2	935	4.0	0.2	0.5	728	0.9	0.0	48.0	35	72.6	0.1
1/4/10 11:00	1.9	1237	3.5	0.2	0.9	1073	1.6	0.1	2.0	935	3.7	0.2	0.5	728	0.9	0.0	35.0	35	51.9	0.1
1/4/10 11:30	2.3	1206	4.2	0.3	1.4	1052	2.6	0.2	2.2	922	4.0	0.2	0.6	728	1.1	0.0	37.0	35	55.0	0.1
1/4/10 12:00	2.6	1216	4.8	0.3	1.7	1059	3.1	0.2	2.4	926	4.4	0.2	0.5	728	0.9	0.0	52.0	35	79.0	0.2
1/4/10 12:30	2.3	1206	4.2	0.3	1.2	1054	2.2	0.1	3.5	925	6.5	0.3	0.4	733	0.7	0.0	29.0	36	42.5	0.1
1/4/10 13:00	2.2	1185	4.0	0.3	1.3	1038	2.4	0.1	2.8	914	5.2	0.3	0.5	728	0.9	0.0	43.0	35	64.6	0.1
1/4/10 13:30	2.2	1216	4.0	0.3	2.2	1062	4.0	0.2	2.5	933	4.6	0.2	0.5	738	0.9	0.0	23.0	36	33.2	0.1
1/4/10 14:00	2.3	1227	4.2	0.3	2.4	1071	4.4	0.3	2.8	940	5.2	0.3	0.6	744	1.1	0.0	40.0	36	59.8	0.1
1/4/10 14:30	2.0	1227	3.7	0.3	2.2	1075	4.0	0.2	2.8	947	5.2	0.3	0.5	754	0.9	0.0	340.0	37	580.4	1.2
1/4/10 15:00	2.4	1248	4.4	0.3	1.8	1096	3.3	0.2	2.4	968	4.4	0.2	0.6	776	1.1	0.0	340.0	38	580.4	1.2
1/4/10 15:30	2.5	1248	4.6	0.3	2.3	1105	4.2	0.3	2.8	985	5.2	0.3	0.5	804	0.9	0.0	330.0	39	562.3	1.2
1/4/10 16:00	2.2	1258	4.0	0.3	2.1	1121	3.9	0.2	4.1	1006	7.6	0.4	0.4	832	0.7	0.0	210.0	40	347.9	0.8
1/4/10 16:30	2.5	1280	4.6	0.3	1.9	1149	3.5	0.2	9.3	1038	17.6	1.0	0.6	873	1.1	0.1	380.0	42	653.2	1.5
1/4/10 17:00	2.8	1301	5.2	0.4	3.4	1177	6.3	0.4	14.7	1072	28.1	1.7	0.6	915	1.1	0.1	200.0	44	330.4	0.8
1/4/10 17:30	3.2	1323	5.9	0.4	6.3	1207	11.8	0.8	17.3	1110	33.2	2.1	0.4	964	0.7	0.0	310.0	46	526.2	1.4
1/4/10 18:00	3.4	1356	6.3	0.5	11.5	1244	21.9	1.5	13.8	1150	26.3	1.7	0.6	1009	1.1	0.1	220.0	48	365.6	1.0
1/4/10 18:30	3.4	1378	6.3	0.5	13.0	1276	24.8	1.8	15.6	1190	29.8	2.0	0.5	1061	0.9	0.1	180.0	50	295.4	0.8
1/4/10 19:00	4.1	1389	7.6	0.6	10.9	1299	20.7	1.5	11.9	1223	22.6	1.6	0.8	1108	1.4	0.1	130.0	53	209.1	0.6
1/4/10 19:30	3.3	1470	6.1	0.5	11.7	1363	22.2	1.7	17.3	1272	33.2	2.4	0.6	1136	1.1	0.1	61.0	54	93.6	0.3

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/4/10 20:00	3.3	1518	6.1	0.5	10.0	1408	19.0	1.5	11.5	1316	21.9	1.6	0.7	1178	1.3	0.1	60.0	56	92.0	0.3
1/4/10 20:30	4.0	1567	7.4	0.7	12.4	1460	23.6	1.9	10.4	1370	19.7	1.5	0.6	1235	1.1	0.1	200.0	58	330.4	1.1
1/4/10 21:00	7.1	1579	13.4	1.2	9.7	1482	18.4	1.5	27.3	1401	52.8	4.2	1.2	1279	2.2	0.2	56.0	60	85.5	0.3
1/4/10 21:30	9.6	1629	18.2	1.7	9.2	1536	17.4	1.5	4.3	1457	8.0	0.7	0.7	1339	1.3	0.1	58.0	63	88.7	0.3
1/4/10 22:00	11.0	1667	20.9	2.0	5.6	1582	10.5	0.9	7.6	1509	14.3	1.2	0.7	1401	1.3	0.1	300.0	66	508.2	1.9
1/4/10 22:30	11.0	1744	20.9	2.0	4.2	1662	7.8	0.7	6.1	1593	11.4	1.0	0.7	1489	1.3	0.1	130.0	69	209.1	0.8
1/4/10 23:00	10.0	1783	19.0	1.9	6.2	1712	11.6	1.1	5.5	1653	10.3	1.0	0.9	1564	1.6	0.1	180.0	73	295.4	1.2
1/4/10 23:30	11.0	1876	20.9	2.2	5.0	1800	9.3	0.9	11.1	1736	21.1	2.1	0.8	1640	1.4	0.1	680.0	76	1211.9	5.2
1/5/10 00:00	11.0	1957	20.9	2.3	6.8	1892	12.8	1.4	12.1	1837	23.0	2.4	0.7	1754	1.3	0.1	250.0	81	418.7	1.9
1/5/10 00:30	8.8	2055	16.6	1.9	13.1	1997	25.0	2.8	12.5	1947	23.8	2.6	0.8	1873	1.4	0.2	300.0	86	508.2	2.5
1/5/10 1:00	7.2	2195	13.6	1.7	10.9	2134	20.7	2.5	23.8	2083	45.9	5.4	1.1	2007	2.0	0.2	150.0	92	243.4	1.3
1/5/10 1:30	6.4	2220	12.0	1.5	18.0	2200	34.5	4.3	15.9	2182	30.4	3.7	0.9	2156	1.6	0.2	310.0	98	526.2	2.9
1/5/10 2:00	8.2	2376	15.5	2.1	17.3	2335	33.2	4.4	14.5	2301	27.7	3.6	1.6	2249	2.9	0.4	110.0	102	175.1	1.0
1/5/10 2:30	8.3	2470	15.7	2.2	14.5	2443	27.7	3.8	12.1	2420	23.0	3.1	2.2	2387	4.0	0.5	150.0	108	243.4	1.5
1/5/10 3:00	11.0	2607	20.9	3.1	13.0	2564	24.8	3.6	10.9	2528	20.7	2.9	1.9	2474	3.5	0.5	160.0	112	260.7	1.6
1/5/10 3:30	13.0	2865	24.8	4.0	13.4	2757	25.5	4.0	9.4	2666	17.8	2.7	2.0	2529	3.7	0.5	110.0	114	175.1	1.1
1/5/10 4:00	16.0	3022	30.6	5.2	11.7	2875	22.2	3.6	10.9	2750	20.7	3.2	1.2	2563	2.2	0.3	130.0	116	209.1	1.4
1/5/10 4:30	18.0	3022	34.5	5.9	12.3	2878	23.4	3.8	17.4	2757	33.3	5.2	1.6	2574	2.9	0.4	100.0	116	158.2	1.0
1/5/10 5:00	17.0	3184	32.6	5.8	12.0	3013	22.8	3.9	9.6	2870	18.2	2.9	2.0	2654	3.7	0.5	180.0	120	295.4	2.0
1/5/10 5:30	15.0	3349	28.7	5.4	13.2	3144	25.2	4.4	11.8	2971	22.4	3.7	1.8	2712	3.3	0.5	120.0	122	192.0	1.3
1/5/10 6:00	14.0	3228	26.7	4.8	11.1	3081	21.1	3.7	10.2	2957	19.3	3.2	1.8	2771	3.3	0.5	260.0	125	436.5	3.1
1/5/10 6:30	15.0	3303	28.7	5.3	12.7	3155	24.2	4.3	15.4	3030	29.4	5.0	1.7	2842	3.1	0.5	110.0	128	175.1	1.3
1/5/10 7:00	14.0	3288	26.7	4.9	15.1	3176	28.9	5.2	13.5	3081	25.7	4.5	1.9	2939	3.5	0.6	160.0	132	260.7	1.9
1/5/10 7:30	14.0	3567	26.7	5.4	15.9	3388	30.4	5.8	10.5	3238	19.9	3.6	2.2	3013	4.0	0.7	94.0	135	148.2	1.1
1/5/10 8:00	16.0	3488	30.6	6.0	15.4	3363	29.4	5.6	14.6	3258	27.9	5.1	2.1	3101	3.9	0.7	81.0	138	126.5	1.0
1/5/10 8:30	14.0	3614	26.7	5.4	18.2	3498	34.9	6.9	15.6	3401	29.8	5.7	3.3	3255	6.1	1.1	110.0	145	175.1	1.4
1/5/10 9:00	16.0	3745	30.6	6.4	18.5	3612	35.5	7.2	12.1	3501	23.0	4.5	3.0	3333	5.6	1.0	140.0	148	226.2	1.9
1/5/10 9:30	19.0	3963	36.5	8.1	20.0	3786	38.4	8.2	14.8	3637	28.3	5.8	3.3	3413	6.1	1.2	97.0	152	153.2	1.3
1/5/10 10:00	20.0	3929	38.4	8.5	20.4	3771	39.2	8.3	15.9	3639	30.4	6.2	3.0	3440	5.6	1.1	130.0	153	209.1	1.8
1/5/10 10:30	17.0	4152	32.6	7.6	22.8	3949	43.9	9.8	14.3	3778	27.3	5.8	4.1	3521	7.6	1.5	79.0	156	123.2	1.1
1/5/10 11:00	28.0	4329	54.2	13.2	24.6	4069	47.5	10.9	30.2	3850	58.5	12.7	4.2	3521	7.8	1.5	110.0	156	175.1	1.5
1/5/10 11:30	25.0	4347	48.3	11.8	22.4	4085	43.1	9.9	14.9	3865	28.5	6.2	4.3	3535	8.0	1.6	82.0	157	128.2	1.1
1/5/10 12:00	27.0	4276	52.2	12.5	22.0	4037	42.4	9.6	13.6	3836	25.9	5.6	3.3	3535	6.1	1.2	66.0	157	101.8	0.9
1/5/10 12:30	29.0	4383	56.1	13.8	22.5	4088	43.3	10.0	12.5	3840	23.8	5.1	3.5	3467	6.5	1.3	70.0	154	108.3	0.9
1/5/10 13:00	31.0	3878	60.1	13.1	20.5	3728	39.4	8.3	11.8	3602	22.4	4.5	2.8	3413	5.2	1.0	78.0	152	121.5	1.0
1/5/10 13:30	30.0	4152	58.1	13.6	19.1	3910	36.7	8.1	11.3	3706	21.5	4.5	3.0	3400	5.6	1.1	90.0	151	141.5	1.2
1/5/10 14:00	31.0	4565	60.1	15.4	15.0	4181	28.7	6.7	10.0	3858	19.0	4.1	3.2	3373	5.9	1.1	79.0	150	123.2	1.0
1/5/10 14:30	29.0	4383	56.1	13.8	16.7	4053	32.0	7.3	10.4	3776	19.7	4.2	3.5	3360	6.5	1.2	54.0	149	82.2	0.7
1/5/10 15:00	27.0	4117	52.2	12.1	16.2	3869	31.0	6.7	10.5	3660	19.9	4.1	3.0	3347	5.6	1.0	120.0	149	192.0	1.6
1/5/10 15:30	26.0	4152	50.2	11.7	14.3	3889	27.3	6.0	8.5	3667	16.1	3.3	2.5	3333	4.6	0.9	130.0	148	209.1	1.7
1/5/10 16:00	23.0	4240	44.3	10.6	16.7	3940	32.0	7.1	9.6	3687	18.2	3.8	2.3	3307	4.2	0.8	110.0	147	175.1	1.4
1/5/10 16:30	23.0	4205	44.3	10.5	15.2	3907	29.1	6.4	11.9	3657	22.6	4.7	2.5	3281	4.6	0.8	95.0	146	149.8	1.2

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/5/10 17:00	24.0	4276	46.3	11.1	18.5	3981	35.5	7.9	10.7	3732	20.3	4.3	2.6	3360	4.8	0.9	55.0	149	83.9	0.7
1/5/10 17:30	24.0	4311	46.3	11.2	17.6	3984	33.7	7.6	11.3	3708	21.5	4.5	2.6	3294	4.8	0.9	150.0	147	243.4	2.0
1/5/10 18:00	22.0	4311	42.4	10.3	16.1	3996	30.8	6.9	8.2	3731	15.5	3.2	2.4	3333	4.4	0.8	74.0	148	114.9	1.0
1/5/10 18:30	20.0	4311	38.4	9.3	29.9	3992	57.9	13.0	11.0	3723	20.9	4.4	2.4	3320	4.4	0.8	55.0	148	83.9	0.7
1/5/10 19:00	24.0	4135	46.3	10.8	15.8	3864	30.2	6.6	8.3	3636	15.7	3.2	2.7	3294	5.0	0.9	60.0	147	92.0	0.8
1/5/10 19:30	22.0	4117	42.4	9.8	17.8	3844	34.1	7.4	10.9	3613	20.7	4.2	2.9	3268	5.4	1.0	73.0	146	113.3	0.9
1/5/10 20:00	22.0	4223	42.4	10.1	18.5	3915	35.5	7.8	9.6	3656	18.2	3.7	3.6	3268	6.7	1.2	180.0	146	295.4	2.4
1/5/10 20:30	27.0	4311	52.2	12.6	13.4	3959	25.5	5.7	8.3	3661	15.7	3.2	2.4	3216	4.4	0.8	81.0	143	126.5	1.0
1/5/10 21:00	24.0	4205	46.3	10.9	13.6	3878	25.9	5.7	11.8	3603	22.4	4.5	2.5	3190	4.6	0.8	110.0	142	175.1	1.4
1/5/10 21:30	21.0	4187	40.4	9.5	14.8	3850	28.3	6.1	9.9	3565	18.8	3.8	2.4	3139	4.4	0.8	98.0	140	154.9	1.2
1/5/10 22:00	23.0	4240	44.3	10.6	14.0	3877	26.7	5.8	10.9	3572	20.7	4.2	2.3	3114	4.2	0.7	110.0	139	175.1	1.4
1/5/10 22:30	19.0	4170	36.5	8.5	12.3	3817	23.4	5.0	8.5	3521	16.1	3.2	2.6	3076	4.8	0.8	100.0	137	158.2	1.2
1/5/10 23:00	20.0	4329	38.4	9.4	14.2	3921	27.1	6.0	8.9	3578	16.8	3.4	2.1	3063	3.9	0.7	84.0	137	131.5	1.0
1/5/10 23:30	19.0	3929	36.5	8.1	12.8	3646	24.4	5.0	8.8	3408	16.6	3.2	2.1	3051	3.9	0.7	96.0	136	151.5	1.2
1/6/10 0:00	22.0	4205	42.4	10.0	14.4	3825	27.5	5.9	8.7	3505	16.4	3.2	2.1	3026	3.9	0.7	89.0	135	139.8	1.1
1/6/10 0:30	18.0	4100	34.5	8.0	15.0	3746	28.7	6.0	8.8	3448	16.6	3.2	2.1	3001	3.9	0.7	140.0	134	226.2	1.7
1/6/10 1:00	18.0	4031	34.5	7.8	13.4	3683	25.5	5.3	8.3	3391	15.7	3.0	2.3	2951	4.2	0.7	120.0	132	192.0	1.4
1/6/10 1:30	20.0	4152	38.4	9.0	12.6	3766	24.0	5.1	9.6	3440	18.2	3.5	2.1	2951	3.9	0.6	160.0	132	260.7	1.9
1/6/10 2:00	19.0	4240	46.3	11.0	16.7	3825	32.0	6.9	11.3	3476	21.5	4.2	2.1	2964	3.5	0.6	160.0	132	260.7	1.9
1/6/10 2:30	24.0	4205	36.5	8.6	14.7	3805	28.1	6.0	10.4	3469	19.7	3.8	1.9	2964	3.5	0.6	110.0	133	175.1	1.3
1/6/10 3:00	20.0	4117	38.4	8.9	16.6	3758	31.8	6.7	9.7	3455	18.4	3.6	2.1	3001	3.9	0.7	110.0	134	175.1	1.3
1/6/10 3:30	19.0	4419	36.5	9.1	17.5	3958	33.5	7.5	8.7	3570	16.4	3.3	2.1	2988	3.9	0.6	280.0	134	472.3	3.6
1/6/10 4:00	30.0	4293	58.1	14.0	16.7	3885	32.0	7.0	9.1	3541	17.2	3.4	1.9	3026	3.5	0.6	120.0	135	192.0	1.5
1/6/10 4:30	21.0	4240	40.4	9.6	15.3	3841	29.2	6.3	12.4	3505	23.6	4.6	1.8	3001	3.3	0.6	69.0	134	106.7	0.8
1/6/10 5:00	22.0	4258	42.4	10.1	17.8	3861	34.1	7.4	9.6	3527	18.2	3.6	1.8	3026	3.3	0.6	630.0	135	1117.5	8.5
1/6/10 5:30	22.0	4365	42.4	10.4	15.9	3926	30.4	6.7	8.0	3556	15.1	3.0	1.9	3001	3.5	0.6	190.0	134	312.9	2.4
1/6/10 6:00	21.0	4492	40.4	10.2	13.9	3996	26.5	6.0	13.6	3578	25.9	5.2	2.0	2951	3.7	0.6	110.0	132	175.1	1.3
1/6/10 6:30	21.0	4100	40.4	9.3	14.2	3734	27.1	5.7	12.7	3426	24.2	4.7	2.9	2964	5.4	0.9	78.0	133	121.5	0.9
1/6/10 7:00	22.0	4152	42.4	9.9	19.1	3754	36.7	7.7	9.0	3418	17.0	3.3	1.8	2915	3.3	0.5	72.0	131	111.6	0.8
1/6/10 7:30	20.0	4031	38.4	8.7	14.4	3660	27.5	5.7	9.7	3347	18.4	3.5	1.7	2878	3.1	0.5	58.0	129	88.7	0.6
1/6/10 8:00	18.0	4083	34.5	7.9	12.3	3679	23.4	4.8	10.7	3340	20.3	3.8	1.9	2830	3.5	0.6	47.0	127	71.0	0.5
1/6/10 8:30	21.0	4100	40.4	9.3	12.7	3683	24.2	5.0	7.5	3333	14.1	2.6	1.7	2806	3.1	0.5	44.0	126	66.2	0.5
1/6/10 9:00	21.0	4293	40.4	9.7	10.4	3792	19.7	4.2	6.7	3369	12.6	2.4	3.3	2736	6.1	0.9	49.0	123	74.2	0.5
1/6/10 9:30	20.0	4083	38.4	8.8	10.5	3630	19.9	4.1	6.4	3249	12.0	2.2	1.6	2677	2.9	0.4	39.0	121	58.2	0.4
1/6/10 10:00	22.0	4170	42.4	9.9	10.0	3678	19.0	3.9	6.7	3264	12.6	2.3	1.4	2643	2.6	0.4	49.0	119	74.2	0.5
1/6/10 10:30	16.0	4065	30.6	7.0	9.5	3593	18.0	3.6	5.8	3194	10.9	2.0	1.9	2597	3.5	0.5	45.0	117	67.8	0.4
1/6/10 11:00	15.0	4135	28.7	6.7	10.0	3636	19.0	3.9	6.6	3216	12.4	2.2	1.7	2586	3.1	0.5	46.0	117	69.4	0.5
1/6/10 11:30	14.0	4100	26.7	6.2	9.7	3587	18.4	3.7	6.5	3155	12.2	2.2	1.7	2507	3.1	0.4	37.0	113	55.0	0.4
1/6/10 12:00	14.0	3895	26.7	5.8	8.5	3437	16.1	3.1	6.3	3052	11.8	2.0	1.6	2474	2.9	0.4	36.0	112	53.5	0.3
1/6/10 12:30	13.0	3567	24.8	5.0	8.6	3190	16.3	2.9	5.8	2873	10.9	1.8	1.4	2397	2.6	0.3	31.0	109	45.6	0.3
1/6/10 13:00	12.0	3811	22.8	4.9	8.0	3345	15.1	2.8	5.2	2953	9.7	1.6	1.4	2365	2.6	0.3	34.0	107	50.3	0.3
1/6/10 13:30	13.0	3811	24.8	5.3	8.4	3325	15.9	3.0	5.2	2915	9.7	1.6	2.4	2301	4.4	0.6	30.0	105	44.0	0.3

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/6/10 14:00	13.0	3488	24.8	4.9	8.8	3092	16.6	2.9	4.6	2759	8.6	1.3	1.2	2259	2.2	0.3	32.0	103	47.2	0.3
1/6/10 14:30	12.0	3551	22.8	4.6	7.5	3121	14.1	2.8	4.7	2760	8.8	1.4	1.4	2218	2.6	0.3	32.0	101	47.2	0.3
1/6/10 15:00	11.0	3567	20.9	4.2	8.4	3116	15.9	2.5	4.8	2736	9.0	1.4	1.2	2166	2.2	0.3	53.0	99	80.6	0.4
1/6/10 15:30	11.5	3441	21.9	4.2	6.9	3024	13.0	2.2	5.1	2673	9.5	1.4	1.6	2146	2.9	0.4	38.0	98	56.6	0.3
1/6/10 16:00	10.0	3303	19.0	3.5	7.7	2911	14.5	2.4	4.9	2581	9.2	1.3	1.2	2086	2.2	0.3	36.0	95	53.5	0.3
1/6/10 16:30	9.8	3410	18.6	3.6	6.4	2965	12.0	2.0	4.9	2589	9.2	1.3	1.2	2026	2.2	0.2	30.0	93	44.0	0.2
1/6/10 17:00	9.8	3395	18.6	3.5	6.2	2951	11.6	1.9	4.5	2577	8.4	1.2	1.3	2017	2.4	0.3	46.0	92	69.4	0.4
1/6/10 17:30	10.0	3243	19.0	3.5	6.5	2833	12.2	1.9	4.8	2487	9.0	1.3	1.4	1968	2.6	0.3	420.0	90	726.5	3.7
1/6/10 18:00	9.0	3243	17.0	3.1	6.5	2826	12.2	1.9	4.3	2475	8.0	1.1	1.1	1949	2.0	0.2	180.0	89	295.4	1.5
1/6/10 18:30	9.6	3080	18.2	3.1	6.8	2695	12.8	1.9	5.1	2370	9.5	1.3	1.3	1883	2.4	0.3	110.0	87	175.1	0.9
1/6/10 19:00	9.6	3169	18.2	3.2	5.6	2749	10.5	1.6	14.8	2395	28.3	3.8	1.1	1864	2.0	0.2	57.0	86	87.1	0.4
1/6/10 19:30	9.0	3198	17.0	3.1	11.4	2757	21.7	3.4	8.2	2385	15.5	2.1	1.1	1827	2.0	0.2	62.0	84	95.2	0.5
1/6/10 20:00	9.1	3169	17.2	3.1	11.3	2737	21.5	3.3	6.4	2373	12.0	1.6	0.8	1827	1.4	0.1	46.0	84	69.4	0.3
1/6/10 20:30	9.3	3154	17.6	3.1	8.3	2715	15.7	2.4	4.7	2345	8.8	1.2	1.3	1791	2.4	0.2	88.0	83	138.1	0.6
1/6/10 21:00	7.5	3037	14.1	2.4	6.5	2618	12.2	1.8	4.8	2265	9.0	1.1	1.1	1737	2.0	0.2	44.0	80	66.2	0.3
1/6/10 21:30	8.5	3008	16.1	2.7	5.5	2593	10.3	1.5	4.3	2243	8.0	1.0	1.4	1719	2.6	0.2	43.0	79	64.6	0.3
1/6/10 22:00	11.0	2880	20.9	3.4	6.6	2495	12.4	1.7	4.6	2170	8.6	1.0	1.4	1683	2.6	0.2	82.0	78	128.2	0.6
1/6/10 22:30	12.0	2922	22.8	3.7	5.6	2518	10.5	1.5	7.2	2177	13.6	1.7	0.9	1666	1.6	0.2	110.0	77	175.1	0.8
1/6/10 23:00	9.5	2922	18.0	3.0	5.5	2509	10.3	1.5	4.6	2162	8.6	1.0	0.9	1640	1.6	0.1	64.0	76	98.5	0.4
1/6/10 23:30	8.3	2979	15.7	2.6	5.1	2542	9.5	1.4	5.5	2175	10.3	1.3	1.4	1623	2.6	0.2	53.0	75	80.6	0.3
1/7/10 00:00	7.1	2880	13.4	2.2	5.9	2459	11.1	1.5	5.6	2104	10.5	1.2	0.8	1572	1.4	0.1	35.0	73	51.9	0.2
1/7/10 0:30	7.0	2763	13.2	2.0	5.6	2374	10.5	1.4	4.6	2047	8.6	1.0	0.8	1555	1.4	0.1	33.0	72	48.7	0.2
1/7/10 1:00	7.5	2663	14.1	2.1	6.0	2301	11.3	1.5	4.5	1996	8.4	0.9	0.8	1539	1.4	0.1	31.0	72	45.6	0.2
1/7/10 1:30	7.3	2678	13.7	2.1	5.6	2298	10.5	1.4	4.8	1977	9.0	1.0	1.0	1497	1.8	0.1	26.0	70	37.8	0.1
1/7/10 2:00	7.0	2663	13.2	2.0	5.4	2280	10.1	1.3	4.1	1957	7.6	0.8	0.9	1473	1.6	0.1	29.0	69	42.5	0.2
1/7/10 2:30	6.9	2607	13.0	1.9	4.2	2239	7.8	1.0	4.4	1930	8.2	0.9	0.8	1465	1.4	0.1	27.0	68	39.4	0.2
1/7/10 3:00	8.1	2649	15.3	2.3	4.3	2260	8.0	1.0	3.1	1932	5.7	0.6	1.3	1441	2.4	0.2	25.0	67	36.3	0.1
1/7/10 3:30	7.5	2621	14.1	2.1	4.5	2236	8.4	1.1	3.7	1912	6.9	0.7	1.0	1425	1.8	0.1	22.0	67	31.7	0.1
1/7/10 4:00	9.8	2566	18.6	2.7	3.3	2193	6.1	0.8	3.7	1880	6.9	0.7	1.0	1409	1.8	0.1	20.0	66	28.6	0.1
1/7/10 4:30	7.3	2607	13.7	2.0	4.1	2206	7.6	0.9	3.1	1869	5.7	0.6	0.8	1362	1.4	0.1	19.0	64	27.1	0.1
1/7/10 5:00	6.4	2579	12.0	1.7	3.7	2185	6.9	0.8	3.3	1853	6.1	0.6	0.6	1355	1.1	0.1	19.0	64	27.1	0.1
1/7/10 5:30	6.1	2470	11.4	1.6	4.7	2106	8.8	1.0	3.2	1799	5.9	0.6	0.8	1339	1.4	0.1	29.0	63	42.5	0.2
1/7/10 6:00	5.9	2429	11.1	1.5	3.7	2076	6.9	0.8	3.1	1778	5.7	0.6	0.7	1332	1.3	0.1	24.0	63	34.8	0.1
1/7/10 6:30	5.8	2389	10.9	1.5	3.5	2039	6.5	0.7	3.5	1744	6.5	0.6	0.6	1302	1.1	0.1	22.0	61	31.7	0.1
1/7/10 7:00	6.3	2443	11.8	1.6	3.3	2073	6.1	0.7	2.9	1761	5.4	0.5	0.7	1294	1.3	0.1	22.0	61	31.7	0.1
1/7/10 7:30	5.1	2456	9.5	1.3	2.9	2075	5.4	0.6	3.4	1754	6.3	0.6	0.7	1272	1.3	0.1	30.0	60	44.0	0.1
1/7/10 8:00	4.9	2403	9.2	1.2	2.9	2036	5.4	0.6	2.4	1727	4.4	0.4	0.8	1264	1.4	0.1	22.0	60	31.7	0.1
1/7/10 8:30	5.2	2470	9.7	1.4	4.3	2075	8.0	0.9	2.7	1742	5.0	0.5	0.7	1242	1.3	0.1	24.0	59	34.8	0.1
1/7/10 9:00	4.8	2298	9.0	1.2	3.4	1953	6.3	0.7	2.8	1663	5.2	0.5	0.7	1228	1.3	0.1	24.0	58	34.8	0.1
1/7/10 9:30	5.3	2337	9.9	1.3	3.5	1973	6.5	0.7	2.5	1666	4.6	0.4	1.0	1206	1.8	0.1	19.0	57	27.1	0.1
1/7/10 10:00	4.9	2403	9.2	1.2	3.3	2013	6.1	0.7	3.0	1684	5.6	0.5	0.7	1192	1.3	0.1	33.0	56	48.7	0.2
1/7/10 10:30	4.7	2208	8.8	1.1	3.9	1878	7.3	0.8	3.0	1601	5.6	0.5	0.6	1185	1.1	0.1	22.0	56	31.7	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/7/10 11:00	4.5	2246	8.4	1.1	2.8	1893	5.2	0.6	2.5	1596	4.6	0.4	0.7	1150	1.3	0.1	23.0	54	33.2	0.1
1/7/10 11:30	4.6	2220	8.6	1.1	3.7	1876	6.9	0.7	2.5	1585	4.6	0.4	0.7	1150	1.3	0.1	28.0	54	40.9	0.1
1/7/10 12:00	4.8	2169	9.0	1.1	3.4	1834	6.3	0.7	2.5	1552	4.6	0.4	0.7	1129	1.3	0.1	29.0	54	42.5	0.1
1/7/10 12:30	6.3	2285	11.8	1.5	3.2	1910	5.9	0.6	2.5	1595	4.6	0.4	0.7	1122	1.3	0.1	21.0	53	30.2	0.1
1/7/10 13:00	4.7	2182	8.8	1.1	2.8	1839	5.2	0.5	3.1	1549	5.7	0.5	0.5	1115	0.9	0.1	17.0	53	24.1	0.1
1/7/10 13:30	4.6	2131	8.6	1.0	2.6	1797	4.8	0.5	2.5	1516	4.6	0.4	0.9	1095	1.6	0.1	42.0	52	63.0	0.2
1/7/10 14:00	4.2	2080	7.8	0.9	2.9	1759	5.4	0.5	2.5	1488	4.6	0.4	0.7	1081	1.3	0.1	25.0	51	36.3	0.1
1/7/10 14:30	4.0	2080	7.4	0.9	2.6	1756	4.8	0.5	3.1	1484	5.7	0.5	0.7	1075	1.3	0.1	19.0	51	27.1	0.1
1/7/10 15:00	3.9	2080	7.3	0.8	2.3	1750	4.2	0.4	2.6	1472	4.8	0.4	0.7	1055	1.3	0.1	18.0	50	25.6	0.1
1/7/10 15:30	4.6	2043	8.6	1.0	3.4	1723	6.3	0.6	2.8	1453	5.2	0.4	0.7	1048	1.3	0.1	22.0	50	31.7	0.1
1/7/10 16:00	4.6	2031	8.6	1.0	2.9	1710	5.4	0.5	2.2	1440	4.0	0.3	0.5	1035	0.9	0.1	17.0	49	24.1	0.1
1/7/10 16:30	4.0	2031	7.4	0.8	2.8	1706	5.2	0.5	2.3	1432	4.2	0.3	0.6	1022	1.1	0.1	18.0	49	25.6	0.1
1/7/10 17:00	4.2	1945	7.8	0.9	2.9	1644	5.4	0.5	2.0	1390	3.7	0.3	0.6	1009	1.1	0.1	24.0	48	34.8	0.1
1/7/10 17:30	3.9	1969	7.3	0.8	2.3	1658	4.2	0.4	1.9	1396	3.5	0.3	0.6	1003	1.1	0.1	61.0	48	93.6	0.3
1/7/10 18:00	5.5	1994	10.3	1.2	2.4	1670	4.4	0.4	1.9	1398	3.5	0.3	0.7	990	1.3	0.1	58.0	47	88.7	0.2
1/7/10 18:30	6.8	1904	12.8	1.4	2.8	1607	5.2	0.5	2.2	1358	4.0	0.3	0.8	983	1.4	0.1	29.0	47	42.5	0.1
1/7/10 19:00	4.0	1945	7.4	0.8	2.1	1633	3.9	0.4	2.7	1371	5.0	0.4	0.7	977	1.3	0.1	27.0	47	39.4	0.1
1/7/10 19:30	3.9	1904	7.3	0.8	2.5	1603	4.6	0.4	3.3	1350	6.1	0.5	0.6	971	1.1	0.1	23.0	46	33.2	0.1
1/7/10 20:00	3.6	1890	6.7	0.7	3.3	1590	6.1	0.5	3.1	1337	5.7	0.4	0.6	958	1.1	0.1	21.0	46	30.2	0.1
1/7/10 20:30	4.3	1809	8.0	0.8	3.1	1529	5.7	0.5	2.6	1293	4.8	0.3	0.6	940	1.1	0.1	22.0	45	31.7	0.1
1/7/10 21:00	3.7	1849	6.9	0.7	3.1	1556	5.7	0.5	2.4	1310	4.4	0.3	0.6	940	1.1	0.1	21.0	45	30.2	0.1
1/7/10 21:30	3.9	1783	7.3	0.7	2.6	1506	4.8	0.4	2.4	1272	4.4	0.3	0.6	921	1.1	0.1	16.0	44	22.6	0.1
1/7/10 22:00	3.7	1757	6.9	0.7	2.8	1486	5.2	0.4	3.1	1258	5.7	0.4	0.8	915	1.4	0.1	16.0	44	22.6	0.1
1/7/10 22:30	3.8	1809	7.1	0.7	2.6	1519	4.8	0.4	2.5	1275	4.6	0.3	0.6	909	1.1	0.1	15.0	44	21.1	0.1
1/7/10 23:00	4.3	1757	8.0	0.8	2.6	1480	4.8	0.4	1.9	1247	3.5	0.2	0.5	897	0.9	0.0	18.0	43	25.6	0.1
1/7/10 23:30	4.4	1757	8.2	0.8	2.2	1476	4.0	0.3	2.2	1240	4.0	0.3	0.6	885	1.1	0.1	15.0	43	21.1	0.1
1/8/10 0:00	3.9	1693	7.3	0.7	2.5	1431	4.6	0.4	1.7	1210	3.1	0.2	0.7	879	1.3	0.1	16.0	42	22.6	0.1
1/8/10 1:00	3.4	1718	6.3	0.6	2.3	1440	4.2	0.3	2.0	1206	3.7	0.2	0.8	856	1.4	0.1	13.0	41	18.1	0.0
1/8/10 1:30	3.6	1705	6.7	0.6	2.0	1436	3.7	0.3	2.0	1208	3.7	0.2	2.2	867	4.0	0.2	13.0	42	18.1	0.0
1/8/10 2:00	3.5	1680	6.5	0.6	2.8	1413	5.2	0.4	1.8	1187	3.3	0.2	0.5	850	0.9	0.0	11.0	41	15.2	0.0
1/8/10 2:30	3.4	1680	6.3	0.6	1.8	1409	3.3	0.3	1.9	1181	3.5	0.2	0.7	838	1.3	0.1	15.0	40	21.1	0.0
1/8/10 3:00	3.2	1642	5.9	0.5	2.1	1381	3.9	0.3	1.6	1162	2.9	0.2	0.6	832	1.1	0.1	14.0	40	19.6	0.0
1/8/10 3:30	3.2	1642	5.9	0.5	2.6	1377	4.8	0.4	1.6	1155	2.9	0.2	0.7	821	1.3	0.1	13.0	40	18.1	0.0
1/8/10 4:00	3.5	1629	6.5	0.6	1.7	1369	3.1	0.2	1.8	1150	3.3	0.2	0.4	821	0.7	0.0	11.0	40	15.2	0.0
1/8/10 4:30	6.0	1616	11.3	1.0	2.5	1357	4.6	0.4	1.6	1138	2.9	0.2	0.5	810	0.9	0.0	10.0	39	13.7	0.0
1/8/10 5:00	3.5	1616	6.5	0.6	1.7	1353	3.1	0.2	1.7	1131	3.1	0.2	0.5	798	0.9	0.0	12.0	39	16.6	0.0
1/8/10 5:30	3.2	1554	5.9	0.5	1.8	1309	3.3	0.2	2.1	1103	3.9	0.2	1.0	793	1.8	0.1	10.0	38	13.7	0.0
1/8/10 6:00	3.2	1579	5.9	0.5	1.7	1326	3.1	0.2	1.6	1113	2.9	0.2	0.6	793	1.1	0.0	13.0	38	18.1	0.0
1/8/10 6:30	3.1	1567	5.7	0.5	2.4	1314	4.4	0.3	1.6	1101	2.9	0.2	0.4	782	0.7	0.0	17.0	38	24.1	0.1
1/8/10 7:00	3.1	1518	5.7	0.5	2.1	1283	3.9	0.3	2.0	1085	3.7	0.2	0.6	787	1.1	0.0	25.0	38	36.3	0.1
1/8/10 7:30	2.9	1554	5.4	0.5	2.1	1300	3.9	0.3	2.2	1086	4.0	0.2	0.7	765	1.3	0.1	14.0	37	19.6	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/8/10 8:00	3.0	1518	5.6	0.5	1.6	1277	2.9	0.2	1.6	1075	2.9	0.2	0.6	771	1.1	0.0	12.0	37	16.6	0.0
1/8/10 8:30	3.1	1518	5.7	0.5	1.7	1276	3.1	0.2	1.7	1071	3.1	0.2	0.4	765	0.7	0.0	18.0	37	25.6	0.1
1/8/10 9:00	4.2	1494	7.8	0.7	1.4	1256	2.6	0.2	1.9	1055	3.5	0.2	0.5	754	0.9	0.0	22.0	37	31.7	0.1
1/8/10 9:30	2.8	1494	5.2	0.4	1.8	1256	3.3	0.2	1.4	1055	2.6	0.2	0.6	754	1.1	0.0	23.0	37	33.2	0.1
1/8/10 10:00	2.9	1506	5.4	0.5	1.8	1260	3.3	0.2	1.5	1054	2.7	0.2	0.5	744	0.9	0.0	30.0	36	44.0	0.1
1/8/10 10:30	2.7	1482	5.0	0.4	2.0	1241	3.7	0.3	1.4	1038	2.6	0.1	0.5	733	0.9	0.0	41.0	36	61.4	0.1
1/8/10 11:00	3.1	1470	5.7	0.5	1.4	1235	2.6	0.2	1.8	1036	3.3	0.2	0.7	738	1.3	0.1	38.0	36	56.6	0.1
1/8/10 11:30	2.6	1424	4.8	0.4	1.7	1199	3.1	0.2	1.6	1011	2.9	0.2	0.5	728	0.9	0.0	35.0	35	51.9	0.1
1/8/10 12:00	2.6	1447	4.8	0.4	2.1	1213	3.9	0.3	2.2	1017	4.0	0.2	0.6	722	1.1	0.0	17.0	35	24.1	0.0
1/8/10 12:30	3.0	1435	5.6	0.4	2.1	1206	3.9	0.3	2.3	1012	4.2	0.2	0.4	722	0.7	0.0	14.0	35	19.6	0.0
1/8/10 13:00	2.8	1424	5.2	0.4	1.8	1194	3.3	0.2	2.2	1001	4.0	0.2	0.6	712	1.1	0.0	15.0	35	21.1	0.0
1/8/10 13:30	3.6	1424	6.7	0.5	2.1	1193	3.9	0.3	2.8	998	5.2	0.3	0.5	707	0.9	0.0	15.0	34	21.1	0.0
1/8/10 14:00	3.7	1401	6.9	0.5	2.1	1177	3.9	0.3	1.9	989	3.5	0.2	0.4	707	0.7	0.0	13.0	34	18.1	0.0
1/8/10 14:30	2.6	1412	4.8	0.4	2.5	1183	4.6	0.3	1.6	991	2.9	0.2	0.4	702	0.7	0.0	16.0	34	22.6	0.0
1/8/10 15:00	2.5	1378	4.6	0.4	1.9	1155	3.5	0.2	2.0	968	3.7	0.2	0.5	686	0.9	0.0	22.0	33	31.7	0.1
1/8/10 15:30	2.6	1378	4.8	0.4	1.7	1157	3.1	0.2	1.5	971	2.7	0.1	0.6	691	1.1	0.0	20.0	34	28.6	0.1
1/8/10 16:00	2.8	1378	5.2	0.4	1.9	1157	3.5	0.2	1.4	971	2.6	0.1	0.5	691	0.9	0.0	18.0	34	25.6	0.0
1/8/10 16:30	3.1	1378	5.7	0.4	1.5	1157	2.7	0.2	1.5	971	2.7	0.1	0.7	691	1.3	0.0	19.0	34	27.1	0.1
1/8/10 17:00	3.0	1356	5.6	0.4	1.9	1142	3.5	0.2	2.0	962	3.7	0.2	0.4	691	0.7	0.0	260.0	34	436.5	0.8
1/8/10 17:30	3.2	1378	5.9	0.5	2.2	1160	4.0	0.3	2.1	977	3.9	0.2	0.5	702	0.9	0.0	430.0	34	744.9	1.4
1/8/10 18:00	3.5	1378	6.5	0.5	2.1	1159	3.9	0.3	2.0	974	3.7	0.2	0.6	696	1.1	0.0	230.0	34	383.2	0.7
1/8/10 18:30	3.1	1389	5.7	0.4	2.0	1168	3.7	0.2	1.6	981	2.9	0.2	0.5	702	0.9	0.0	160.0	34	260.7	0.5
1/8/10 19:00	3.2	1389	5.9	0.5	1.7	1168	3.1	0.2	4.6	981	8.6	0.5	0.9	702	1.6	0.1	340.0	34	580.4	1.1
1/8/10 19:30	3.1	1367	5.7	0.4	2.2	1154	4.0	0.3	11.8	975	22.4	1.2	0.5	707	0.9	0.0	400.0	34	689.8	1.3
1/8/10 20:00	3.3	1367	6.1	0.5	3.1	1154	5.7	0.4	11.7	975	22.2	1.2	0.5	707	0.9	0.0	170.0	34	278.0	0.5
1/8/10 20:30	2.7	1367	5.0	0.4	7.8	1153	14.7	1.0	8.0	972	15.1	0.8	0.4	702	0.7	0.0	66.0	34	101.8	0.2
1/8/10 21:00	2.9	1345	5.4	0.4	9.5	1138	18.0	1.1	10.0	963	19.0	1.0	0.6	702	1.1	0.0	130.0	34	209.1	0.4
1/8/10 21:30	3.2	1345	5.9	0.4	7.1	1138	13.4	0.9	14.2	963	27.1	1.5	0.4	702	0.7	0.0	48.0	34	72.6	0.1
1/8/10 22:00	2.9	1356	5.4	0.4	7.3	1145	13.7	0.9	13.0	968	24.8	1.3	0.4	702	0.7	0.0	100.0	34	158.2	0.3
1/8/10 22:30	2.9	1334	5.4	0.4	9.0	1128	17.0	1.1	7.7	956	14.5	0.8	0.4	696	0.7	0.0	160.0	34	260.7	0.5
1/8/10 23:00	2.8	1345	5.2	0.4	10.6	1136	20.1	1.3	4.6	960	8.6	0.5	0.4	696	0.7	0.0	38.0	34	56.6	0.1
1/9/10 0:00	3.1	1334	5.7	0.4	6.6	1128	12.4	0.8	4.0	956	7.4	0.4	0.5	696	0.9	0.0	43.0	34	64.6	0.1
1/9/10 0:30	5.6	1334	10.5	0.8	4.3	1128	8.0	0.5	3.7	956	6.9	0.4	0.5	696	0.9	0.0	70.0	34	108.3	0.2
1/9/10 1:00	8.2	1334	15.5	1.2	3.2	1130	5.9	0.4	6.4	959	12.0	0.6	0.4	702	0.7	0.0	42.0	34	63.0	0.1
1/9/10 1:30	8.0	1345	15.1	1.1	3.2	1136	5.9	0.4	4.7	960	8.8	0.5	0.6	696	1.1	0.0	42.0	34	63.0	0.1
1/9/10 2:00	7.6	1334	14.3	1.1	5.0	1128	9.3	0.6	2.9	956	5.4	0.3	0.5	696	0.9	0.0	120.0	34	192.0	0.4
1/9/10 2:30	8.3	1301	15.7	1.1	4.3	1108	8.0	0.5	3.7	945	6.9	0.4	0.5	702	1.1	0.0	170.0	34	278.0	0.5
1/9/10 3:00	9.5	1312	18.0	1.3	3.2	1115	5.9	0.4	3.3	950	6.1	0.3	0.6	702	1.1	0.0	120.0	34	192.0	0.4
1/9/10 3:30	8.4	1312	15.9	1.2	2.7	1115	5.0	0.3	2.4	950	4.4	0.2	0.4	702	0.7	0.0	180.0	34	295.4	0.6
1/9/10 4:00	5.9	1312	11.1	0.8	2.5	1112	4.6	0.3	5.0	944	9.3	0.5	0.5	691	0.9	0.0	140.0	34	226.2	0.4
1/9/10 4:30	4.5	1323	8.4	0.6	1.9	1121	3.5	0.2	5.2	951	9.7	0.5	0.6	696	1.1	0.0	52.0	34	79.0	0.2
1/9/10 4:30	4.3	1290	8.0	0.6	3.7	1097	6.9	0.4	5.5	935	10.3	0.5	0.4	691	0.7	0.0	29.0	34	42.5	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/9/10 5:00	5.4	1312	10.1	0.7	3.9	1114	7.3	0.5	6.5	947	12.2	0.6	0.4	696	0.7	0.0	31.0	34	45.6	0.1
1/9/10 5:30	5.1	1280	9.5	0.7	4.8	1093	9.0	0.6	6.9	937	13.0	0.7	0.5	702	0.9	0.0	55.0	34	83.9	0.2
1/9/10 6:00	4.4	1290	8.2	0.6	5.4	1101	10.1	0.6	5.1	941	9.5	0.5	0.5	702	0.9	0.0	200.0	34	330.4	0.6
1/9/10 6:30	5.9	1290	11.1	0.8	6.1	1101	11.4	0.7	2.9	941	5.4	0.3	0.4	702	0.7	0.0	360.0	34	616.8	1.2
1/9/10 7:00	3.5	1301	6.5	0.5	4.3	1108	8.0	0.5	3.1	945	5.7	0.3	0.5	702	0.9	0.0	150.0	34	243.4	0.5
1/9/10 7:30	3.8	1269	7.1	0.5	3.4	1086	6.3	0.4	2.6	932	4.8	0.3	0.4	702	0.7	0.0	130.0	34	209.1	0.4
1/9/10 8:00	4.0	1290	7.4	0.5	2.3	1101	4.2	0.3	6.4	941	12.0	0.6	0.5	702	0.9	0.0	41.0	34	61.4	0.1
1/9/10 8:30	4.5	1280	8.4	0.6	2.1	1095	3.9	0.2	9.1	940	17.2	0.9	0.5	707	0.9	0.0	59.0	34	90.3	0.2
1/9/10 9:00	4.8	1280	9.0	0.6	3.3	1097	6.1	0.4	10.1	943	19.1	1.0	0.3	712	0.5	0.0	73.0	35	113.3	0.2
1/9/10 9:30	5.0	1269	9.3	0.7	6.4	1086	12.0	0.7	7.3	932	13.7	0.7	0.4	702	0.7	0.0	39.0	34	58.2	0.1
1/9/10 10:00	5.5	1301	10.3	0.8	8.1	1111	15.3	1.0	4.1	952	7.6	0.4	0.4	712	0.7	0.0	81.0	35	126.5	0.2
1/9/10 10:30	5.1	1258	9.5	0.7	6.4	1081	12.0	0.7	3.1	931	5.7	0.3	0.4	707	0.7	0.0	44.0	34	66.2	0.1
1/9/10 11:00	4.5	1280	8.4	0.6	4.4	1098	8.2	0.5	3.1	946	5.7	0.3	0.3	717	0.5	0.0	41.0	35	61.4	0.1
1/9/10 11:30	3.3	1258	6.1	0.4	3.2	1081	5.9	0.4	2.9	931	5.4	0.3	0.4	707	0.7	0.0	28.0	34	40.9	0.1
1/9/10 12:00	3.6	1269	6.7	0.5	2.6	1088	4.8	0.3	3.2	935	5.9	0.3	0.4	707	0.7	0.0	24.0	34	34.8	0.1
1/9/10 12:30	3.2	1269	5.9	0.4	2.6	1091	4.8	0.3	3.0	942	5.6	0.3	0.4	717	0.7	0.0	20.0	35	28.6	0.1
1/9/10 13:00	4.4	1248	8.2	0.6	2.4	1073	4.4	0.3	3.3	927	6.1	0.3	0.4	707	0.7	0.0	24.0	34	34.8	0.1
1/9/10 13:30	6.5	1258	12.2	0.9	2.3	1081	4.2	0.3	2.0	931	3.7	0.2	0.3	707	0.5	0.0	20.0	34	28.6	0.1
1/9/10 14:00	6.8	1248	12.8	0.9	2.0	1072	3.7	0.2	1.9	924	3.5	0.2	0.5	702	0.9	0.0	20.0	34	28.6	0.1
1/9/10 14:30	5.4	1248	10.1	0.7	2.6	1073	4.8	0.3	1.7	927	3.1	0.2	0.3	707	0.5	0.0	19.0	34	27.1	0.1
1/9/10 15:00	4.6	1248	8.6	0.6	1.7	1070	3.1	0.2	1.6	921	2.9	0.2	0.4	696	0.7	0.0	21.0	34	30.2	0.1
1/9/10 15:30	3.6	1227	6.7	0.5	2.0	1056	3.7	0.2	1.6	912	2.9	0.1	0.4	696	0.7	0.0	18.0	34	25.6	0.0
1/9/10 16:00	3.7	1227	6.9	0.5	1.1	1058	2.0	0.1	2.4	915	4.4	0.2	0.4	702	0.7	0.0	18.0	34	25.6	0.0
1/9/10 16:30	3.5	1237	6.5	0.5	1.4	1061	2.6	0.2	1.6	913	2.9	0.2	0.4	691	0.7	0.0	19.0	34	27.1	0.1
1/9/10 17:00	3.0	1237	5.6	0.4	1.1	1063	2.0	0.1	1.7	916	3.1	0.2	0.4	696	0.7	0.0	16.0	34	22.6	0.0
1/9/10 17:30	3.2	1227	5.9	0.4	2.0	1056	3.7	0.2	1.7	912	3.1	0.2	0.3	696	0.5	0.0	12.0	34	16.6	0.0
1/9/10 18:00	2.9	1216	5.4	0.4	1.2	1047	2.2	0.1	1.7	905	3.1	0.2	0.3	691	0.5	0.0	12.0	34	16.6	0.0
1/9/10 18:30	3.2	1227	5.9	0.4	1.4	1054	2.6	0.2	1.4	909	2.6	0.1	0.4	691	0.7	0.0	12.0	34	16.6	0.0
1/9/10 19:00	2.7	1216	5.0	0.3	1.3	1047	2.4	0.1	2.2	905	4.0	0.2	0.4	691	0.7	0.0	14.0	34	19.6	0.0
1/9/10 19:30	2.9	1227	5.4	0.4	1.5	1053	2.7	0.2	1.7	906	3.1	0.2	0.5	686	0.9	0.0	13.0	33	18.1	0.0
1/9/10 20:00	2.9	1206	5.4	0.4	1.7	1037	3.1	0.2	1.6	895	2.9	0.1	0.3	681	0.5	0.0	15.0	33	21.1	0.0
1/9/10 20:30	2.5	1196	4.6	0.3	0.9	1030	1.6	0.1	1.5	890	2.7	0.1	0.5	681	0.9	0.0	14.0	33	19.6	0.0
1/9/10 21:00	2.3	1206	4.2	0.3	1.4	1035	2.6	0.1	1.3	892	2.4	0.1	0.6	676	1.1	0.0	14.0	33	19.6	0.0
1/9/10 21:30	2.3	1196	4.2	0.3	1.0	1027	1.8	0.1	1.4	884	2.6	0.1	0.5	671	0.9	0.0	12.0	33	16.6	0.0
1/9/10 22:00	2.4	1185	4.4	0.3	1.2	1023	2.2	0.1	1.3	886	2.4	0.1	0.4	681	0.7	0.0	13.0	33	18.1	0.0
1/9/10 22:30	2.5	1227	4.6	0.3	1.2	1048	2.2	0.1	1.3	897	2.4	0.1	0.3	671	0.5	0.0	13.0	33	18.1	0.0
1/9/10 23:00	2.1	1175	3.9	0.3	2.1	1013	3.9	0.2	1.4	876	2.6	0.1	0.4	671	0.7	0.0	13.0	33	18.1	0.0
1/9/10 23:30	2.5	1175	4.6	0.3	0.8	1013	1.4	0.1	1.3	876	2.4	0.1	0.3	671	0.5	0.0	14.0	33	19.6	0.0
1/10/10 0:00	2.4	1185	4.4	0.3	1.0	1017	1.8	0.1	1.3	874	2.4	0.1	0.5	661	0.9	0.0	12.0	32	16.6	0.0
1/10/10 0:30	2.5	1165	4.6	0.3	1.1	1001	2.0	0.1	1.3	863	2.4	0.1	0.4	656	0.7	0.0	13.0	32	18.1	0.0
1/10/10 1:00	2.2	1155	4.0	0.3	1.0	991	1.8	0.1	1.3	853	2.4	0.1	0.4	646	0.7	0.0	27.0	32	39.4	0.1
1/10/10 1:30	2.9	1155	5.4	0.3	1.5	993	2.7	0.2	1.3	856	2.4	0.1	0.3	651	0.5	0.0	15.0	32	21.1	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/10/10 2:00	2.4	1145	4.4	0.3	1.2	984	2.2	0.1	1.2	849	2.2	0.1	0.4	646	0.7	0.0	18.0	32	25.6	0.0
1/10/10 2:30	2.3	1135	4.2	0.3	1.2	979	2.2	0.1	1.3	848	2.4	0.1	0.5	651	0.9	0.0	16.0	32	22.6	0.0
1/10/10 3:00	2.3	1135	4.2	0.3	0.9	979	1.6	0.1	1.5	848	2.7	0.1	0.5	651	0.9	0.0	43.0	32	64.6	0.1
1/10/10 3:30	2.2	1135	4.0	0.3	1.5	976	2.7	0.2	1.3	842	2.4	0.1	0.4	641	0.7	0.0	24.0	31	34.8	0.1
1/10/10 4:00	2.2	1125	4.0	0.3	1.3	969	2.4	0.1	1.3	838	2.4	0.1	0.4	641	0.7	0.0	29.0	31	42.5	0.1
1/10/10 4:30	2.3	1125	4.2	0.3	1.2	966	2.2	0.1	1.3	832	2.4	0.1	0.3	631	0.5	0.0	22.0	31	31.7	0.1
1/10/10 5:00	2.2	1125	4.0	0.3	1.4	966	2.6	0.1	1.6	832	2.9	0.1	0.5	631	0.9	0.0	14.0	31	19.6	0.0
1/10/10 5:30	2.1	1125	3.9	0.2	0.9	968	1.6	0.1	1.9	835	3.5	0.2	0.4	636	0.7	0.0	16.0	31	22.6	0.0
1/10/10 6:00	2.4	1115	4.4	0.3	1.0	961	1.8	0.1	1.7	831	3.1	0.1	0.3	636	0.5	0.0	16.0	31	22.6	0.0
1/10/10 6:30	2.1	1096	3.9	0.2	1.5	946	2.7	0.1	1.9	820	3.5	0.2	0.4	631	0.7	0.0	13.0	31	18.1	0.0
1/10/10 7:00	2.1	1096	3.9	0.2	1.6	943	2.9	0.2	1.5	815	2.7	0.1	0.3	622	0.5	0.0	13.0	31	18.1	0.0
1/10/10 7:30	2.2	1096	4.0	0.2	1.4	940	2.6	0.1	1.6	809	2.9	0.1	0.4	612	0.7	0.0	13.0	30	18.1	0.0
1/10/10 8:00	2.2	1096	4.0	0.2	1.2	943	2.2	0.1	1.7	815	3.1	0.1	0.4	622	0.7	0.0	12.0	31	16.6	0.0
1/10/10 8:30	2.1	1086	3.9	0.2	1.2	935	2.2	0.1	1.7	808	3.1	0.1	0.4	617	0.7	0.0	12.0	30	16.6	0.0
1/10/10 9:00	2.3	1086	4.2	0.3	0.9	934	1.6	0.1	1.5	805	2.7	0.1	0.4	612	0.7	0.0	13.0	30	18.1	0.0
1/10/10 9:30	2.4	1067	4.4	0.3	0.9	920	1.6	0.1	1.3	797	2.4	0.1	0.3	612	0.5	0.0	13.0	30	18.1	0.0
1/10/10 10:00	2.4	1067	4.4	0.3	1.6	920	2.9	0.2	1.2	797	2.2	0.1	0.3	612	0.5	0.0	9.2	30	12.6	0.0
1/10/10 10:30	2.3	1048	4.2	0.2	0.9	905	1.6	0.1	1.6	784	2.9	0.1	0.6	602	1.1	0.0	13.0	30	18.1	0.0
1/10/10 11:00	2.8	1058	5.2	0.3	0.9	913	1.6	0.1	1.4	790	2.6	0.1	0.3	607	0.5	0.0	12.0	30	16.6	0.0
1/10/10 11:30	2.6	1067	4.8	0.3	1.0	916	1.8	0.1	1.2	789	2.2	0.1	0.3	598	0.5	0.0	13.0	29	18.1	0.0
1/10/10 12:00	2.2	1048	4.0	0.2	0.8	903	1.4	0.1	1.2	781	2.2	0.1	0.5	598	0.9	0.0	9.9	29	13.6	0.0
1/10/10 12:30	2.0	1058	3.7	0.2	0.8	908	1.4	0.1	1.1	782	2.0	0.1	0.4	593	0.7	0.0	16.0	29	22.6	0.0
1/10/10 13:00	2.1	1058	3.9	0.2	0.9	908	1.6	0.1	2.7	782	5.0	0.2	0.4	593	0.7	0.0	22.0	29	31.7	0.1
1/10/10 13:30	1.9	1020	3.5	0.2	1.0	881	1.8	0.1	1.3	778	2.4	0.1	0.3	593	0.5	0.0	20.0	29	28.6	0.0
1/10/10 14:00	2.3	1039	4.2	0.2	1.0	894	1.8	0.1	1.4	764	2.6	0.1	0.4	588	0.7	0.0	16.0	29	22.6	0.0
1/10/10 14:30	1.9	1029	3.5	0.2	2.1	886	3.9	0.2	1.2	772	2.2	0.1	0.4	588	0.7	0.0	16.0	29	22.6	0.0
1/10/10 15:00	1.9	1029	3.5	0.2	0.7	884	1.3	0.1	1.5	765	2.6	0.1	0.3	584	0.5	0.0	13.0	29	18.1	0.0
1/10/10 16:00	2.1	1012	3.9	0.2	1.0	872	1.8	0.1	1.3	762	2.7	0.1	0.4	579	0.7	0.0	11.0	29	15.2	0.0
1/10/10 16:30	2.2	1003	4.0	0.2	1.0	865	1.8	0.1	1.3	755	2.4	0.1	0.4	579	0.7	0.0	12.0	29	16.6	0.0
1/10/10 17:00	1.8	995	3.3	0.2	1.2	859	2.2	0.1	1.2	745	2.2	0.1	0.4	575	0.7	0.0	11.0	28	15.2	0.0
1/10/10 17:30	2.3	1003	4.2	0.2	1.1	862	2.0	0.1	1.2	743	2.2	0.1	0.3	565	0.5	0.0	10.0	28	13.7	0.0
1/10/10 18:00	1.9	978	3.5	0.2	1.0	847	1.8	0.1	1.3	736	2.4	0.1	0.4	570	0.7	0.0	10.0	28	13.7	0.0
1/10/10 18:30	1.6	1012	2.9	0.2	1.0	868	1.8	0.1	1.2	747	2.2	0.1	0.3	565	0.5	0.0	9.6	28	13.1	0.0
1/10/10 19:00	2.0	978	3.7	0.2	1.0	845	1.8	0.1	1.1	733	2.0	0.1	0.3	565	0.5	0.0	12.0	28	16.6	0.0
1/10/10 19:30	2.0	978	3.7	0.2	0.8	844	1.4	0.1	1.3	731	2.4	0.1	0.4	561	0.7	0.0	7.8	28	10.5	0.0
1/10/10 20:00	1.9	986	3.5	0.2	0.7	849	1.3	0.1	1.4	734	2.6	0.1	0.5	561	0.9	0.0	8.4	28	11.4	0.0
1/10/10 20:30	1.7	986	3.1	0.2	0.9	848	1.6	0.1	1.1	731	2.0	0.1	0.3	556	0.5	0.0	13.0	27	18.1	0.0
1/10/10 21:00	2.0	970	3.7	0.2	1.2	835	2.2	0.1	1.2	722	2.2	0.1	0.4	552	0.7	0.0	20.0	27	28.6	0.0
1/10/10 21:30	2.0	970	3.7	0.2	0.8	834	1.4	0.1	1.3	719	2.4	0.1	0.3	547	0.5	0.0	20.0	27	28.6	0.0
1/10/10 22:00	2.1	962	3.9	0.2	1.1	828	2.0	0.1	1.3	716	2.4	0.1	0.4	547	0.7	0.0	17.0	27	24.1	0.0
1/10/10 22:30	2.1	953	3.9	0.2	1.0	823	1.8	0.1	0.9	713	1.6	0.1	0.4	547	0.7	0.0	19.0	27	27.1	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/10/10 23:00	2.1	962	3.9	0.2	0.9	828	1.6	0.1	1.3	716	2.4	0.1	0.4	547	0.7	0.0	24.0	27	34.8	0.1
1/10/10 23:30	2.0	970	3.7	0.2	0.6	834	1.1	0.1	1.4	719	2.6	0.1	0.3	547	0.5	0.0	23.0	27	33.2	0.1
1/10/10 0:00	1.8	937	3.3	0.2	0.8	810	1.4	0.1	2.4	703	4.4	0.2	0.3	543	0.5	0.0	17.0	27	24.1	0.0
1/11/10 0:30	2.4	953	4.4	0.2	0.7	820	1.3	0.1	1.4	707	2.6	0.1	0.4	539	0.7	0.0	17.0	27	24.1	0.0
1/11/10 1:00	1.6	937	2.9	0.2	1.4	806	2.6	0.1	1.2	695	2.2	0.1	0.4	530	0.7	0.0	20.0	26	28.6	0.0
1/11/10 1:30	2.0	937	3.7	0.2	0.9	809	1.6	0.1	1.7	701	3.1	0.1	0.5	539	0.9	0.0	14.0	27	19.6	0.0
1/11/10 2:00	1.9	937	3.5	0.2	1.0	807	1.8	0.1	1.4	698	2.6	0.1	0.3	534	0.5	0.0	13.0	26	18.1	0.0
1/11/10 2:30	1.8	937	3.3	0.2	0.8	807	1.4	0.1	1.3	698	2.4	0.1	0.3	534	0.5	0.0	11.0	26	15.2	0.0
1/11/10 3:00	1.6	937	2.9	0.2	1.0	805	1.8	0.1	1.3	693	2.4	0.1	0.5	525	0.9	0.0	9.7	26	13.3	0.0
1/11/10 3:30	1.9	929	3.5	0.2	1.0	801	1.8	0.1	1.5	692	2.7	0.1	0.3	530	0.5	0.0	11.0	26	15.2	0.0
1/11/10 4:00	1.8	921	3.3	0.2	1.1	794	2.0	0.1	1.3	686	2.4	0.1	0.5	525	0.9	0.0	8.9	26	12.1	0.0
1/11/10 4:30	1.8	921	3.3	0.2	0.8	792	1.4	0.1	1.2	684	2.2	0.1	0.5	521	0.9	0.0	9.7	26	13.3	0.0
1/11/10 5:00	2.1	929	3.9	0.2	1.0	798	1.8	0.1	1.1	687	2.0	0.1	0.3	521	0.5	0.0	11.0	26	15.2	0.0
1/11/10 5:30	2.3	913	4.2	0.2	1.0	786	1.8	0.1	3.0	678	5.6	0.2	0.4	517	0.7	0.0	12.0	26	16.6	0.0
1/11/10 6:00	1.9	913	3.5	0.2	1.0	786	1.8	0.1	1.0	678	1.8	0.1	0.3	517	0.5	0.0	12.0	26	16.6	0.0
1/11/10 6:30	1.9	897	3.5	0.2	0.7	775	1.3	0.1	1.0	672	1.8	0.1	0.3	517	0.5	0.0	9.4	26	12.8	0.0
1/11/10 7:00	2.2	905	4.0	0.2	1.0	779	1.8	0.1	1.1	672	2.0	0.1	0.3	512	0.5	0.0	12.0	25	16.6	0.0
1/11/10 7:30	2.2	905	4.0	0.2	0.7	779	1.3	0.1	1.2	672	2.2	0.1	0.4	512	0.7	0.0	12.0	25	16.6	0.0
1/11/10 8:00	2.2	905	4.0	0.2	0.6	777	1.3	0.1	1.2	670	2.2	0.1	0.3	508	0.5	0.0	9.5	25	13.0	0.0
1/11/10 8:30	1.9	897	3.5	0.2	0.6	772	1.1	0.0	1.3	666	2.4	0.1	0.3	508	0.5	0.0	13.0	25	18.1	0.0
1/11/10 9:00	2.1	905	3.9	0.2	1.0	777	1.8	0.1	1.2	670	2.2	0.1	0.4	508	0.7	0.0	9.7	25	13.3	0.0
1/11/10 9:30	1.7	890	3.1	0.2	0.7	767	1.3	0.1	0.9	663	1.6	0.1	0.5	508	0.9	0.0	7.7	25	10.4	0.0
1/11/10 10:00	2.1	890	3.9	0.2	0.7	765	1.3	0.1	0.9	661	1.6	0.1	0.4	504	0.7	0.0	11.0	25	15.2	0.0
1/11/10 10:30	1.9	882	3.5	0.2	0.6	760	1.1	0.0	1.1	658	2.0	0.1	1.0	504	1.8	0.1	9.1	25	12.4	0.0
1/11/10 11:00	1.8	874	3.3	0.2	0.9	755	1.6	0.1	1.0	654	1.8	0.1	0.4	504	0.7	0.0	9.5	25	13.0	0.0
1/11/10 11:30	2.0	874	3.7	0.2	1.3	755	2.4	0.1	1.1	654	2.0	0.1	0.3	504	0.5	0.0	10.0	25	13.7	0.0
1/11/10 12:00	1.7	882	3.1	0.2	0.7	759	1.3	0.1	1.2	655	2.2	0.1	0.4	500	0.7	0.0	11.0	25	15.2	0.0
1/11/10 12:30	1.7	874	3.1	0.2	1.0	753	1.8	0.1	1.0	652	1.8	0.1	0.3	500	0.5	0.0	8.2	25	11.1	0.0
1/11/10 13:00	1.7	874	3.1	0.2	0.6	752	1.1	0.0	0.9	649	1.6	0.1	0.3	495	0.5	0.0	8.6	25	11.7	0.0
1/11/10 13:30	1.8	874	3.3	0.2	1.0	752	1.8	0.1	1.0	649	1.8	0.1	0.6	495	1.1	0.0	9.6	25	13.1	0.0
1/11/10 14:00	2.2	882	4.0	0.2	1.8	757	3.3	0.1	0.9	653	1.6	0.1	0.4	495	0.7	0.0	8.2	25	11.1	0.0
1/11/10 14:30	2.1	866	3.9	0.2	0.6	745	1.1	0.0	0.8	644	1.4	0.1	0.4	491	0.7	0.0	9.8	24	13.4	0.0
1/11/10 15:00	1.7	866	3.1	0.2	0.6	744	1.1	0.0	1.0	641	1.8	0.1	0.3	487	0.5	0.0	8.1	24	11.0	0.0
1/11/10 15:30	1.9	843	3.5	0.2	0.7	730	1.3	0.1	1.1	634	2.0	0.1	0.3	491	0.5	0.0	9.8	24	13.4	0.0
1/11/10 16:00	1.9	859	3.5	0.2	0.7	739	1.3	0.1	1.0	638	1.8	0.1	0.3	487	0.5	0.0	7.9	24	10.7	0.0
1/11/10 16:30	2.5	851	4.6	0.2	0.7	732	1.3	0.1	0.9	633	1.6	0.1	0.7	483	1.3	0.0	12.0	24	16.6	0.0
1/11/10 17:00	1.8	836	3.3	0.2	0.6	723	1.1	0.0	0.8	629	1.4	0.1	0.5	487	0.9	0.0	9.2	24	12.6	0.0
1/11/10 17:30	1.9	851	3.5	0.2	0.5	732	0.9	0.0	1.0	633	1.8	0.1	0.3	483	0.5	0.0	8.4	24	11.4	0.0
1/11/10 18:00	1.8	851	3.3	0.2	0.4	731	0.7	0.0	1.0	630	1.8	0.1	0.4	479	0.7	0.0	7.6	24	10.2	0.0
1/11/10 18:30	1.5	859	2.7	0.1	0.9	736	1.6	0.1	0.9	633	1.6	0.1	0.3	479	0.5	0.0	6.9	24	9.2	0.0
1/11/10 19:00	2.4	836	4.4	0.2	0.6	721	1.1	0.0	0.9	624	1.6	0.1	0.5	479	0.9	0.0	9.1	24	12.4	0.0
1/11/10 19:30	1.8	836	3.3	0.2	0.5	721	0.9	0.0	1.0	624	1.8	0.1	0.3	479	0.5	0.0	8.6	24	11.7	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/11/10 20:00	1.8	843	3.3	0.2	0.7	725	1.3	0.1	1.0	625	1.8	0.1	0.4	475	0.7	0.0	7.7	24	10.4	0.0
1/11/10 20:30	1.8	836	3.3	0.2	0.6	720	1.1	0.0	1.7	622	3.1	0.1	0.7	475	1.3	0.0	7.3	24	9.8	0.0
1/11/10 21:00	2.1	836	3.9	0.2	0.9	720	1.6	0.1	1.0	622	1.8	0.1	0.3	475	0.5	0.0	6.8	24	9.1	0.0
1/11/10 21:30	1.9	828	3.5	0.2	1.1	713	2.0	0.1	0.8	616	1.4	0.0	0.4	471	0.7	0.0	8.9	23	12.1	0.0
1/11/10 22:00	1.5	836	2.7	0.1	0.6	718	1.1	0.0	1.1	619	2.0	0.1	0.4	471	0.7	0.0	8.2	23	11.1	0.0
1/11/10 22:30	1.6	821	2.9	0.1	0.9	708	1.6	0.1	0.8	613	1.4	0.0	0.3	471	0.5	0.0	7.0	23	9.4	0.0
1/11/10 23:00	1.5	828	2.7	0.1	0.9	712	1.6	0.1	0.9	614	1.6	0.1	0.3	467	0.5	0.0	9.9	23	13.6	0.0
1/11/10 23:30	1.5	821	2.7	0.1	1.2	708	2.2	0.1	2.2	613	4.0	0.1	0.4	471	0.7	0.0	11.0	23	15.2	0.0
1/12/10 00:00	1.5	821	2.7	0.1	0.6	708	1.1	0.0	1.0	613	1.8	0.1	0.3	471	0.5	0.0	9.3	23	12.7	0.0
1/12/10 03:00	1.9	813	3.5	0.2	0.8	702	1.4	0.1	1.4	608	2.6	0.1	0.3	467	0.5	0.0	8.3	23	11.3	0.0
1/12/10 1:00	1.5	813	2.7	0.1	0.7	702	1.3	0.0	1.0	608	1.8	0.1	0.3	467	0.5	0.0	6.9	23	9.2	0.0
1/12/10 1:30	1.7	813	3.1	0.1	0.6	700	1.1	0.0	1.3	605	2.4	0.1	0.3	462	0.5	0.0	7.2	23	9.7	0.0
1/12/10 2:00	1.5	806	2.7	0.1	0.8	695	1.4	0.1	1.2	602	2.2	0.1	0.4	462	0.7	0.0	7.0	23	9.4	0.0
1/12/10 2:30	1.8	813	3.3	0.2	0.6	702	1.1	0.0	1.0	608	1.8	0.1	0.4	467	0.7	0.0	7.3	23	9.8	0.0
1/12/10 3:00	1.8	821	3.3	0.2	0.8	707	1.4	0.1	1.1	611	2.0	0.1	0.4	467	0.7	0.0	7.9	23	10.7	0.0
1/12/10 3:30	2.0	821	3.7	0.2	0.6	708	1.1	0.0	1.0	613	1.8	0.1	0.4	471	0.7	0.0	8.1	23	11.0	0.0
1/12/10 4:00	2.3	813	4.2	0.2	0.7	704	1.3	0.0	1.0	612	1.8	0.1	0.4	475	0.7	0.0	11.0	24	15.2	0.0
1/12/10 4:30	1.9	821	3.5	0.2	0.9	711	1.6	0.1	1.2	618	2.2	0.1	0.7	479	1.3	0.0	15.0	24	21.1	0.0
1/12/10 5:00	1.7	821	3.1	0.1	1.2	713	2.2	0.1	1.1	623	2.0	0.1	0.3	487	0.5	0.0	180.0	24	295.4	0.4
1/12/10 5:30	1.9	836	3.5	0.2	0.7	725	1.3	0.1	1.2	631	2.2	0.1	0.4	491	0.7	0.0	190.0	24	312.9	0.4
1/12/10 6:00	2.0	851	3.7	0.2	0.9	736	1.6	0.1	3.7	640	6.9	0.2	0.4	495	0.7	0.0	150.0	25	243.4	0.3
1/12/10 6:30	1.8	851	3.3	0.2	1.2	738	2.2	0.1	1.2	643	2.2	0.1	0.3	500	0.5	0.0	160.0	25	260.7	0.4
1/12/10 7:00	2.0	843	3.7	0.2	0.7	734	1.3	0.1	1.3	642	2.4	0.1	0.4	504	0.7	0.0	310.0	25	526.2	0.7
1/12/10 7:30	2.1	843	3.9	0.2	1.2	737	2.2	0.1	2.8	647	5.2	0.2	0.4	512	0.7	0.0	130.0	25	209.1	0.3
1/12/10 8:00	2.1	851	3.9	0.2	1.5	743	2.7	0.1	4.9	653	9.2	0.3	0.4	517	0.7	0.0	41.0	26	61.4	0.1
1/12/10 8:30	2.1	851	3.9	0.2	1.1	743	2.0	0.1	5.3	653	9.9	0.4	0.4	517	0.7	0.0	23.0	26	33.2	0.0
1/12/10 9:00	2.2	859	4.0	0.2	2.4	750	4.4	0.2	6.1	658	11.4	0.4	0.4	521	0.7	0.0	31.0	26	45.6	0.1
1/12/10 9:30	2.1	851	3.9	0.2	3.7	745	6.9	0.3	7.7	655	14.5	0.5	0.3	521	0.5	0.0	21.0	26	30.2	0.0
1/12/10 10:00	1.9	851	3.5	0.2	4.1	743	7.6	0.3	6.9	653	13.0	0.5	0.4	517	0.7	0.0	20.0	26	28.6	0.0
1/12/10 10:30	2.0	851	3.7	0.2	4.8	743	9.0	0.4	4.8	653	9.0	0.3	0.4	517	0.7	0.0	16.0	26	22.6	0.0
1/12/10 11:00	2.0	843	3.7	0.2	5.9	737	11.1	0.5	2.5	647	4.6	0.2	0.3	512	0.5	0.0	17.0	25	24.1	0.0
1/12/10 12:00	2.0	859	3.7	0.2	5.4	748	10.1	0.4	1.9	656	3.5	0.1	0.4	517	0.7	0.0	16.0	26	22.6	0.0
1/12/10 12:30	2.3	860	4.1	0.2	2.0	752	3.7	0.2	1.3	661	2.4	0.1	0.5	525	0.9	0.0	28.0	26	40.9	0.1
1/12/10 13:00	2.8	861	5.1	0.2	1.5	755	2.7	0.1	1.2	665	2.2	0.1	0.3	530	0.5	0.0	40.0	26	59.8	0.1
1/12/10 13:30	3.3	863	6.0	0.3	1.1	757	2.0	0.1	1.2	668	2.2	0.1	0.3	534	0.5	0.0	43.0	26	64.6	0.1
1/12/10 14:00	3.8	865	7.0	0.3	1.1	757	2.0	0.1	1.1	666	2.0	0.1	0.4	530	0.7	0.0	190.0	26	312.9	0.5
1/12/10 14:30	4.5	874	8.4	0.4	1.0	763	1.8	0.1	1.4	670	2.6	0.1	0.4	530	0.7	0.0	470.0	26	818.7	1.2
1/12/10 15:00	4.9	859	9.2	0.4	0.9	754	1.6	0.1	1.8	666	3.3	0.1	0.3	534	0.5	0.0	190.0	26	312.9	0.5
1/12/10 15:30	5.2	866	9.7	0.5	0.7	762	1.3	0.1	2.0	674	3.7	0.1	0.3	543	0.5	0.0	83.0	27	129.8	0.2
1/12/10 16:00	5.1	861	9.6	0.5	0.7	757	1.3	0.1	2.2	670	4.0	0.2	0.4	539	0.7	0.0	71.0	27	110.0	0.2
1/12/10 16:30	4.4	866	8.2	0.4	1.2	762	2.2	0.1	4.3	674	8.0	0.3	0.3	543	0.5	0.0	51.0	27	77.4	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/12/10 17:00	3.3	866	6.1	0.3	1.2	764	2.2	0.1	8.6	677	16.3	0.6	0.3	547	0.5	0.0	34.0	27	50.3	0.1
1/12/10 17:30	2.6	874	4.8	0.2	1.8	769	3.3	0.1	8.4	680	15.9	0.6	0.4	547	0.7	0.0	31.0	27	45.6	0.1
1/12/10 18:00	2.2	874	4.0	0.2	3.6	770	6.7	0.3	6.7	683	12.6	0.5	0.3	552	0.5	0.0	34.0	27	50.3	0.1
1/12/10 18:30	2.1	859	3.9	0.2	6.6	757	12.4	0.5	3.7	671	6.9	0.3	0.3	543	0.5	0.0	26.0	27	37.8	0.1
1/12/10 19:00	2.1	866	3.9	0.2	6.2	764	11.6	0.5	2.8	677	5.2	0.2	0.5	547	0.9	0.0	21.0	27	30.2	0.0
1/12/10 19:30	2.1	874	3.9	0.2	4.5	767	8.4	0.4	2.2	678	4.0	0.2	0.3	543	0.5	0.0	18.0	27	25.6	0.0
1/12/10 20:00	2.1	874	3.9	0.2	2.9	767	5.4	0.2	2.0	678	3.7	0.1	0.3	543	0.5	0.0	22.0	27	31.7	0.0
1/12/10 20:30	1.9	866	3.5	0.2	2.4	762	4.4	0.2	1.5	674	2.7	0.1	0.3	543	0.5	0.0	20.0	27	28.6	0.0
1/12/10 21:00	1.8	866	3.3	0.2	2.1	762	3.9	0.2	1.4	674	2.6	0.1	0.3	543	0.5	0.0	85.0	27	133.1	0.2
1/12/10 21:30	2.0	866	3.7	0.2	1.4	762	2.6	0.1	1.2	674	2.2	0.1	0.3	543	0.5	0.0	70.0	27	108.3	0.2
1/12/10 22:00	2.4	859	4.4	0.2	1.2	756	2.2	0.1	1.2	669	2.2	0.1	0.4	539	0.7	0.0	41.0	27	61.4	0.1
1/12/10 22:30	3.6	851	6.7	0.3	1.0	750	1.8	0.1	1.3	666	2.4	0.1	0.3	539	0.5	0.0	36.0	27	53.5	0.1
1/12/10 23:00	5.4	859	10.1	0.5	1.0	754	1.8	0.1	1.2	666	2.2	0.1	0.4	534	0.7	0.0	53.0	26	80.6	0.1
1/12/10 23:30	5.9	866	11.1	0.5	1.2	759	2.2	0.1	1.7	669	3.1	0.1	0.4	534	0.7	0.0	30.0	26	44.0	0.1
1/13/10 0:00	5.3	859	9.9	0.5	1.2	754	2.2	0.1	2.3	666	4.2	0.2	0.4	534	0.7	0.0	31.0	26	45.6	0.1
1/13/10 0:30	4.2	859	7.8	0.4	1.0	754	1.8	0.1	2.0	666	3.7	0.1	0.3	534	0.5	0.0	34.0	26	50.3	0.1
1/13/10 1:00	2.8	851	5.2	0.2	1.7	749	3.1	0.1	1.9	663	3.5	0.1	0.3	534	0.5	0.0	56.0	26	85.5	0.1
1/13/10 1:30	2.6	843	4.8	0.2	2.1	747	3.9	0.2	2.0	665	3.7	0.1	0.4	543	0.7	0.0	28.0	27	40.9	0.1
1/13/10 2:00	2.3	859	4.2	0.2	1.8	754	3.3	0.1	1.9	666	3.5	0.1	0.3	534	0.5	0.0	35.0	26	51.9	0.1
1/13/10 2:30	2.0	851	3.7	0.2	1.5	748	2.7	0.1	1.6	660	2.9	0.1	0.4	530	0.7	0.0	39.0	26	58.2	0.1
1/13/10 3:00	2.2	843	4.0	0.2	1.3	742	2.4	0.1	1.7	657	3.1	0.1	0.3	530	0.5	0.0	35.0	26	51.9	0.1
1/13/10 3:30	1.8	851	3.3	0.2	1.2	749	2.2	0.1	1.6	663	2.9	0.1	0.3	534	0.5	0.0	34.0	26	50.3	0.1
1/13/10 4:00	2.1	851	3.9	0.2	1.7	749	3.1	0.1	1.7	663	3.1	0.1	0.3	534	0.5	0.0	31.0	26	45.6	0.1
1/13/10 4:30	1.7	851	3.1	0.1	1.7	749	3.1	0.1	2.0	663	3.7	0.1	0.3	534	0.5	0.0	38.0	26	56.6	0.1
1/13/10 5:00	2.4	843	4.4	0.2	1.1	742	2.0	0.1	1.7	657	3.1	0.1	0.3	530	0.5	0.0	22.0	26	31.7	0.0
1/13/10 5:30	2.2	843	4.0	0.2	1.1	744	2.0	0.1	1.6	660	2.9	0.1	0.3	534	0.5	0.0	30.0	26	44.0	0.1
1/13/10 6:00	2.3	851	4.2	0.2	1.1	749	2.0	0.1	1.5	663	2.7	0.1	0.5	534	0.9	0.0	110.0	26	175.1	0.3
1/13/10 6:30	2.4	836	4.4	0.2	0.9	740	1.6	0.1	1.6	659	2.9	0.1	0.3	539	0.5	0.0	44.0	27	66.2	0.1
1/13/10 7:00	2.3	836	4.2	0.2	1.1	740	2.0	0.1	1.9	659	3.5	0.1	0.3	539	0.5	0.0	24.0	27	34.8	0.1
1/13/10 7:30	2.1	851	3.9	0.2	1.0	750	1.8	0.1	1.9	666	3.5	0.1	0.3	539	0.5	0.0	21.0	27	30.2	0.0
1/13/10 8:00	2.1	851	3.9	0.2	1.0	752	1.8	0.1	2.8	668	5.2	0.2	0.5	543	0.9	0.0	74.0	27	114.9	0.2
1/13/10 8:30	2.1	851	3.9	0.2	1.2	752	2.2	0.1	2.1	668	3.9	0.1	0.4	543	0.7	0.0	480.0	27	837.2	1.3
1/13/10 9:00	2.6	836	4.8	0.2	0.9	740	1.6	0.1	2.4	659	4.4	0.2	0.7	539	1.3	0.0	77.0	27	119.9	0.2
1/13/10 9:30	1.9	836	3.5	0.2	0.9	741	1.6	0.1	2.4	662	4.4	0.2	0.4	543	0.7	0.0	58.0	27	88.7	0.1
1/13/10 10:00	2.3	851	4.2	0.2	1.7	752	3.1	0.1	1.3	668	2.4	0.1	0.3	543	0.5	0.0	34.0	27	50.3	0.1
1/13/10 10:30	1.9	843	3.5	0.2	1.9	747	3.5	0.1	2.2	665	4.0	0.2	0.3	543	0.5	0.0	28.0	27	40.9	0.1
1/13/10 11:00	2.0	843	3.7	0.2	1.0	747	1.8	0.1	7.1	665	13.4	0.5	0.3	543	0.5	0.0	22.0	27	31.7	0.0
1/13/10 11:30	3.1	859	5.7	0.3	0.9	757	1.6	0.1	6.8	671	12.8	0.5	1.5	543	2.7	0.1	23.0	27	33.2	0.1
1/13/10 12:00	2.1	851	3.9	0.2	2.0	758	3.7	0.2	3.7	679	6.9	0.3	0.7	561	1.3	0.0	24.0	28	34.8	0.1
1/13/10 12:30	2.1	851	3.9	0.2	5.3	763	9.9	0.4	2.2	690	4.0	0.2	0.4	579	0.7	0.0	29.0	29	42.5	0.1
1/13/10 13:00	2.1	851	3.9	0.2	4.8	766	9.0	0.4	1.4	695	2.6	0.1	0.4	588	0.7	0.0	220.0	29	365.6	0.6
1/13/10 13:30	1.9	851	3.5	0.2	2.4	771	4.4	0.2	1.5	704	2.7	0.1	0.4	602	0.7	0.0	340.0	30	580.4	1.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/13/10 14:00	2.0	859	3.7	0.2	1.8	785	3.3	0.1	1.3	724	2.4	0.1	0.4	631	0.7	0.0	360.0	31	616.8	1.1
1/13/10 14:30	2.4	859	4.4	0.2	1.2	790	2.2	0.1	2.2	732	4.0	0.2	0.4	646	0.7	0.0	540.0	32	948.7	1.7
1/13/10 15:00	2.7	866	5.0	0.2	0.9	803	1.6	0.1	1.9	750	3.5	0.1	0.8	671	1.4	0.1	330.0	33	562.3	1.0
1/13/10 15:30	2.4	882	4.4	0.2	2.1	820	3.9	0.2	5.1	769	9.5	0.4	0.4	691	0.7	0.0	230.0	34	383.2	0.7
1/13/10 16:00	2.1	882	3.9	0.2	1.0	829	1.8	0.1	9.5	784	18.0	0.8	0.4	717	0.7	0.0	75.0	35	116.6	0.2
1/13/10 16:30	2.6	897	4.8	0.2	2.1	841	3.9	0.2	12.0	794	22.8	1.0	0.4	722	0.7	0.0	58.0	35	88.7	0.2
1/13/10 17:00	4.2	921	7.8	0.4	5.3	862	9.9	0.5	14.0	813	26.7	1.2	0.4	738	0.7	0.0	40.0	36	59.8	0.1
1/13/10 17:30	4.7	929	8.8	0.5	7.8	871	14.7	0.7	10.3	822	19.5	0.9	0.6	749	1.1	0.0	36.0	36	53.5	0.1
1/13/10 18:00	3.5	953	6.5	0.3	10.6	889	20.1	1.0	6.6	835	12.4	0.6	0.4	754	0.7	0.0	28.0	37	40.9	0.1
1/13/10 18:30	2.8	970	5.2	0.3	10.0	900	19.0	1.0	4.3	842	8.0	0.4	0.5	754	0.9	0.0	25.0	37	36.3	0.1
1/13/10 19:00	2.4	986	4.4	0.2	7.4	915	13.9	0.7	2.5	855	4.6	0.2	0.5	765	0.9	0.0	24.0	37	34.8	0.1
1/13/10 19:30	2.6	1003	4.8	0.3	4.4	925	8.2	0.4	3.0	859	5.6	0.3	0.5	760	0.9	0.0	21.0	37	30.2	0.1
1/13/10 20:00	2.0	1012	3.7	0.2	2.5	930	4.6	0.2	2.9	862	5.4	0.3	0.4	760	0.7	0.0	20.0	37	28.6	0.1
1/13/10 20:30	2.9	1020	5.4	0.3	1.7	938	3.1	0.2	2.0	869	3.7	0.2	0.4	765	0.7	0.0	21.0	37	30.2	0.1
1/13/10 21:00	4.3	1029	8.0	0.5	1.6	946	2.9	0.2	2.1	876	3.9	0.2	0.4	771	0.7	0.0	30.0	37	44.0	0.1
1/13/10 21:30	6.9	1039	13.0	0.8	1.5	951	2.7	0.1	1.4	876	2.6	0.1	0.5	765	0.9	0.0	36.0	37	53.5	0.1
1/13/10 22:00	8.5	1048	16.1	0.9	1.2	957	2.2	0.1	1.3	880	2.4	0.1	0.4	765	0.7	0.0	59.0	37	90.3	0.2
1/13/10 22:30	9.0	1048	17.0	1.0	1.3	955	2.4	0.1	1.4	877	2.6	0.1	0.5	760	0.9	0.0	280.0	37	472.3	1.0
1/13/10 23:00	7.8	1039	14.7	0.9	1.2	954	2.2	0.1	1.7	883	3.1	0.2	0.5	776	0.9	0.0	180.0	38	295.4	0.6
1/13/10 23:30	6.2	1048	11.6	0.7	1.1	959	2.0	0.1	1.5	884	2.7	0.1	0.5	771	0.9	0.0	110.0	37	175.1	0.4
1/14/10 0:00	4.2	1058	7.8	0.5	1.0	965	1.8	0.1	1.9	887	3.5	0.2	0.5	771	0.9	0.0	130.0	37	209.1	0.4
1/14/10 0:30	3.0	1067	5.6	0.3	1.2	973	2.2	0.1	3.4	895	6.3	0.3	0.4	776	0.7	0.0	73.0	38	113.3	0.2
1/14/10 1:00	2.5	1039	4.6	0.3	1.0	952	1.8	0.1	5.2	880	9.7	0.5	0.6	771	1.1	0.0	33.0	37	48.7	0.1
1/14/10 1:30	2.4	1058	4.4	0.3	2.0	969	3.7	0.2	4.5	894	8.4	0.4	0.4	782	0.7	0.0	27.0	38	39.4	0.1
1/14/10 2:00	2.2	1058	4.0	0.2	3.7	965	6.9	0.4	4.5	887	8.4	0.4	0.4	771	0.7	0.0	23.0	37	33.2	0.1
1/14/10 2:30	2.1	1058	3.9	0.2	3.8	963	7.1	0.4	3.6	884	6.7	0.3	0.7	765	1.3	0.1	21.0	37	30.2	0.1
1/14/10 3:00	1.9	1058	3.5	0.2	3.9	967	7.3	0.4	1.9	891	3.5	0.2	0.4	776	0.7	0.0	21.0	38	30.2	0.1
1/14/10 3:30	2.1	1067	3.9	0.2	2.9	970	5.4	0.3	2.7	888	5.0	0.2	0.6	765	1.1	0.0	21.0	37	30.2	0.1
1/14/10 4:00	1.9	1067	3.5	0.2	2.0	968	3.7	0.2	1.6	885	2.9	0.1	0.4	760	0.7	0.0	19.0	37	27.1	0.1
1/14/10 4:30	3.1	1058	5.7	0.3	1.8	960	3.3	0.2	1.3	878	2.4	0.1	0.4	754	0.7	0.0	21.0	37	30.2	0.1
1/14/10 5:00	2.1	1058	3.9	0.2	1.4	962	2.6	0.1	1.7	881	3.1	0.2	0.4	760	0.7	0.0	18.0	37	25.6	0.1
1/14/10 5:30	2.4	1058	4.4	0.3	0.9	963	1.6	0.1	1.4	884	2.6	0.1	0.4	765	0.7	0.0	14.0	37	19.6	0.0
1/14/10 6:00	3.4	1058	6.3	0.4	2.0	960	3.7	0.2	1.6	878	2.9	0.1	0.3	754	0.5	0.0	16.0	37	22.6	0.0
1/14/10 6:30	4.0	1048	7.4	0.4	0.7	954	1.3	0.1	1.1	874	2.0	0.1	0.6	754	1.1	0.1	19.0	37	27.1	0.1
1/14/10 7:00	3.9	1067	7.3	0.4	1.0	965	1.8	0.1	1.1	878	2.0	0.1	0.3	749	0.5	0.0	17.0	36	24.1	0.0
1/14/10 7:30	3.4	1048	6.3	0.4	0.9	950	1.6	0.1	1.0	867	1.8	0.1	0.6	744	1.1	0.0	18.0	36	25.6	0.1
1/14/10 8:00	3.2	1039	5.9	0.3	0.9	942	1.6	0.1	1.2	860	2.2	0.1	0.4	738	0.7	0.0	14.0	36	19.6	0.0
1/14/10 8:30	2.5	1039	4.6	0.3	0.7	940	1.3	0.1	1.1	857	2.0	0.1	0.3	733	0.5	0.0	14.0	36	19.6	0.0
1/14/10 9:00	2.2	1029	4.0	0.2	0.6	934	1.1	0.1	1.4	854	2.6	0.1	0.4	733	0.7	0.0	16.0	36	22.6	0.0
1/14/10 9:30	2.0	1039	3.7	0.2	0.6	939	1.1	0.1	1.2	854	2.2	0.1	0.5	728	0.9	0.0	16.0	35	22.6	0.0
1/14/10 10:00	2.1	1020	3.9	0.2	0.6	924	1.1	0.1	1.4	843	2.6	0.1	0.3	722	0.5	0.0	13.0	35	18.1	0.0
1/14/10 10:30	1.6	1039	2.9	0.2	0.7	935	1.3	0.1	0.9	848	1.6	0.1	0.4	717	0.7	0.0	13.0	35	18.1	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/14/10 11:00	3.7	1020	6.9	0.4	0.7	922	1.3	0.1	0.9	840	1.6	0.1	0.3	717	0.5	0.0	14.0	35	19.6	0.0
1/14/10 11:30	2.1	1012	3.9	0.2	0.8	915	1.4	0.1	1.0	834	1.8	0.1	0.3	712	0.5	0.0	14.0	35	19.6	0.0
1/14/10 12:00	1.7	1003	3.1	0.2	0.7	908	1.3	0.1	1.7	827	3.1	0.1	0.3	707	0.5	0.0	14.0	34	19.6	0.0
1/14/10 12:30	1.6	1020	2.9	0.2	0.7	916	1.3	0.1	0.8	828	1.4	0.1	0.3	696	0.5	0.0	12.0	34	16.6	0.0
1/14/10 13:00	1.7	995	3.1	0.2	0.4	899	0.7	0.0	0.9	818	1.6	0.1	0.3	696	0.5	0.0	11.0	34	15.2	0.0
1/14/10 13:30	2.6	995	4.8	0.3	0.3	899	0.5	0.0	1.3	818	2.4	0.1	0.3	696	0.5	0.0	13.0	34	18.1	0.0
1/14/10 14:00	2.4	995	4.4	0.2	0.4	897	0.7	0.0	0.9	815	1.6	0.1	0.3	691	0.5	0.0	12.0	34	16.6	0.0
1/14/10 14:30	1.7	1012	3.1	0.2	0.5	905	0.9	0.0	0.9	815	1.6	0.1	0.3	681	0.5	0.0	11.0	33	15.2	0.0
1/14/10 15:00	1.4	986	2.6	0.1	0.7	888	1.3	0.1	0.9	805	1.6	0.1	0.4	681	0.7	0.0	10.0	33	13.7	0.0
1/14/10 15:30	1.4	978	2.6	0.1	0.3	881	0.5	0.0	0.9	799	1.6	0.1	0.4	676	0.7	0.0	11.0	33	15.2	0.0
1/14/10 16:00	1.8	970	3.3	0.2	0.4	874	0.7	0.0	0.9	792	1.6	0.1	0.5	671	0.9	0.0	11.0	33	15.2	0.0
1/14/10 16:30	1.4	953	2.6	0.1	0.7	864	1.3	0.1	1.1	789	2.0	0.1	0.3	676	0.5	0.0	10.0	33	13.7	0.0
1/14/10 17:00	1.3	970	2.4	0.1	0.6	870	1.1	0.1	1.5	787	2.7	0.1	0.3	661	0.5	0.0	10.0	32	13.7	0.0
1/14/10 17:30	1.5	970	2.7	0.1	0.4	870	0.7	0.0	0.9	787	1.6	0.1	0.3	661	0.5	0.0	11.0	32	15.2	0.0
1/14/10 18:00	1.4	970	2.6	0.1	0.5	870	0.9	0.0	1.0	787	1.8	0.1	0.3	661	0.5	0.0	9.3	32	12.7	0.0
1/14/10 18:30	1.4	970	2.6	0.1	0.8	867	1.4	0.1	1.1	781	2.0	0.1	0.3	651	0.5	0.0	10.0	32	13.7	0.0
1/14/10 19:00	1.4	953	2.6	0.1	0.6	856	1.1	0.1	1.0	774	1.8	0.1	0.4	651	0.7	0.0	11.0	32	15.2	0.0
1/14/10 19:30	1.6	953	2.9	0.2	0.5	854	0.9	0.0	1.0	771	1.8	0.1	0.3	646	0.5	0.0	13.0	32	18.1	0.0
1/14/10 20:00	1.3	945	2.4	0.1	0.4	847	0.7	0.0	0.7	765	1.3	0.1	0.3	641	0.5	0.0	12.0	31	16.6	0.0
1/14/10 20:30	1.4	945	2.6	0.1	0.5	847	0.9	0.0	0.9	765	1.6	0.1	0.4	641	0.7	0.0	12.0	31	16.6	0.0
1/14/10 21:00	1.6	929	2.9	0.2	0.3	835	0.5	0.0	0.9	755	1.6	0.1	0.3	636	0.5	0.0	9.9	31	13.6	0.0
1/14/10 21:30	1.4	921	2.6	0.1	1.0	829	1.8	0.1	1.0	752	1.8	0.1	0.3	636	0.5	0.0	9.2	31	12.6	0.0
1/14/10 22:00	1.4	921	2.6	0.1	0.5	828	0.9	0.0	0.9	749	1.6	0.1	0.4	631	0.7	0.0	9.5	31	13.0	0.0
1/14/10 22:30	1.4	937	2.6	0.1	0.6	836	1.1	0.1	0.9	750	1.6	0.1	0.4	622	0.7	0.0	9.8	31	13.4	0.0
1/14/10 23:00	1.5	913	2.7	0.1	0.3	819	0.5	0.0	1.3	740	2.4	0.1	0.3	622	0.5	0.0	9.1	31	12.4	0.0
1/14/10 23:30	1.8	913	3.3	0.2	0.4	819	0.7	0.0	0.9	740	1.6	0.1	0.5	622	0.9	0.0	9.3	31	12.7	0.0
1/15/10 0:00	1.5	913	2.7	0.1	0.3	819	0.5	0.0	0.9	740	1.6	0.1	0.3	622	0.5	0.0	9.1	31	12.4	0.0
1/15/10 0:30	1.4	905	2.6	0.1	0.3	809	0.5	0.0	0.9	728	1.6	0.1	0.3	607	0.5	0.0	12.0	30	16.6	0.0
1/15/10 1:00	1.4	897	2.6	0.1	0.4	804	0.7	0.0	0.9	725	1.6	0.1	0.3	607	0.5	0.0	8.9	30	12.1	0.0
1/15/10 1:30	1.3	905	2.4	0.1	0.3	811	0.5	0.0	0.9	731	1.6	0.1	0.5	612	0.9	0.0	10.0	30	13.7	0.0
1/15/10 2:00	1.3	890	2.4	0.1	0.7	796	1.3	0.1	0.8	716	1.4	0.1	0.4	598	0.7	0.0	7.9	29	10.7	0.0
1/15/10 2:30	1.5	890	2.7	0.1	0.3	797	0.5	0.0	0.8	719	1.4	0.1	0.3	602	0.5	0.0	9.4	30	12.8	0.0
1/15/10 3:00	1.2	882	2.2	0.1	0.2	790	0.4	0.0	0.8	713	1.4	0.1	0.3	598	0.5	0.0	9.5	29	13.0	0.0
1/15/10 3:30	1.3	897	2.4	0.1	1.0	798	1.8	0.1	0.8	714	1.4	0.1	0.4	588	0.7	0.0	8.8	29	12.0	0.0
1/15/10 4:00	1.4	874	2.6	0.1	0.3	782	0.5	0.0	1.7	705	3.1	0.1	0.3	588	0.5	0.0	8.0	29	10.8	0.0
1/15/10 4:30	1.4	882	2.6	0.1	0.3	787	0.5	0.0	0.7	708	1.3	0.1	0.3	588	0.5	0.0	7.6	29	10.2	0.0
1/15/10 5:00	1.4	874	2.6	0.1	0.5	782	0.9	0.0	0.7	705	1.3	0.1	0.3	588	0.5	0.0	9.3	29	12.7	0.0
1/15/10 5:30	1.4	859	2.6	0.1	0.7	770	1.3	0.1	1.6	696	2.9	0.1	0.3	584	0.5	0.0	7.6	29	10.2	0.0
1/15/10 6:00	1.4	866	2.6	0.1	0.3	772	0.5	0.0	0.7	693	1.3	0.0	0.3	575	0.5	0.0	9.1	28	12.4	0.0
1/15/10 6:30	1.2	859	2.2	0.1	0.1	767	0.2	0.0	0.7	690	1.3	0.0	0.3	575	0.5	0.0	9.0	28	12.3	0.0
1/15/10 7:00	1.4	859	2.6	0.1	0.4	767	0.7	0.0	1.1	690	2.0	0.1	0.4	575	0.7	0.0	11.0	28	15.2	0.0
1/15/10 7:30	1.1	859	2.0	0.1	0.5	764	0.9	0.0	0.9	685	1.6	0.1	0.4	565	0.7	0.0	8.7	28	11.8	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/15/10 8:00	1.4	866	2.6	0.1	0.3	771	0.5	0.0	0.7	690	1.3	0.0	0.3	570	0.5	0.0	11.0	28	15.2	0.0
1/15/10 8:30	1.5	859	2.7	0.1	0.4	764	0.7	0.0	0.8	685	1.4	0.1	0.3	565	0.5	0.0	9.8	28	13.4	0.0
1/15/10 9:00	1.4	851	2.6	0.1	0.1	758	0.2	0.0	0.7	679	1.3	0.0	0.3	561	0.5	0.0	7.9	28	10.7	0.0
1/15/10 9:30	1.2	843	2.2	0.1	1.4	752	2.6	0.1	1.8	676	3.3	0.1	0.4	561	0.7	0.0	8.9	28	12.1	0.0
1/15/10 10:00	1.1	836	2.0	0.1	0.4	746	0.7	0.0	0.7	670	1.3	0.0	0.3	556	0.5	0.0	7.8	27	10.5	0.0
1/15/10 10:30	1.4	843	2.6	0.1	0.2	748	0.4	0.0	1.3	668	2.4	0.1	0.3	547	0.5	0.0	8.5	27	11.5	0.0
1/15/10 11:00	1.4	836	2.6	0.1	0.3	744	0.5	0.0	0.7	667	1.3	0.0	0.4	552	0.7	0.0	12.0	27	16.6	0.0
1/15/10 11:30	1.8	828	3.3	0.2	0.7	738	1.3	0.1	0.6	662	1.1	0.0	0.3	547	0.5	0.0	7.6	27	10.2	0.0
1/15/10 12:00	1.3	821	2.4	0.1	0.4	733	0.7	0.0	0.7	659	1.3	0.0	0.3	547	0.5	0.0	9.2	27	12.6	0.0
1/15/10 12:30	1.4	813	2.6	0.1	0.4	725	0.7	0.0	0.9	650	1.6	0.1	0.3	539	0.5	0.0	9.3	27	12.7	0.0
1/15/10 13:00	1.8	806	3.3	0.1	0.4	723	0.7	0.0	1.0	653	1.8	0.1	0.4	547	0.7	0.0	8.0	27	10.8	0.0
1/15/10 13:30	1.4	821	2.6	0.1	0.2	730	0.4	0.0	0.8	653	1.4	0.1	0.3	539	0.5	0.0	8.9	27	12.1	0.0
1/15/10 14:00	1.1	821	2.0	0.1	0.3	728	0.5	0.0	0.6	651	1.1	0.0	0.3	534	0.5	0.0	9.5	26	13.0	0.0
1/15/10 14:30	1.3	806	2.4	0.1	0.3	717	0.5	0.0	1.0	642	1.8	0.1	0.3	530	0.5	0.0	8.3	26	11.3	0.0
1/15/10 15:00	1.4	806	2.6	0.1	0.3	717	0.5	0.0	0.7	642	1.3	0.0	0.3	530	0.5	0.0	10.0	26	13.7	0.0
1/15/10 15:30	1.3	813	2.4	0.1	0.6	722	1.1	0.0	0.7	645	1.3	0.0	0.3	530	0.5	0.0	8.1	26	11.0	0.0
1/15/10 16:00	1.4	821	2.6	0.1	0.4	728	0.7	0.0	0.8	651	1.4	0.1	0.3	534	0.5	0.0	9.3	26	12.7	0.0
1/15/10 16:30	1.4	806	2.6	0.1	0.7	723	1.3	0.1	0.7	653	1.3	0.0	0.4	547	0.7	0.0	8.4	27	11.4	0.0
1/15/10 17:00	1.4	813	2.6	0.1	0.4	726	0.7	0.0	0.7	653	1.3	0.0	0.4	543	0.7	0.0	8.4	27	11.4	0.0
1/15/10 17:30	1.6	806	2.9	0.1	0.5	724	0.9	0.0	1.1	655	2.0	0.1	0.4	552	0.7	0.0	18.0	27	25.6	0.0
1/15/10 18:00	1.8	821	3.3	0.2	0.5	736	0.9	0.0	0.9	664	1.6	0.1	0.3	556	0.5	0.0	57.0	27	87.1	0.1
1/15/10 18:30	1.9	806	3.5	0.2	0.4	727	0.7	0.0	1.2	661	2.2	0.1	0.3	561	0.5	0.0	50.0	28	75.8	0.1
1/15/10 19:00	1.3	836	2.4	0.1	0.4	747	0.7	0.0	0.9	673	1.6	0.1	0.3	575	0.5	0.0	55.0	28	83.9	0.1
1/15/10 19:30	1.5	828	2.7	0.1	0.4	747	0.7	0.0	0.7	678	1.3	0.0	0.3	584	0.5	0.0	53.0	28	80.6	0.1
1/15/10 20:00	1.7	828	3.1	0.1	0.5	750	0.9	0.0	1.0	683	1.8	0.1	0.3	584	0.5	0.0	59.0	29	90.3	0.1
1/15/10 20:30	1.5	843	2.7	0.1	0.5	763	0.9	0.0	1.8	695	3.3	0.1	0.4	593	0.7	0.0	37.0	29	55.0	0.1
1/15/10 21:00	1.5	859	2.7	0.1	0.6	775	1.1	0.0	2.2	704	4.0	0.2	0.5	598	0.9	0.0	32.0	29	47.2	0.1
1/15/10 21:30	1.7	859	3.1	0.2	0.9	779	1.6	0.1	2.5	712	4.6	0.2	0.4	612	0.7	0.0	88.0	30	138.1	0.2
1/15/10 22:00	1.8	866	3.3	0.2	1.2	787	2.2	0.1	2.2	721	4.0	0.2	0.3	622	0.5	0.0	240.0	31	401.0	0.7
1/15/10 22:30	1.6	882	2.9	0.1	1.5	800	2.7	0.1	2.4	730	4.4	0.2	0.4	626	0.7	0.0	260.0	31	436.5	0.8
1/15/10 23:00	2.5	874	4.6	0.2	1.5	799	2.7	0.1	1.9	736	3.5	0.1	0.4	641	0.7	0.0	290.0	31	490.2	0.9
1/15/10 23:30	1.7	897	3.1	0.2	2.3	821	4.2	0.2	1.8	757	3.3	0.1	0.4	661	0.7	0.0	230.0	32	383.2	0.7
1/16/10 0:00	1.9	921	3.5	0.2	2.0	842	3.7	0.2	3.4	776	6.3	0.3	0.4	676	0.7	0.0	180.0	33	295.4	0.5
1/16/10 0:30	2.4	937	4.4	0.2	1.4	863	2.6	0.1	5.6	800	10.5	0.5	0.4	707	0.7	0.0	260.0	34	436.5	0.8
1/16/10 1:00	1.9	962	3.5	0.2	2.0	888	3.7	0.2	7.7	826	14.5	0.7	0.6	733	1.1	0.0	340.0	36	580.4	1.2
1/16/10 1:30	2.1	970	3.9	0.2	3.9	900	7.3	0.4	8.1	842	15.3	0.7	0.9	754	1.6	0.1	280.0	37	472.3	1.0
1/16/10 2:00	2.5	1003	4.6	0.3	5.6	941	10.5	0.6	7.5	888	14.1	0.7	0.5	810	0.9	0.0	170.0	39	278.0	0.6
1/16/10 2:30	2.7	1029	5.0	0.3	6.6	971	12.4	0.7	7.2	923	13.6	0.7	0.8	850	1.4	0.1	450.0	41	781.7	1.8
1/16/10 3:00	3.1	1058	5.7	0.3	6.9	1006	13.0	0.7	10.8	962	20.5	1.1	0.6	897	1.1	0.1	320.0	43	544.2	1.3
1/16/10 3:30	3.2	1096	5.9	0.4	8.7	1046	16.4	1.0	11.6	1003	22.1	1.2	0.5	940	0.9	0.0	330.0	45	562.3	1.4
1/16/10 4:00	3.4	1125	6.3	0.4	7.8	1082	14.7	0.9	8.0	1045	15.1	0.9	0.5	990	0.9	0.0	190.0	47	312.9	0.8
1/16/10 4:30	3.5	1185	6.5	0.4	8.7	1129	16.4	1.0	11.5	1081	21.9	1.3	0.5	1009	0.9	0.1	250.0	48	418.7	1.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/16/10 5:00	3.7	1258	6.9	0.5	7.8	1191	14.7	1.0	10.7	1134	20.3	1.3	0.7	1048	1.3	0.1	300.0	50	508.2	1.4
1/16/10 5:30	5.3	1301	9.9	0.7	10.4	1217	19.7	1.3	9.8	1147	18.6	1.2	1.2	1041	2.2	0.1	250.0	50	418.7	1.2
1/16/10 6:00	6.8	1389	12.8	1.0	10.9	1292	20.7	1.5	7.1	1211	13.4	0.9	0.7	1088	1.3	0.1	260.0	52	436.5	1.3
1/16/10 6:30	8.0	1424	15.1	1.2	9.1	1313	17.2	1.3	9.4	1221	17.8	1.2	0.7	1081	1.3	0.1	290.0	51	490.2	1.4
1/16/10 7:00	8.0	1482	15.1	1.3	6.9	1357	13.0	1.0	9.0	1252	17.0	1.2	0.8	1095	1.4	0.1	290.0	52	490.2	1.4
1/16/10 7:30	9.0	1542	17.0	1.5	8.0	1398	15.1	1.2	7.4	1277	13.9	1.0	0.5	1095	0.9	0.1	220.0	52	365.6	1.1
1/16/10 8:00	9.9	1567	18.8	1.7	7.6	1415	14.3	1.1	9.2	1287	17.4	1.3	0.7	1095	1.3	0.1	270.0	52	454.4	1.3
1/16/10 8:30	9.4	1579	17.8	1.6	7.0	1425	13.2	1.1	7.6	1296	14.3	1.0	0.6	1102	1.1	0.1	110.0	52	175.1	0.5
1/16/10 9:00	11.0	1654	20.9	1.9	8.7	1476	16.4	1.4	8.5	1326	16.1	1.2	0.6	1102	1.1	0.1	64.0	52	98.5	0.3
1/16/10 9:30	10.0	1616	19.0	1.7	7.3	1451	13.7	1.1	11.6	1311	22.1	1.6	0.5	1102	0.9	0.1	120.0	52	192.0	0.6
1/16/10 10:00	8.7	1604	16.4	1.5	8.0	1440	15.1	1.2	7.9	1302	14.9	1.1	0.6	1095	1.1	0.1	120.0	52	192.0	0.6
1/16/10 10:30	8.4	1642	15.9	1.5	10.4	1470	19.7	1.6	4.5	1325	8.4	0.6	0.6	1108	1.1	0.1	86.0	53	134.8	0.4
1/16/10 11:00	8.7	1642	16.4	1.5	6.3	1459	11.8	1.0	3.7	1305	6.9	0.5	0.6	1075	1.1	0.1	67.0	51	103.4	0.3
1/16/10 11:30	8.6	1680	16.3	1.5	8.2	1485	15.4	1.3	4.3	1321	8.0	0.6	0.5	1075	0.9	0.1	54.0	51	82.2	0.2
1/16/10 12:00	8.0	1654	15.1	1.4	10.0	1468	19.0	1.6	4.2	1310	7.8	0.6	0.4	1075	0.7	0.0	89.0	51	139.8	0.4
1/16/10 12:30	8.3	1654	15.7	1.5	11.9	1466	22.6	1.9	5.7	1306	10.7	0.8	0.5	1068	0.9	0.1	60.0	51	92.0	0.3
1/16/10 13:00	8.2	1616	15.5	1.4	4.5	1440	8.4	0.7	2.9	1291	5.4	0.4	0.7	1068	1.3	0.1	38.0	51	56.6	0.2
1/16/10 13:30	7.9	1616	14.9	1.4	3.4	1438	6.3	0.5	2.8	1287	5.2	0.4	0.4	1061	0.7	0.0	42.0	50	63.0	0.2
1/16/10 14:00	8.2	1654	15.5	1.4	3.2	1463	5.9	0.5	2.7	1303	5.0	0.4	0.6	1061	1.1	0.1	38.0	50	56.6	0.2
1/16/10 14:30	6.4	1667	12.0	1.1	2.8	1466	5.2	0.4	2.4	1296	4.4	0.3	0.5	1041	0.9	0.1	150.0	50	243.4	0.7
1/16/10 15:00	5.0	1616	9.3	0.8	2.9	1433	5.4	0.4	2.4	1279	4.4	0.3	0.5	1048	0.9	0.1	180.0	50	295.4	0.8
1/16/10 15:30	4.2	1642	7.8	0.7	3.4	1455	6.3	0.5	1.7	1297	3.1	0.2	0.7	1061	1.3	0.1	160.0	50	260.7	0.7
1/16/10 16:00	4.6	1654	8.6	0.8	4.8	1455	9.0	0.7	3.0	1287	5.6	0.4	0.4	1035	0.7	0.0	200.0	49	330.4	0.9
1/16/10 16:30	4.6	1604	8.6	0.8	2.4	1425	4.4	0.4	4.0	1274	7.4	0.5	0.5	1048	0.9	0.1	320.0	50	544.2	1.5
1/16/10 17:00	4.5	1629	8.4	0.8	3.4	1442	6.3	0.5	4.5	1284	8.4	0.6	0.4	1048	0.7	0.0	220.0	50	365.6	1.0
1/16/10 17:30	3.9	1616	7.3	0.7	4.1	1429	7.6	0.6	5.7	1271	10.7	0.8	0.5	1035	0.9	0.1	78.0	49	121.5	0.3
1/16/10 18:00	4.4	1604	8.2	0.7	6.1	1423	11.4	0.9	7.1	1270	13.4	1.0	0.4	1041	0.7	0.0	120.0	50	192.0	0.5
1/16/10 18:30	4.2	1604	7.8	0.7	6.4	1423	12.0	1.0	9.2	1270	17.4	1.2	0.5	1041	0.9	0.1	290.0	50	490.2	1.4
1/16/10 19:00	3.2	1604	5.9	0.5	8.5	1423	16.1	1.3	6.6	1270	12.4	0.9	0.5	1041	0.9	0.1	110.0	50	175.1	0.5
1/16/10 19:30	2.8	1567	5.2	0.5	9.1	1400	17.2	1.4	3.8	1259	7.1	0.5	0.5	1048	0.9	0.1	66.0	50	101.8	0.3
1/16/10 20:00	2.9	1591	5.4	0.5	7.0	1416	13.2	1.0	5.3	1269	9.9	0.7	0.7	1048	0.9	0.1	180.0	50	295.4	0.8
1/16/10 20:30	3.7	1567	6.9	0.6	4.2	1398	7.8	0.6	7.3	1255	13.7	1.0	0.7	1041	1.3	0.1	69.0	50	106.7	0.3
1/16/10 21:00	4.3	1604	8.0	0.7	5.7	1427	10.7	0.9	4.5	1278	8.4	0.6	0.4	1055	0.7	0.0	50.0	50	75.8	0.2
1/16/10 21:30	5.3	1616	9.9	0.9	7.2	1436	13.6	1.1	3.7	1283	6.9	0.5	0.5	1055	0.9	0.1	180.0	50	295.4	0.8
1/16/10 22:00	5.6	1604	10.5	0.9	5.1	1425	9.5	0.8	5.0	1274	9.3	0.7	0.4	1048	0.7	0.0	54.0	50	82.2	0.2
1/16/10 22:30	7.2	1591	13.6	1.2	4.0	1414	7.4	0.6	3.2	1265	5.9	0.4	0.5	1041	0.9	0.1	50.0	50	75.8	0.2
1/16/10 23:00	6.9	1591	13.0	1.2	5.5	1416	10.3	0.8	3.5	1269	6.5	0.5	0.6	1048	1.1	0.1	42.0	50	63.0	0.2
1/16/10 23:30	5.8	1591	10.9	1.0	3.4	1421	6.3	0.5	5.0	1277	9.3	0.7	0.5	1061	0.9	0.1	28.0	50	40.9	0.1
1/17/10 0:00	4.6	1567	8.6	0.8	3.8	1402	7.1	0.6	3.2	1263	5.9	0.4	0.5	1055	0.9	0.1	34.0	50	50.3	0.1
1/17/10 0:30	5.4	1604	10.1	0.9	4.7	1425	8.8	0.7	2.6	1274	4.8	0.3	0.5	1048	0.9	0.1	34.0	50	50.3	0.1
1/17/10 1:00	5.5	1579	10.3	0.9	3.2	1410	5.9	0.5	2.2	1268	4.0	0.3	0.5	1055	0.9	0.1	34.0	50	50.3	0.1
1/17/10 1:30	4.5	1567	8.4	0.7	3.1	1395	5.7	0.5	1.8	1251	3.3	0.2	0.5	1035	0.9	0.1	26.0	49	37.8	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/17/10 2:00	4.7	1579	8.8	0.8	2.5	1408	4.6	0.4	2.3	1264	4.2	0.3	0.6	1048	1.1	0.1	27.0	50	39.4	0.1
1/17/10 2:30	5.1	1604	9.5	0.9	3.5	1421	6.5	0.5	2.0	1266	3.7	0.3	0.3	1035	0.5	0.0	52.0	49	79.0	0.2
1/17/10 3:00	3.9	1567	7.3	0.6	2.3	1395	4.2	0.3	1.8	1251	3.3	0.2	0.4	1035	0.7	0.0	40.0	49	59.8	0.2
1/17/10 3:30	4.5	1579	8.4	0.7	4.1	1404	7.6	0.6	1.7	1256	3.1	0.2	0.4	1035	0.7	0.0	60.0	49	92.0	0.3
1/17/10 4:00	4.2	1554	7.8	0.7	2.5	1387	4.6	0.4	1.8	1246	3.3	0.2	0.5	1035	0.9	0.1	61.0	49	93.6	0.3
1/17/10 4:30	4.0	1579	7.4	0.7	1.7	1404	3.1	0.2	2.1	1256	3.9	0.3	0.6	1035	1.1	0.1	120.0	49	192.0	0.5
1/17/10 5:00	3.4	1567	6.3	0.6	1.9	1398	3.5	0.3	2.9	1255	5.4	0.4	0.4	1041	0.7	0.0	280.0	50	472.3	1.3
1/17/10 5:30	3.3	1554	6.1	0.5	2.5	1381	4.6	0.4	2.5	1235	4.6	0.3	0.4	1015	0.7	0.0	84.0	48	131.5	0.4
1/17/10 6:00	3.0	1542	5.6	0.5	2.5	1377	4.6	0.4	3.0	1237	5.6	0.4	0.4	1028	0.7	0.0	40.0	49	59.8	0.2
1/17/10 6:30	3.2	1554	5.9	0.5	3.3	1389	6.1	0.5	5.1	1250	9.5	0.7	0.4	1041	0.7	0.0	50.0	50	75.8	0.2
1/17/10 7:00	2.8	1579	5.2	0.5	3.7	1406	6.9	0.5	8.5	1260	16.1	1.1	0.4	1041	0.7	0.0	190.0	50	312.9	0.9
1/17/10 7:30	3.0	1554	5.6	0.5	6.9	1393	13.0	1.0	4.3	1258	8.0	0.6	0.5	1055	0.9	0.1	210.0	50	347.9	1.0
1/17/10 8:00	2.5	1579	4.6	0.4	7.5	1410	14.1	1.1	2.9	1268	5.4	0.4	0.5	1055	0.9	0.1	170.0	50	278.0	0.8
1/17/10 8:30	3.0	1579	5.6	0.5	5.0	1412	9.3	0.7	3.8	1272	7.1	0.5	0.5	1061	0.9	0.1	120.0	50	192.0	0.5
1/17/10 9:00	3.1	1591	5.7	0.5	2.9	1425	5.4	0.4	6.2	1285	11.6	0.8	0.5	1075	0.9	0.1	88.0	51	138.1	0.4
1/17/10 9:30	3.5	1604	6.5	0.6	3.9	1438	7.3	0.6	6.9	1298	13.0	0.9	0.4	1088	0.7	0.0	100.0	52	158.2	0.5
1/17/10 10:00	3.5	1591	6.5	0.6	6.4	1429	12.0	1.0	5.4	1293	10.1	0.7	0.4	1088	0.7	0.0	80.0	52	124.8	0.4
1/17/10 10:30	4.2	1604	7.8	0.7	7.1	1438	13.4	1.1	4.6	1298	8.6	0.6	0.4	1088	0.7	0.0	55.0	52	83.9	0.2
1/17/10 11:00	5.6	1591	10.5	0.9	6.0	1434	11.3	0.9	4.4	1301	8.2	0.6	0.5	1102	0.9	0.1	40.0	52	59.8	0.2
1/17/10 11:30	6.3	1616	11.8	1.1	5.7	1451	10.7	0.9	3.7	1311	6.9	0.5	0.5	1102	0.9	0.1	35.0	52	51.9	0.2
1/17/10 12:00	4.5	1629	8.4	0.8	4.9	1459	9.2	0.8	3.2	1316	5.9	0.4	0.4	1102	0.7	0.0	30.0	52	44.0	0.1
1/17/10 12:30	4.1	1616	7.6	0.7	4.3	1455	8.0	0.7	2.7	1319	5.0	0.4	0.4	1115	0.7	0.0	45.0	53	67.8	0.2
1/17/10 13:00	4.5	1654	8.4	0.8	3.7	1479	6.9	0.6	2.1	1330	3.9	0.3	0.4	1108	0.7	0.0	46.0	53	69.4	0.2
1/17/10 13:30	5.7	1654	10.7	1.0	2.9	1479	5.4	0.4	1.9	1330	3.5	0.3	0.4	1108	0.7	0.0	30.0	53	44.0	0.1
1/17/10 14:00	6.1	1667	11.4	1.1	2.8	1487	5.2	0.4	1.9	1336	3.5	0.3	0.4	1108	0.7	0.0	35.0	53	51.9	0.2
1/17/10 14:30	5.8	1629	10.9	1.0	3.2	1464	5.9	0.5	2.9	1324	5.4	0.4	0.5	1115	0.9	0.1	45.0	53	67.8	0.2
1/17/10 15:00	4.8	1654	9.0	0.8	2.6	1476	4.8	0.4	2.4	1326	4.4	0.3	0.5	1102	0.9	0.1	210.0	52	347.9	1.0
1/17/10 15:30	5.5	1642	10.3	1.0	3.1	1468	5.7	0.5	2.0	1321	3.7	0.3	0.5	1102	0.9	0.1	67.0	52	103.4	0.3
1/17/10 16:00	4.4	1654	8.2	0.8	2.6	1476	4.8	0.4	1.9	1326	3.5	0.3	0.5	1102	0.9	0.1	33.0	52	48.7	0.1
1/17/10 16:30	3.9	1642	7.3	0.7	2.3	1463	4.2	0.3	3.7	1313	6.9	0.5	0.6	1088	1.1	0.1	26.0	52	37.8	0.1
1/17/10 17:00	3.6	1680	6.7	0.6	2.1	1496	3.9	0.3	5.4	1341	10.1	0.8	0.4	1108	0.7	0.0	27.0	53	39.4	0.1
1/17/10 18:00	3.3	1667	6.1	0.6	4.4	1487	8.2	0.7	3.8	1336	7.1	0.5	0.4	1108	0.7	0.0	30.0	53	44.0	0.1
1/17/10 18:30	3.4	1667	6.3	0.6	6.2	1489	11.6	1.0	2.4	1340	4.4	0.3	0.4	1115	0.7	0.0	62.0	53	95.2	0.3
1/17/10 19:00	3.2	1629	5.9	0.5	2.1	1468	3.9	0.3	1.9	1340	3.5	0.3	0.7	1115	1.3	0.1	62.0	53	95.2	0.3
1/17/10 19:30	3.7	1667	6.9	0.6	2.3	1498	4.2	0.4	2.0	1356	3.7	0.3	0.4	1143	0.7	0.0	230.0	54	383.2	1.2
1/17/10 20:00	3.3	1667	6.1	0.6	2.1	1498	3.9	0.3	3.3	1356	6.1	0.5	0.5	1136	0.7	0.0	62.0	54	95.2	0.3
1/17/10 20:30	3.9	1680	7.3	0.7	3.1	1505	5.7	0.5	3.8	1357	7.1	0.5	0.4	1136	0.7	0.0	62.0	54	95.2	0.3
1/17/10 21:00	4.5	1629	8.4	0.8	5.0	1470	9.3	0.8	4.4	1336	8.2	0.6	0.8	1136	1.4	0.1	110.0	54	175.1	0.5
1/17/10 21:30	4.6	1642	8.6	0.8	5.0	1479	9.3	0.8	2.7	1342	5.0	0.4	0.5	1136	0.9	0.1	33.0	54	48.7	0.1
1/17/10 22:00	3.8	1654	7.1	0.7	4.8	1487	9.0	0.7	3.8	1347	7.1	0.5	0.4	1136	0.7	0.0	26.0	54	37.8	0.1
1/17/10 22:30	3.4	1642	6.3	0.6	3.0	1479	5.6	0.5	3.0	1342	5.6	0.4	0.4	1136	0.7	0.0	21.0	54	30.2	0.1
																	17.0	54	24.1	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/17/10 23:00	3.1	1680	5.7	0.5	4.4	1500	8.2	0.7	2.4	1349	4.4	0.3	0.6	1122	1.1	0.1	13.0	53	18.1	0.1
1/17/10 23:30	3.1	1693	5.7	0.5	3.6	1509	6.7	0.6	1.7	1354	3.1	0.2	1.6	1122	2.9	0.2	19.0	53	27.1	0.1
1/18/10 0:00	3.1	1654	5.7	0.5	2.1	1479	3.9	0.3	1.6	1330	2.9	0.2	0.5	1108	0.9	0.1	15.0	53	21.1	0.1
1/18/10 0:30	3.7	1629	6.9	0.6	2.4	1464	4.4	0.4	1.3	1324	2.4	0.2	0.7	1115	1.3	0.1	16.0	53	22.6	0.1
1/18/10 1:00	4.5	1642	8.4	0.8	1.6	1468	2.9	0.2	1.3	1321	2.4	0.2	0.6	1102	1.1	0.1	14.0	52	19.6	0.1
1/18/10 1:30	4.2	1629	7.8	0.7	2.8	1455	5.2	0.4	1.3	1308	2.4	0.2	0.5	1088	0.9	0.1	14.0	52	19.6	0.1
1/18/10 2:00	6.6	1642	12.4	1.1	1.6	1466	2.9	0.2	1.9	1317	3.5	0.3	0.6	1095	1.1	0.1	14.0	52	19.6	0.1
1/18/10 2:30	4.1	1654	7.6	0.7	2.3	1468	4.2	0.3	1.5	1310	2.7	0.2	0.6	1075	1.1	0.1	13.0	51	18.1	0.1
1/18/10 3:00	3.8	1642	7.1	0.7	1.8	1455	3.3	0.3	1.3	1297	2.4	0.2	0.4	1061	0.7	0.0	16.0	50	22.6	0.1
1/18/10 3:30	3.1	1604	5.7	0.5	1.4	1429	2.6	0.2	1.3	1282	2.4	0.2	0.4	1061	0.7	0.0	13.0	50	18.1	0.1
1/18/10 4:00	2.7	1604	5.0	0.4	1.5	1421	2.7	0.2	1.4	1266	2.6	0.2	0.4	1035	0.7	0.0	14.0	49	19.6	0.1
1/18/10 4:30	2.4	1604	4.4	0.4	1.4	1423	2.6	0.2	1.1	1270	2.0	0.1	0.5	1041	0.9	0.1	12.0	50	16.6	0.0
1/18/10 5:00	2.5	1591	4.6	0.4	1.4	1412	2.6	0.2	1.1	1261	2.0	0.1	0.5	1035	0.9	0.1	12.0	49	16.6	0.0
1/18/10 5:30	2.4	1579	4.4	0.4	1.5	1402	2.7	0.2	1.1	1252	2.0	0.1	0.3	1028	0.5	0.0	9.6	49	13.1	0.0
1/18/10 6:00	2.7	1554	5.0	0.4	1.8	1381	3.3	0.3	1.2	1235	2.2	0.2	0.4	1015	0.7	0.0	12.0	48	16.6	0.0
1/18/10 6:30	2.4	1542	4.4	0.4	1.2	1373	2.2	0.2	1.2	1230	2.2	0.2	0.6	1015	1.1	0.1	12.0	48	16.6	0.0
1/18/10 7:00	2.4	1530	4.4	0.4	1.5	1362	2.7	0.2	1.2	1221	2.2	0.1	0.4	1009	0.7	0.0	12.0	48	16.6	0.0
1/18/10 7:30	2.7	1554	5.0	0.4	1.5	1375	2.7	0.2	1.1	1223	2.0	0.1	0.4	996	0.7	0.0	11.0	48	15.2	0.0
1/18/10 8:00	2.4	1494	4.4	0.4	1.4	1332	2.6	0.2	1.4	1195	2.6	0.2	0.4	990	0.7	0.0	10.0	47	13.7	0.0
1/18/10 8:30	2.2	1494	4.0	0.3	1.4	1325	2.6	0.2	1.8	1184	3.3	0.2	0.5	971	0.9	0.0	11.0	46	15.2	0.0
1/18/10 9:00	2.0	1518	3.7	0.3	1.5	1342	2.7	0.2	1.4	1193	2.6	0.2	0.4	971	0.7	0.0	12.0	46	16.6	0.0
1/18/10 9:30	2.0	1494	3.7	0.3	5.5	1321	10.3	0.8	1.1	1176	2.0	0.1	0.4	958	0.7	0.0	12.0	46	16.6	0.0
1/18/10 10:00	3.1	1494	5.7	0.5	1.2	1323	2.2	0.2	1.0	1180	1.8	0.1	0.7	964	1.3	0.1	11.0	46	15.2	0.0
1/18/10 10:30	2.5	1458	4.6	0.4	1.0	1295	1.8	0.1	1.3	1158	2.4	0.2	0.4	952	0.7	0.0	10.0	46	13.7	0.0
1/18/10 11:00	2.5	1447	4.6	0.4	1.2	1283	2.1	0.2	1.0	1146	1.8	0.1	0.4	940	0.7	0.0	14.0	45	19.6	0.0
1/18/10 11:30	2.7	1470	5.0	0.4	1.3	1297	2.4	0.2	1.0	1152	1.8	0.1	0.5	933	0.9	0.0	11.0	45	15.2	0.0
1/18/10 12:00	2.3	1447	4.2	0.3	5.3	1279	9.9	0.7	1.1	1139	2.0	0.1	0.4	927	0.7	0.0	11.0	44	15.2	0.0
1/18/10 12:30	1.8	1470	3.3	0.3	1.2	1291	2.2	0.2	1.1	1141	2.0	0.1	0.4	915	0.7	0.0	13.0	44	18.1	0.0
1/18/10 13:00	2.1	1435	3.9	0.3	1.4	1268	2.6	0.2	0.9	1127	1.6	0.1	0.4	915	0.7	0.0	14.0	44	19.6	0.0
1/18/10 13:30	2.0	1401	3.7	0.3	1.2	1242	2.2	0.2	1.1	1109	2.0	0.1	0.4	909	0.7	0.0	13.0	44	18.1	0.0
1/18/10 14:00	1.9	1401	3.5	0.3	1.7	1240	3.1	0.2	1.1	1105	2.0	0.1	0.4	903	0.7	0.0	11.0	43	15.2	0.0
1/18/10 15:00	2.2	1389	4.0	0.3	1.4	1225	2.6	0.2	1.2	1087	2.2	0.1	0.4	879	0.7	0.0	9.7	43	13.3	0.0
1/18/10 15:30	1.8	1389	3.3	0.3	2.9	1223	5.4	0.4	1.6	1083	2.9	0.2	0.5	873	0.9	0.0	12.0	42	16.6	0.0
1/18/10 16:00	2.3	1378	4.2	0.3	1.2	1212	2.2	0.1	1.1	1072	2.0	0.1	0.6	861	1.1	0.1	10.0	41	13.7	0.0
1/18/10 16:30	2.5	1389	4.6	0.4	1.0	1221	1.8	0.1	1.1	1080	2.0	0.1	0.3	867	0.5	0.0	9.1	42	12.4	0.0
1/18/10 17:00	2.2	1356	4.0	0.3	0.9	1199	1.6	0.1	0.9	1066	1.6	0.1	0.4	867	0.7	0.0	10.0	42	13.7	0.0
1/18/10 17:30	2.4	1367	4.4	0.3	1.0	1202	1.8	0.1	1.0	1064	1.8	0.1	0.4	856	0.7	0.0	8.8	41	12.0	0.0
1/18/10 18:00	2.1	1323	3.9	0.3	1.9	1167	3.5	0.2	1.0	1035	1.8	0.1	0.4	838	0.7	0.0	7.7	40	10.4	0.0
1/18/10 18:30	2.0	1323	3.7	0.3	0.7	1165	1.3	0.1	1.1	1032	2.0	0.1	0.3	832	0.5	0.0	8.0	40	10.8	0.0
1/18/10 19:00	2.5	1323	4.6	0.3	0.9	1165	1.6	0.1	0.9	1032	1.6	0.1	0.4	832	0.7	0.0	7.4	40	10.0	0.0
1/18/10 19:30	2.2	1312	4.0	0.3	0.9	1156	1.6	0.1	1.9	1024	3.5	0.2	0.4	827	0.7	0.0	11.0	40	15.2	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/18/10 20:00	2.5	1280	4.6	0.3	1.2	1132	2.2	0.1	1.0	1008	1.8	0.1	0.5	821	0.9	0.0	10.0	40	13.7	0.0
1/18/10 20:30	1.9	1290	3.5	0.3	1.2	1135	2.2	0.1	1.1	1005	2.0	0.1	0.4	810	0.7	0.0	8.4	39	11.4	0.0
1/18/10 21:00	2.1	1280	3.9	0.3	0.9	1128	1.6	0.1	0.9	1001	1.6	0.1	0.4	810	0.7	0.0	9.1	39	12.4	0.0
1/18/10 21:30	1.9	1269	3.5	0.2	0.7	1117	1.3	0.1	1.0	990	1.8	0.1	0.3	798	0.5	0.0	7.4	39	10.0	0.0
1/18/10 22:00	2.1	1258	3.9	0.3	0.9	1107	1.6	0.1	1.0	979	1.8	0.1	0.4	787	0.7	0.0	8.2	38	11.1	0.0
1/18/10 22:30	1.9	1227	3.5	0.2	0.9	1085	1.6	0.1	0.9	966	1.6	0.1	0.3	787	0.5	0.0	7.9	38	10.7	0.0
1/18/10 23:00	2.0	1237	3.7	0.3	1.3	1091	2.4	0.1	1.0	967	1.8	0.1	0.3	782	0.5	0.0	6.4	38	8.5	0.0
1/18/10 23:30	1.9	1227	3.5	0.2	1.3	1082	2.4	0.1	1.0	959	1.8	0.1	0.3	776	0.5	0.0	6.6	38	8.8	0.0
1/19/10 00:00	2.1	1206	3.9	0.3	1.1	1064	2.0	0.1	1.1	945	2.0	0.1	0.4	765	0.7	0.0	6.2	37	8.3	0.0
1/19/10 0:30	1.9	1237	3.5	0.2	0.9	1085	1.6	0.1	0.9	957	1.6	0.1	0.4	765	0.7	0.0	7.3	37	9.8	0.0
1/19/10 1:00	2.0	1216	3.7	0.3	0.9	1069	1.6	0.1	1.0	946	1.8	0.1	0.4	760	0.7	0.0	5.7	37	7.5	0.0
1/19/10 1:30	1.9	1206	3.5	0.2	1.1	1059	2.0	0.1	1.1	935	2.0	0.1	0.4	749	0.7	0.0	7.1	36	9.5	0.0
1/19/10 2:00	1.8	1185	3.3	0.2	1.1	1047	2.0	0.1	1.0	930	1.8	0.1	0.5	754	0.9	0.0	5.6	37	7.4	0.0
1/19/10 2:30	2.2	1165	4.0	0.3	0.9	1029	1.6	0.1	0.9	915	1.6	0.1	0.3	744	0.5	0.0	6.0	36	8.0	0.0
1/19/10 3:00	2.6	1175	4.8	0.3	0.9	1036	1.6	0.1	0.9	919	1.6	0.1	0.3	744	0.5	0.0	6.7	36	9.0	0.0
1/19/10 3:30	2.0	1196	3.7	0.2	1.0	1047	1.8	0.1	0.9	921	1.6	0.1	0.4	733	0.7	0.0	5.8	36	7.7	0.0
1/19/10 4:00	2.9	1196	5.4	0.4	1.5	1043	2.7	0.2	0.7	915	1.3	0.1	0.3	722	0.5	0.0	6.3	35	8.4	0.0
1/19/10 4:30	2.0	1155	3.7	0.2	1.0	1014	1.8	0.1	0.8	895	1.4	0.1	0.4	717	0.7	0.0	5.9	35	7.8	0.0
1/19/10 5:00	2.3	1165	4.2	0.3	1.1	1021	2.0	0.1	1.1	899	2.0	0.1	0.4	717	0.7	0.0	5.2	35	6.8	0.0
1/19/10 5:30	2.0	1155	3.7	0.2	1.0	1011	1.8	0.1	0.7	889	1.3	0.1	0.4	707	0.7	0.0	4.0	34	5.2	0.0
1/19/10 6:00	1.9	1125	3.5	0.2	1.0	989	1.8	0.1	0.9	874	1.6	0.1	0.3	702	0.5	0.0	3.8	34	4.9	0.0
1/19/10 6:30	1.8	1115	3.3	0.2	0.7	980	1.3	0.1	1.0	867	1.8	0.1	0.4	696	0.7	0.0	4.6	34	6.0	0.0
1/19/10 7:00	2.3	1135	4.2	0.3	0.8	994	1.4	0.1	0.9	875	1.6	0.1	0.3	691	0.5	0.0	4.2	34	5.5	0.0
1/19/10 7:30	2.0	1096	3.7	0.2	2.2	966	4.0	0.2	1.0	856	1.8	0.1	0.3	691	0.5	0.0	5.1	34	6.7	0.0
1/19/10 8:00	2.1	1096	3.9	0.2	0.7	964	1.3	0.1	0.9	853	1.6	0.1	0.3	686	0.5	0.0	4.2	33	5.5	0.0
1/19/10 8:30	2.0	1106	3.7	0.2	1.7	969	3.1	0.2	0.7	854	1.3	0.1	0.4	681	0.7	0.0	3.8	33	4.9	0.0
1/19/10 9:00	1.9	1115	3.5	0.2	0.7	974	1.3	0.1	0.7	855	1.3	0.1	0.3	676	0.5	0.0	3.7	33	4.8	0.0
1/19/10 9:30	2.2	1086	4.0	0.2	0.8	954	1.4	0.1	0.6	843	1.1	0.1	0.3	676	0.5	0.0	3.3	33	4.2	0.0
1/19/10 10:00	1.8	1096	3.3	0.2	0.6	956	1.1	0.1	0.7	838	1.3	0.1	0.4	661	0.7	0.0	3.5	32	4.5	0.0
1/19/10 10:30	2.1	1077	3.9	0.2	1.0	943	1.8	0.1	0.6	830	1.1	0.1	0.6	661	1.1	0.0	3.1	32	4.0	0.0
1/19/10 11:00	2.1	1086	3.9	0.2	0.9	949	1.6	0.1	0.8	834	1.4	0.1	0.3	661	0.5	0.0	4.3	32	5.6	0.0
1/19/10 11:30	1.9	1067	3.5	0.2	0.7	936	1.3	0.1	1.0	826	1.8	0.1	0.4	661	0.7	0.0	5.4	32	7.1	0.0
1/19/10 12:00	2.0	1067	3.7	0.2	0.6	933	1.1	0.1	0.7	820	1.3	0.1	0.4	651	0.7	0.0	3.0	32	3.8	0.0
1/19/10 12:30	2.0	1067	3.7	0.2	0.7	930	1.3	0.1	0.9	814	1.6	0.1	0.4	641	0.7	0.0	4.4	31	5.7	0.0
1/19/10 13:00	1.9	1039	3.5	0.2	1.0	912	1.8	0.1	0.6	806	1.1	0.0	0.4	646	0.7	0.0	5.0	32	6.6	0.0
1/19/10 13:30	1.7	1058	3.1	0.2	1.0	920	1.8	0.1	0.7	805	1.3	0.1	0.3	631	0.5	0.0	4.1	31	5.3	0.0
1/19/10 14:00	1.8	1039	3.3	0.2	0.6	906	1.1	0.1	0.7	794	1.3	0.1	0.4	626	0.7	0.0	3.2	31	4.1	0.0
1/19/10 14:30	1.8	1039	3.3	0.2	0.6	906	1.1	0.1	0.8	794	1.4	0.1	0.4	626	0.7	0.0	4.0	31	5.2	0.0
1/19/10 15:00	1.8	1020	3.3	0.2	1.3	893	2.4	0.1	0.7	787	1.3	0.1	0.3	626	0.5	0.0	3.4	31	4.4	0.0
1/19/10 15:30	1.8	1029	3.3	0.2	0.6	898	1.1	0.1	0.5	787	0.9	0.0	0.3	622	0.5	0.0	3.4	31	4.4	0.0
1/19/10 16:00	1.8	1020	3.3	0.2	0.7	890	1.3	0.1	0.7	781	1.3	0.1	0.3	617	0.5	0.0	2.8	30	3.5	0.0
1/19/10 16:30	1.8	1012	3.3	0.2	1.0	884	1.8	0.1	0.6	777	1.1	0.0	0.4	617	0.7	0.0	4.4	30	5.7	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/19/10 17:00	1.8	1003	3.3	0.2	0.8	877	1.4	0.1	0.7	771	1.3	0.1	0.3	612	0.5	0.0	3.5	30	4.5	0.0
1/19/10 17:30	1.8	995	3.3	0.2	0.7	868	1.3	0.1	2.0	762	3.7	0.2	0.3	602	0.5	0.0	3.2	30	4.1	0.0
1/19/10 18:00	1.8	1003	3.3	0.2	1.0	876	1.8	0.1	0.6	768	1.1	0.0	0.3	607	0.5	0.0	3.7	30	4.8	0.0
1/19/10 18:30	1.8	995	3.3	0.2	0.4	868	0.7	0.0	0.7	762	1.3	0.1	0.3	602	0.5	0.0	3.2	30	4.1	0.0
1/19/10 19:00	2.0	986	3.7	0.2	0.8	861	1.4	0.1	0.7	756	1.3	0.1	0.3	598	0.5	0.0	3.1	29	4.0	0.0
1/19/10 19:30	1.8	986	3.3	0.2	0.5	860	0.9	0.0	0.9	753	1.6	0.1	0.3	593	0.5	0.0	3.0	29	3.8	0.0
1/19/10 20:00	1.8	978	3.3	0.2	1.0	853	1.8	0.1	0.7	747	1.3	0.1	0.3	588	0.5	0.0	3.6	29	4.6	0.0
1/19/10 20:30	1.8	962	3.3	0.2	0.9	840	1.6	0.1	0.6	737	1.1	0.0	0.4	584	0.7	0.0	3.3	29	4.2	0.0
1/19/10 21:00	1.9	970	3.5	0.2	0.7	844	1.3	0.1	0.8	738	1.4	0.1	0.3	579	0.5	0.0	2.4	29	3.0	0.0
1/19/10 21:30	1.7	962	3.1	0.2	0.6	837	1.1	0.1	0.8	732	1.4	0.1	0.4	575	0.7	0.0	2.7	28	3.4	0.0
1/19/10 22:00	1.9	953	3.5	0.2	0.5	830	0.9	0.0	0.7	726	1.3	0.1	0.3	570	0.5	0.0	2.6	28	3.3	0.0
1/19/10 22:30	1.9	962	3.5	0.2	0.6	835	1.1	0.1	0.6	729	1.1	0.0	0.3	570	0.5	0.0	2.9	28	3.7	0.0
1/19/10 23:00	2.2	953	4.0	0.2	0.6	828	1.1	0.1	0.6	723	1.1	0.0	0.3	565	0.5	0.0	2.9	28	3.7	0.0
1/19/10 23:30	1.8	953	3.3	0.2	0.7	827	1.3	0.1	0.7	721	1.3	0.1	0.3	561	0.5	0.0	2.2	28	2.7	0.0
1/20/10 0:00	1.7	937	3.1	0.2	0.6	816	1.1	0.0	0.7	714	1.3	0.1	0.3	561	0.5	0.0	2.7	28	3.4	0.0
1/20/10 0:30	1.9	937	3.5	0.2	0.6	815	1.1	0.0	0.6	711	1.1	0.0	0.4	556	0.7	0.0	2.2	27	2.7	0.0
1/20/10 1:00	1.9	913	3.5	0.2	0.5	798	0.9	0.0	0.8	702	1.4	0.1	0.3	556	0.5	0.0	2.5	27	3.1	0.0
1/20/10 1:30	1.8	913	3.3	0.2	0.6	798	1.1	0.0	0.7	702	1.3	0.0	0.3	556	0.5	0.0	1.9	27	2.4	0.0
1/20/10 2:00	1.9	921	3.5	0.2	0.5	801	0.9	0.0	0.7	699	1.3	0.0	0.4	547	0.7	0.0	3.0	27	3.8	0.0
1/20/10 2:30	2.3	913	4.2	0.2	0.6	794	1.1	0.0	0.9	694	1.6	0.1	0.3	543	0.5	0.0	2.3	27	2.9	0.0
1/20/10 3:00	1.9	905	3.5	0.2	0.9	789	1.6	0.1	0.7	690	1.3	0.0	0.3	543	0.5	0.0	1.9	27	2.4	0.0
1/20/10 3:30	2.2	897	4.0	0.2	1.2	782	2.2	0.1	0.6	684	1.1	0.0	0.3	539	0.5	0.0	2.5	27	3.1	0.0
1/20/10 4:00	2.4	890	4.4	0.2	0.7	774	1.3	0.1	0.6	676	1.1	0.0	0.3	530	0.5	0.0	2.2	26	2.7	0.0
1/20/10 4:30	1.8	905	3.3	0.2	0.7	786	1.3	0.1	0.6	685	1.1	0.0	0.3	534	0.5	0.0	2.1	26	2.6	0.0
1/20/10 5:00	1.8	897	3.3	0.2	0.6	778	1.1	0.0	0.5	677	0.9	0.0	0.3	525	0.5	0.0	3.3	26	4.2	0.0
1/20/10 5:30	1.7	897	3.1	0.2	0.6	778	1.1	0.0	0.6	677	1.1	0.0	0.4	525	0.7	0.0	3.8	26	4.9	0.0
1/20/10 6:00	2.2	897	4.0	0.2	0.6	778	1.1	0.0	1.1	677	2.0	0.1	0.3	525	0.5	0.0	2.1	26	2.6	0.0
1/20/10 6:30	1.6	882	2.9	0.1	0.6	766	1.1	0.0	0.7	668	1.3	0.0	0.3	521	0.5	0.0	1.1	26	1.3	0.0
1/20/10 7:00	3.3	882	6.1	0.3	1.8	763	3.3	0.1	0.6	663	1.1	0.0	0.3	512	0.5	0.0	1.9	25	2.4	0.0
1/20/10 7:30	1.7	874	3.1	0.2	1.1	759	2.0	0.1	1.6	662	2.9	0.1	0.3	517	0.5	0.0	1.9	26	2.4	0.0
1/20/10 8:00	1.9	874	3.5	0.2	0.7	759	1.3	0.1	0.7	662	1.3	0.0	0.3	517	0.5	0.0	1.0	26	1.2	0.0
1/20/10 8:30	2.1	874	3.9	0.2	0.7	758	1.3	0.1	0.5	659	0.9	0.0	0.3	512	0.5	0.0	2.1	25	2.6	0.0
1/20/10 9:00	1.6	866	2.9	0.1	0.7	750	1.3	0.1	0.6	651	1.1	0.0	0.2	504	0.4	0.0	1.8	25	2.2	0.0
1/20/10 9:30	1.8	859	3.3	0.2	0.6	743	1.1	0.0	0.7	646	1.3	0.0	0.3	500	0.5	0.0	1.9	25	2.4	0.0
1/20/10 10:00	1.8	859	3.3	0.2	0.7	743	1.3	0.1	0.5	646	0.9	0.0	0.3	500	0.5	0.0	1.3	25	1.6	0.0
1/20/10 10:30	2.0	859	3.7	0.2	0.7	743	1.3	0.1	0.7	646	1.3	0.0	0.4	500	0.7	0.0	1.0	25	1.2	0.0
1/20/10 11:00	1.6	843	2.9	0.1	0.6	730	1.1	0.0	0.5	634	0.9	0.0	0.3	491	0.5	0.0	1.5	24	1.8	0.0
1/20/10 11:30	1.7	843	3.1	0.1	0.9	730	1.6	0.1	0.6	634	1.1	0.0	0.3	491	0.5	0.0	0.7	24	0.8	0.0
1/20/10 12:00	1.7	836	3.1	0.1	0.6	725	1.1	0.0	0.8	631	1.4	0.1	0.4	491	0.7	0.0	1.3	24	1.6	0.0
1/20/10 12:30	1.7	843	3.1	0.1	0.5	729	0.9	0.0	0.6	632	1.1	0.0	0.3	487	0.5	0.0	1.5	24	1.8	0.0
1/20/10 13:00	3.0	843	5.6	0.3	0.4	729	0.7	0.0	0.6	632	1.1	0.0	0.3	487	0.5	0.0	1.0	24	1.2	0.0
1/20/10 13:30	1.7	828	3.1	0.1	0.6	717	1.1	0.0	0.6	623	1.1	0.0	0.3	483	0.5	0.0	1.1	24	1.3	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/20/10 14:00	1.7	828	3.1	0.1	1.0	717	1.8	0.1	0.7	623	1.3	0.0	0.4	483	0.7	0.0	1.3	24	1.6	0.0
1/20/10 14:30	1.7	828	3.1	0.1	0.6	717	1.1	0.0	1.0	623	1.8	0.1	0.3	483	0.5	0.0	0.4	24	0.4	0.0
1/20/10 15:00	2.3	821	4.2	0.2	0.6	711	1.1	0.0	0.7	618	1.3	0.0	0.3	479	0.5	0.0	0.8	24	0.9	0.0
1/20/10 15:30	1.6	821	2.9	0.1	0.7	709	1.3	0.1	0.9	615	1.6	0.1	0.2	475	0.4	0.0	1.0	24	1.2	0.0
1/20/10 16:00	1.9	813	3.5	0.2	0.6	703	1.1	0.0	0.7	610	1.3	0.0	0.4	471	0.7	0.0	1.6	23	2.0	0.0
1/20/10 16:30	2.3	806	4.2	0.2	0.5	698	0.9	0.0	0.6	607	1.1	0.0	0.3	471	0.5	0.0	1.2	23	1.4	0.0
1/20/10 17:00	1.7	806	3.1	0.1	0.5	697	0.9	0.0	1.2	605	2.2	0.1	0.3	467	0.5	0.0	2.2	23	2.7	0.0
1/20/10 17:30	1.8	813	3.3	0.2	0.6	702	1.1	0.0	0.5	608	0.9	0.0	0.5	467	0.9	0.0	1.4	23	1.7	0.0
1/20/10 18:00	1.7	799	3.1	0.1	0.6	690	1.1	0.0	0.6	599	1.1	0.0	0.3	462	0.5	0.0	1.1	23	1.3	0.0
1/20/10 18:30	1.9	791	3.5	0.2	0.9	685	1.6	0.1	0.5	596	0.9	0.0	0.3	462	0.5	0.0	0.6	23	0.7	0.0
1/20/10 19:00	1.7	791	3.1	0.1	0.6	684	1.1	0.0	0.6	594	1.1	0.0	0.4	458	0.7	0.0	2.5	23	3.1	0.0
1/20/10 19:30	2.2	799	4.0	0.2	1.2	688	2.2	0.1	0.5	594	0.9	0.0	0.3	454	0.5	0.0	0.6	23	0.7	0.0
1/20/10 20:00	1.6	791	2.9	0.1	0.7	682	1.3	0.0	0.6	589	1.1	0.0	0.3	450	0.5	0.0	5.0	23	6.6	0.0
1/20/10 20:30	1.7	791	3.1	0.1	1.3	682	2.4	0.1	0.9	589	1.6	0.1	0.4	450	0.7	0.0	1.2	23	1.4	0.0
1/20/10 21:00	1.7	784	3.1	0.1	0.4	675	0.7	0.0	0.6	584	1.1	0.0	0.3	447	0.5	0.0	2.5	22	3.1	0.0
1/20/10 21:30	2.1	777	3.9	0.2	0.6	672	1.1	0.0	1.2	583	2.2	0.1	0.3	450	0.5	0.0	0.8	23	0.9	0.0
1/20/10 22:00	1.7	777	3.1	0.1	0.6	670	1.1	0.0	1.2	581	2.2	0.1	0.3	447	0.5	0.0	1.2	22	1.4	0.0
1/20/10 22:30	1.7	777	3.1	0.1	0.8	669	1.4	0.1	1.2	579	2.2	0.1	1.2	443	2.2	0.1	1.4	22	1.7	0.0
1/20/10 23:00	1.7	784	3.1	0.1	0.7	674	1.3	0.0	0.7	581	1.3	0.0	0.3	443	0.5	0.0	1.8	22	2.2	0.0
1/20/10 23:30	1.7	777	3.1	0.1	0.7	668	1.3	0.0	0.6	576	1.1	0.0	0.3	439	0.5	0.0	7.6	22	10.2	0.0
1/21/10 0:00	1.7	770	3.1	0.1	0.6	662	1.1	0.0	0.4	571	0.7	0.0	0.3	435	0.5	0.0	3.2	22	4.1	0.0
1/21/10 0:30	1.8	762	3.3	0.1	0.7	656	1.3	0.0	0.6	566	1.1	0.0	0.3	431	0.5	0.0	1.2	22	1.4	0.0
1/21/10 1:00	1.8	770	3.3	0.1	0.7	661	1.3	0.0	0.8	569	1.4	0.0	0.3	431	0.5	0.0	0.9	22	1.1	0.0
1/21/10 1:30	1.7	755	3.1	0.1	0.7	662	1.3	0.0	0.6	571	1.1	0.0	0.4	435	0.7	0.0	1.2	22	1.4	0.0
1/21/10 2:00	1.7	755	3.1	0.1	0.7	648	1.3	0.0	1.0	558	1.8	0.1	0.4	423	0.7	0.0	1.6	21	2.0	0.0
1/21/10 2:30	1.7	748	3.1	0.1	0.5	645	0.9	0.0	0.7	558	1.3	0.0	0.3	427	0.5	0.0	2.0	21	2.5	0.0
1/21/10 3:00	1.9	755	3.5	0.1	0.5	648	0.9	0.0	0.7	558	1.3	0.0	0.3	423	0.5	0.0	1.0	21	1.2	0.0
1/21/10 3:30	1.8	741	3.3	0.1	0.5	639	0.9	0.0	0.6	553	1.1	0.0	0.3	423	0.5	0.0	1.7	21	2.1	0.0
1/21/10 4:00	1.7	748	3.1	0.1	0.7	642	1.3	0.0	0.9	553	1.6	0.1	1.1	419	2.0	0.0	1.3	21	1.6	0.0
1/21/10 4:30	1.7	741	3.1	0.1	1.5	638	2.7	0.1	0.5	550	0.9	0.0	0.4	419	0.7	0.0	3.3	21	4.2	0.0
1/21/10 5:00	1.8	741	3.3	0.1	0.7	636	1.3	0.0	0.6	548	1.1	0.0	0.5	416	0.9	0.0	1.1	21	1.3	0.0
1/21/10 5:30	1.7	734	3.1	0.1	0.4	632	0.7	0.0	0.6	545	1.1	0.0	0.6	416	1.1	0.0	2.7	21	3.4	0.0
1/21/10 6:00	1.7	727	3.1	0.1	0.7	626	1.3	0.0	0.6	540	1.1	0.0	0.3	412	0.5	0.0	1.3	21	1.6	0.0
1/21/10 6:30	1.7	734	3.1	0.1	0.5	630	0.9	0.0	0.6	543	1.1	0.0	0.6	412	1.1	0.0	1.2	21	1.4	0.0
1/21/10 7:00	1.9	734	3.5	0.1	0.6	630	1.1	0.0	0.6	543	1.1	0.0	0.6	412	1.1	0.0	0.6	21	0.7	0.0
1/21/10 7:30	1.9	720	3.5	0.1	0.6	620	1.1	0.0	0.6	535	1.1	0.0	0.3	408	0.5	0.0	1.1	21	1.3	0.0
1/21/10 8:00	1.6	720	2.9	0.1	0.7	620	1.3	0.0	1.4	535	2.6	0.1	0.4	408	0.7	0.0	0.6	21	0.7	0.0
1/21/10 8:30	2.9	720	5.4	0.2	0.6	619	1.1	0.0	1.0	533	1.8	0.1	0.3	404	0.5	0.0	1.3	20	1.6	0.0
1/21/10 9:00	1.7	720	3.1	0.1	0.4	617	0.7	0.0	0.5	531	0.9	0.0	0.3	401	0.5	0.0	0.7	20	0.8	0.0
1/21/10 9:30	1.7	707	3.1	0.1	0.6	607	1.1	0.0	0.6	523	1.1	0.0	0.3	397	0.5	0.0	1.4	20	1.7	0.0
1/21/10 10:00	2.0	707	3.7	0.1	0.5	608	0.9	0.0	0.5	525	0.9	0.0	0.3	401	0.5	0.0	0.3	20	0.3	0.0
1/21/10 10:30	1.5	707	2.7	0.1	0.4	607	0.7	0.0	0.6	523	1.1	0.0	0.3	397	0.5	0.0	1.5	20	1.8	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/21/10 11:00	1.7	707	3.1	0.1	0.6	606	1.1	0.0	0.7	521	1.3	0.0	0.3	393	0.5	0.0	2.1	20	2.6	0.0
1/21/10 11:30	2.3	700	4.2	0.2	0.5	600	0.9	0.0	0.6	516	1.1	0.0	0.3	390	0.5	0.0	0.3	20	0.3	0.0
1/21/10 12:00	1.8	693	3.3	0.1	0.6	597	1.1	0.0	0.5	515	0.9	0.0	0.2	393	0.4	0.0	0.9	20	1.1	0.0
1/21/10 12:30	1.8	693	3.3	0.1	0.6	595	1.1	0.0	0.4	513	0.7	0.0	0.3	390	0.5	0.0	1.3	20	1.6	0.0
1/21/10 13:00	1.7	693	3.1	0.1	0.7	594	1.3	0.0	0.5	511	0.9	0.0	0.3	386	0.5	0.0	0.7	19	0.8	0.0
1/21/10 13:30	2.0	693	3.7	0.1	0.7	594	1.3	0.0	0.9	511	1.6	0.0	0.2	386	0.4	0.0	2.4	19	3.0	0.0
1/21/10 14:00	1.6	680	2.9	0.1	0.6	584	1.1	0.0	0.6	503	1.1	0.0	0.3	382	0.5	0.0	3.0	19	3.8	0.0
1/21/10 14:30	2.2	686	4.0	0.2	0.3	589	0.5	0.0	0.6	506	1.1	0.0	0.3	382	0.5	0.0	1.6	19	2.0	0.0
1/21/10 15:00	1.7	680	3.1	0.1	0.6	584	1.1	0.0	1.0	503	1.8	0.1	0.2	382	0.4	0.0	0.5	19	0.6	0.0
1/21/10 15:30	1.7	673	3.1	0.1	0.6	580	1.1	0.0	0.7	501	1.3	0.0	0.3	382	0.5	0.0	2.0	19	2.5	0.0
1/21/10 16:00	1.7	680	3.1	0.1	0.6	583	1.1	0.0	0.4	501	0.7	0.0	0.3	379	0.5	0.0	2.0	19	2.5	0.0
1/21/10 16:30	1.6	673	2.9	0.1	0.6	577	1.1	0.0	0.4	496	0.7	0.0	0.3	375	0.5	0.0	1.1	19	1.3	0.0
1/21/10 17:00	1.6	673	2.9	0.1	0.4	577	0.7	0.0	0.5	496	0.9	0.0	0.3	375	0.5	0.0	1.4	19	1.7	0.0
1/21/10 17:30	1.7	660	3.1	0.1	0.4	567	0.7	0.0	0.6	489	1.1	0.0	0.3	372	0.5	0.0	0.8	19	0.9	0.0
1/21/10 18:00	1.5	673	2.7	0.1	0.5	576	0.9	0.0	0.7	494	1.3	0.0	0.3	372	0.5	0.0	0.9	19	1.1	0.0
1/21/10 18:30	1.7	660	3.1	0.1	0.6	567	1.1	0.0	0.5	489	0.9	0.0	0.3	372	0.5	0.0	1.9	19	2.4	0.0
1/21/10 19:00	2.2	667	4.0	0.2	0.8	570	1.4	0.0	0.7	490	1.3	0.0	0.3	368	0.5	0.0	1.6	19	2.0	0.0
1/21/10 19:30	1.7	653	3.1	0.1	0.6	562	1.1	0.0	0.7	484	1.3	0.0	0.3	368	0.5	0.0	1.4	19	1.7	0.0
1/21/10 20:00	1.7	653	3.1	0.1	1.5	562	2.7	0.1	0.7	484	1.3	0.0	0.3	368	0.5	0.0	0.7	19	0.8	0.0
1/21/10 20:30	2.1	660	3.9	0.1	0.5	565	0.9	0.0	0.4	485	0.7	0.0	0.3	365	0.5	0.0	1.4	18	1.7	0.0
1/21/10 21:00	1.7	653	3.1	0.1	0.5	560	0.9	0.0	0.6	482	1.1	0.0	0.3	365	0.5	0.0	0.5	18	0.6	0.0
1/21/10 21:30	1.8	647	3.3	0.1	0.3	556	0.5	0.0	0.6	480	1.1	0.0	0.3	365	0.5	0.0	0.6	18	0.7	0.0
1/21/10 22:00	1.7	653	3.1	0.1	0.5	559	0.9	0.0	0.5	480	0.9	0.0	0.3	361	0.5	0.0	1.3	18	1.6	0.0
1/21/10 22:30	1.6	641	2.9	0.1	0.3	550	0.5	0.0	0.6	473	1.1	0.0	0.5	358	0.9	0.0	1.2	18	1.4	0.0
1/21/10 23:00	1.7	647	3.1	0.1	0.4	555	0.7	0.0	1.0	477	1.8	0.0	0.3	361	0.5	0.0	1.1	18	1.3	0.0
1/21/10 23:30	1.7	653	3.1	0.1	0.6	558	1.1	0.0	0.6	478	1.1	0.0	0.4	358	0.7	0.0	1.1	18	1.3	0.0
1/22/10 0:00	1.7	635	3.1	0.1	0.7	544	1.3	0.0	0.6	468	1.1	0.0	0.3	354	0.5	0.0	1.2	18	1.4	0.0
1/22/10 0:30	1.8	635	3.3	0.1	0.4	544	0.7	0.0	0.8	468	1.4	0.0	0.3	354	0.5	0.0	1.1	18	1.3	0.0
1/22/10 1:00	1.6	635	2.9	0.1	0.7	544	1.3	0.0	0.5	468	0.9	0.0	0.3	354	0.5	0.0	0.9	18	1.1	0.0
1/22/10 1:30	1.6	635	2.9	0.1	0.4	543	0.7	0.0	0.4	466	0.7	0.0	0.4	351	0.7	0.0	1.6	18	2.0	0.0
1/22/10 2:00	1.6	629	2.9	0.1	0.7	539	1.3	0.0	0.5	464	0.9	0.0	0.3	351	0.5	0.0	0.7	18	0.8	0.0
1/22/10 2:30	1.9	629	3.5	0.1	0.7	538	1.3	0.0	0.5	462	0.9	0.0	0.3	347	0.5	0.0	0.3	18	0.3	0.0
1/22/10 3:00	2.0	623	3.7	0.1	0.6	534	1.1	0.0	0.7	459	1.3	0.0	0.3	347	0.5	0.0	1.0	18	1.2	0.0
1/22/10 3:30	1.7	629	3.1	0.1	1.2	538	2.2	0.1	0.4	462	0.7	0.0	0.3	347	0.5	0.0	0.7	18	0.8	0.0
1/22/10 4:00	1.7	623	3.1	0.1	0.6	533	1.1	0.0	0.6	457	1.1	0.0	0.3	344	0.5	0.0	0.3	17	0.3	0.0
1/22/10 4:30	2.8	623	5.2	0.2	0.4	533	0.7	0.0	0.9	457	1.6	0.0	0.3	344	0.5	0.0	0.3	17	0.3	0.0
1/22/10 5:00	1.9	617	3.5	0.1	0.5	529	0.9	0.0	0.5	455	0.9	0.0	0.3	344	0.5	0.0	0.5	17	0.6	0.0
1/22/10 5:30	1.8	617	3.3	0.1	0.3	529	0.5	0.0	0.7	455	1.3	0.0	0.3	344	0.5	0.0	0.5	17	0.6	0.0
1/22/10 6:00	1.7	617	3.1	0.1	0.3	528	0.5	0.0	0.6	453	1.1	0.0	0.3	341	0.5	0.0	0.6	17	0.7	0.0
1/22/10 6:30	1.5	623	2.7	0.1	0.4	532	0.7	0.0	0.5	455	0.9	0.0	0.5	341	0.9	0.0	0.6	17	0.7	0.0
1/22/10 7:00	1.7	611	3.1	0.1	0.5	523	0.9	0.0	0.4	449	0.7	0.0	0.3	337	0.5	0.0	0.3	17	0.3	0.0
1/22/10 7:30	1.9	611	3.5	0.1	0.4	523	0.7	0.0	0.5	449	0.9	0.0	1.2	337	2.2	0.0	0.6	17	0.7	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/22/10 8:00	1.9	611	3.5	0.1	0.5	523	0.9	0.0	0.6	449	1.1	0.0	0.3	337	0.5	0.0	0.5	17	0.6	0.0
1/22/10 8:30	1.6	605	2.9	0.1	0.4	519	0.7	0.0	0.6	446	1.1	0.0	0.3	337	0.5	0.0	2.1	17	2.6	0.0
1/22/10 9:00	1.6	611	2.9	0.1	0.5	523	0.9	0.0	0.7	449	1.3	0.0	0.3	337	0.5	0.0	1.2	17	1.4	0.0
1/22/10 9:30	1.8	605	3.3	0.1	0.2	518	0.4	0.0	0.7	444	1.3	0.0	0.3	334	0.5	0.0	2.0	17	2.5	0.0
1/22/10 10:00	1.7	605	3.1	0.1	0.5	518	0.9	0.0	1.0	444	1.8	0.0	0.3	334	0.5	0.0	0.5	17	0.6	0.0
1/22/10 10:30	1.6	599	2.9	0.1	0.3	514	0.5	0.0	0.4	442	0.7	0.0	0.6	334	1.1	0.0	1.5	17	1.8	0.0
1/22/10 11:00	1.9	605	3.5	0.1	0.5	518	0.9	0.0	0.4	444	0.7	0.0	0.3	334	0.5	0.0	1.3	17	1.6	0.0
1/22/10 11:30	1.6	605	2.9	0.1	0.3	518	0.5	0.0	0.5	444	0.9	0.0	0.3	334	0.5	0.0	1.3	17	1.6	0.0
1/22/10 12:00	1.6	605	2.9	0.1	0.3	518	0.5	0.0	0.6	444	1.1	0.0	0.3	334	0.5	0.0	2.4	17	3.0	0.0
1/22/10 12:30	1.6	605	2.9	0.1	0.4	517	0.7	0.0	0.5	442	0.9	0.0	0.3	331	0.5	0.0	1.0	17	1.2	0.0
1/22/10 13:00	1.6	605	2.9	0.1	0.4	517	0.7	0.0	0.5	442	0.9	0.0	0.2	331	0.4	0.0	3.3	17	4.2	0.0
1/22/10 13:30	1.6	605	2.9	0.1	0.7	518	1.3	0.0	0.6	444	1.1	0.0	0.3	334	0.5	0.0	4.1	17	5.3	0.0
1/22/10 14:00	1.7	611	3.1	0.1	0.7	521	1.3	0.0	0.8	445	1.4	0.0	0.3	331	0.5	0.0	6.5	17	8.7	0.0
1/22/10 14:30	1.6	605	2.9	0.1	1.1	518	2.0	0.1	0.6	444	1.1	0.0	0.3	334	0.5	0.0	6.4	17	8.5	0.0
1/22/10 15:00	1.6	605	2.9	0.1	0.5	518	0.9	0.0	0.5	444	0.9	0.0	0.3	334	0.5	0.0	9.9	17	13.6	0.0
1/22/10 15:30	1.7	617	3.1	0.1	0.5	526	0.9	0.0	0.5	449	0.9	0.0	0.3	334	0.5	0.0	22.0	17	31.7	0.0
1/22/10 16:00	1.7	611	3.1	0.1	0.6	522	1.1	0.0	0.6	447	1.1	0.0	0.3	334	0.5	0.0	30.0	17	44.0	0.0
1/22/10 16:30	2.2	617	4.0	0.1	0.5	526	0.9	0.0	0.6	449	1.1	0.0	0.3	334	0.5	0.0	28.0	17	40.9	0.0
1/22/10 17:00	1.8	629	3.3	0.1	0.5	535	0.9	0.0	0.6	456	1.1	0.0	0.2	337	0.4	0.0	34.0	17	50.3	0.0
1/22/10 17:30	1.9	635	3.5	0.1	1.1	540	2.0	0.1	0.7	460	1.3	0.0	0.3	341	0.5	0.0	34.0	17	50.3	0.0
1/22/10 18:00	2.0	635	3.7	0.1	0.8	540	1.4	0.0	0.9	460	1.6	0.0	0.2	341	0.4	0.0	49.0	17	74.2	0.1
1/22/10 18:30	2.0	641	3.7	0.1	0.8	544	1.4	0.0	1.2	463	2.2	0.1	0.5	341	0.9	0.0	130.0	17	209.1	0.2
1/22/10 19:00	2.1	641	3.9	0.1	1.0	543	1.8	0.1	1.1	461	2.0	0.1	0.3	337	0.5	0.0	41.0	17	61.4	0.1
1/22/10 19:30	2.4	647	4.4	0.2	0.8	547	1.4	0.0	1.6	463	2.9	0.1	0.3	337	0.5	0.0	41.0	17	61.4	0.1
1/22/10 20:00	2.7	653	5.0	0.2	0.9	551	1.6	0.1	1.4	464	2.6	0.1	0.7	334	1.3	0.0	73.0	17	113.3	0.1
1/22/10 20:30	2.2	653	4.0	0.1	1.0	551	1.8	0.1	1.5	464	2.7	0.1	0.2	334	0.4	0.0	48.0	17	72.6	0.1
1/22/10 21:00	2.5	653	4.6	0.2	1.1	550	2.0	0.1	1.5	462	2.7	0.1	0.3	331	0.5	0.0	26.0	17	37.8	0.0
1/22/10 21:30	2.9	647	5.4	0.2	1.3	545	2.4	0.1	2.2	459	4.0	0.1	0.3	331	0.5	0.0	25.0	17	36.3	0.0
1/22/10 22:00	2.3	647	4.4	0.2	1.4	544	2.6	0.1	2.8	457	5.2	0.1	0.3	327	0.5	0.0	55.0	17	83.9	0.1
1/22/10 22:30	2.3	635	4.2	0.2	1.6	535	2.9	0.1	2.8	451	5.2	0.1	0.3	324	0.5	0.0	75.0	17	116.6	0.1
1/22/10 23:00	2.8	635	5.2	0.2	1.7	535	3.1	0.1	2.4	451	4.4	0.1	0.4	324	0.7	0.0	100.0	17	158.2	0.1
1/22/10 23:30	2.9	629	5.4	0.2	2.0	530	3.7	0.1	2.4	446	4.4	0.1	0.3	321	0.5	0.0	69.0	16	106.7	0.1
1/23/10 0:00	2.5	629	4.6	0.2	2.8	530	5.2	0.2	2.3	446	4.2	0.1	0.2	321	0.5	0.0	46.0	16	69.4	0.1
1/23/10 0:30	2.3	629	4.2	0.1	2.4	529	4.4	0.1	2.2	444	4.0	0.1	0.3	318	0.5	0.0	45.0	16	67.8	0.1
1/23/10 1:00	2.4	617	4.4	0.2	2.0	521	3.7	0.1	1.9	439	3.5	0.1	0.3	318	0.5	0.0	45.0	16	67.8	0.1
1/23/10 1:30	2.2	605	4.0	0.1	2.1	511	3.9	0.1	1.7	433	3.1	0.1	0.3	314	0.5	0.0	38.0	16	56.6	0.1
1/23/10 2:00	2.4	605	4.4	0.2	1.7	510	3.1	0.1	2.2	431	4.0	0.1	0.3	311	0.4	0.0	44.0	16	66.2	0.1
1/23/10 2:30	2.3	599	4.2	0.1	1.6	506	2.9	0.1	3.0	428	5.6	0.1	0.3	311	0.5	0.0	32.0	16	47.2	0.0
1/23/10 3:00	2.3	605	4.2	0.1	1.3	510	2.4	0.1	3.0	431	5.6	0.1	0.3	311	0.5	0.0	43.0	16	64.6	0.1
1/23/10 3:30	2.4	599	4.4	0.1	1.5	505	2.7	0.1	2.7	427	5.0	0.1	0.2	308	0.4	0.0	49.0	16	74.2	0.1
1/23/10 4:00	2.5	588	4.6	0.2	2.0	498	3.7	0.1	2.5	422	4.6	0.1	0.3	308	0.5	0.0	32.0	16	47.2	0.0
1/23/10 4:30	2.6	588	4.8	0.2	2.4	498	4.4	0.1	2.2	422	4.0	0.1	1.4	308	2.6	0.0	30.0	16	44.0	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/23/10 5:00	2.8	582	5.2	0.2	2.5	493	4.6	0.1	1.9	418	3.5	0.1	0.3	305	0.5	0.0	57.0	16	87.1	0.1
1/23/10 5:30	3.4	582	6.3	0.2	2.0	493	3.7	0.1	1.9	418	3.5	0.1	0.5	305	0.9	0.0	54.0	16	82.2	0.1
1/23/10 6:00	2.8	582	5.2	0.2	1.8	492	3.3	0.1	1.7	416	3.1	0.1	0.3	302	0.5	0.0	65.0	15	100.1	0.1
1/23/10 6:30	2.9	582	5.4	0.2	1.6	492	2.9	0.1	1.8	416	3.3	0.1	0.3	302	0.5	0.0	48.0	15	72.6	0.1
1/23/10 7:00	2.9	576	5.4	0.2	1.5	487	2.7	0.1	1.8	412	3.3	0.1	0.5	299	0.9	0.0	40.0	15	59.8	0.1
1/23/10 7:30	3.0	576	5.6	0.2	1.5	487	2.7	0.1	2.3	412	4.2	0.1	0.3	299	0.5	0.0	23.0	15	33.2	0.0
1/23/10 8:00	2.8	570	5.2	0.2	1.6	483	2.9	0.1	1.6	409	2.9	0.1	0.3	299	0.5	0.0	44.0	15	66.2	0.1
1/23/10 8:30	2.7	570	5.0	0.2	1.4	483	2.6	0.1	1.6	409	2.9	0.1	0.3	299	0.5	0.0	37.0	15	55.0	0.0
1/23/10 9:00	2.6	565	4.8	0.2	1.9	479	3.5	0.1	2.0	407	3.7	0.1	0.3	299	0.5	0.0	22.0	15	31.7	0.0
1/23/10 9:30	3.0	565	5.6	0.2	1.3	478	2.4	0.1	2.1	405	3.9	0.1	0.3	296	0.5	0.0	17.0	15	24.1	0.0
1/23/10 10:00	2.9	559	5.4	0.2	1.3	474	2.4	0.1	2.1	403	3.9	0.1	0.3	296	0.5	0.0	25.0	15	36.3	0.0
1/23/10 10:30	3.3	565	6.1	0.2	1.8	478	3.3	0.1	2.0	405	3.7	0.1	0.3	296	0.5	0.0	24.0	15	34.8	0.0
1/23/10 11:00	3.1	565	5.7	0.2	1.5	478	2.7	0.1	1.7	405	3.1	0.1	0.3	296	0.5	0.0	21.0	15	30.2	0.0
1/23/10 11:30	3.1	553	5.7	0.2	1.7	469	3.1	0.1	1.6	399	2.9	0.1	0.3	293	0.5	0.0	12.0	15	16.6	0.0
1/23/10 12:00	2.8	553	5.2	0.2	1.8	468	3.3	0.1	1.4	397	2.6	0.1	0.3	290	0.5	0.0	12.0	15	16.6	0.0
1/23/10 12:30	2.5	559	4.6	0.1	1.5	472	2.7	0.1	2.0	399	3.7	0.1	0.2	290	0.4	0.0	11.0	15	15.2	0.0
1/23/10 13:00	2.6	548	4.8	0.1	1.4	465	2.6	0.1	1.3	395	2.4	0.1	0.4	290	0.7	0.0	25.0	15	36.3	0.0
1/23/10 13:30	2.3	548	4.2	0.1	1.1	465	2.0	0.1	1.2	395	2.2	0.0	0.3	290	0.5	0.0	44.0	15	66.2	0.1
1/23/10 14:00	2.6	548	4.8	0.1	1.3	465	2.4	0.1	1.2	395	2.2	0.0	0.3	290	0.5	0.0	35.0	15	51.9	0.0
1/23/10 14:30	2.6	542	4.8	0.1	1.2	460	2.2	0.1	1.2	391	2.2	0.0	0.3	286	0.5	0.0	26.0	15	37.8	0.0
1/23/10 15:00	2.2	548	4.0	0.1	1.1	464	2.0	0.1	1.2	393	2.2	0.0	0.2	286	0.4	0.0	20.0	15	28.6	0.0
1/23/10 15:30	2.5	542	4.6	0.1	0.8	459	1.4	0.0	1.1	389	2.0	0.0	0.3	283	0.5	0.0	29.0	15	42.5	0.0
1/23/10 16:00	2.6	542	4.8	0.1	1.0	460	1.8	0.0	1.0	391	1.8	0.0	0.2	286	0.4	0.0	18.0	15	25.6	0.0
1/23/10 16:30	2.2	537	4.0	0.1	0.8	456	1.4	0.0	0.9	388	1.6	0.0	0.2	286	0.4	0.0	17.0	15	24.1	0.0
1/23/10 17:00	2.2	537	4.0	0.1	0.9	455	1.6	0.0	1.1	387	2.0	0.0	0.5	283	0.9	0.0	8.5	15	11.5	0.0
1/23/10 17:30	2.6	537	4.8	0.1	0.8	455	1.4	0.0	1.3	387	2.4	0.1	0.3	283	0.5	0.0	9.7	15	13.3	0.0
1/23/10 18:00	2.5	537	4.6	0.1	0.8	455	1.4	0.0	1.5	387	2.7	0.1	0.3	283	0.5	0.0	8.3	15	11.3	0.0
1/23/10 18:30	2.4	531	4.4	0.1	1.1	452	2.0	0.1	1.6	384	2.9	0.1	0.3	283	0.5	0.0	5.8	15	7.7	0.0
1/23/10 19:00	2.5	537	4.6	0.1	1.0	455	1.8	0.0	1.3	387	2.4	0.1	0.3	283	0.5	0.0	7.3	15	9.8	0.0
1/23/10 19:30	2.6	531	4.8	0.1	1.3	452	2.4	0.1	1.3	384	2.4	0.1	0.3	283	0.5	0.0	19.0	15	27.1	0.0
1/23/10 20:00	2.2	526	4.0	0.1	1.1	448	2.0	0.1	1.2	382	2.2	0.0	0.3	283	0.5	0.0	15.0	15	21.1	0.0
1/23/10 20:30	2.2	531	4.0	0.1	1.3	452	2.4	0.1	1.0	384	1.8	0.0	0.2	283	0.4	0.0	28.0	15	40.9	0.0
1/23/10 21:00	2.3	526	4.2	0.1	1.6	447	2.9	0.1	0.9	380	1.6	0.0	0.3	280	0.5	0.0	18.0	14	25.6	0.0
1/23/10 21:30	1.9	526	3.5	0.1	2.6	447	4.8	0.1	1.0	380	1.8	0.0	0.4	280	0.7	0.0	11.0	14	15.2	0.0
1/23/10 22:00	2.0	526	3.7	0.1	0.9	446	1.6	0.0	0.7	379	1.3	0.0	0.3	277	0.5	0.0	14.0	14	19.6	0.0
1/23/10 22:30	2.0	521	3.7	0.1	0.8	443	1.4	0.0	0.9	378	1.6	0.0	0.3	280	0.5	0.0	29.0	14	42.5	0.0
1/23/10 23:00	1.8	521	3.3	0.1	0.8	442	1.4	0.0	0.8	376	1.4	0.0	0.3	277	0.5	0.0	19.0	14	27.1	0.0
1/23/10 23:30	1.9	521	3.5	0.1	0.6	442	1.1	0.0	0.9	376	1.6	0.0	0.3	277	0.5	0.0	18.0	14	25.6	0.0
1/24/10 0:00	1.8	521	3.3	0.1	0.9	441	1.6	0.0	0.9	375	1.6	0.0	0.5	275	0.9	0.0	11.0	14	15.2	0.0
1/24/10 0:30	1.8	521	3.3	0.1	0.8	441	1.4	0.0	1.0	375	1.8	0.0	0.3	275	0.5	0.0	11.0	14	15.2	0.0
1/24/10 1:00	1.9	521	3.5	0.1	0.5	441	0.9	0.0	1.2	375	2.2	0.0	0.3	275	0.5	0.0	17.0	14	24.1	0.0
1/24/10 1:30	2.2	515	4.0	0.1	0.6	438	1.1	0.0	1.0	372	1.8	0.0	0.3	275	0.5	0.0	27.0	14	39.4	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/24/10 2:00	2.0	515	3.7	0.1	0.6	437	1.1	0.0	1.0	371	1.8	0.0	0.3	272	0.5	0.0	12.0	14	16.6	0.0
1/24/10 2:30	2.3	515	4.2	0.1	0.8	437	1.4	0.0	1.1	371	2.0	0.0	0.3	272	0.5	0.0	9.3	14	12.7	0.0
1/24/10 3:00	1.9	510	3.5	0.1	0.9	433	1.6	0.0	1.1	368	2.0	0.0	0.3	272	0.5	0.0	6.6	14	8.8	0.0
1/24/10 3:30	2.0	510	3.7	0.1	0.6	432	1.1	0.0	1.0	367	1.8	0.0	0.3	269	0.5	0.0	6.4	14	8.5	0.0
1/24/10 4:00	2.1	504	3.9	0.1	1.0	429	1.8	0.0	0.9	365	1.6	0.0	0.2	269	0.4	0.0	7.4	14	10.0	0.0
1/24/10 4:30	1.9	510	3.5	0.1	0.8	432	1.4	0.0	0.9	367	1.6	0.0	0.3	269	0.5	0.0	7.8	14	10.5	0.0
1/24/10 5:00	1.9	510	3.5	0.1	0.9	432	1.6	0.0	0.9	367	1.6	0.0	0.3	269	0.5	0.0	8.7	14	11.8	0.0
1/24/10 5:30	1.8	504	3.3	0.1	0.7	429	1.3	0.0	0.9	365	1.6	0.0	0.2	269	0.4	0.0	6.5	14	8.7	0.0
1/24/10 6:00	1.8	504	3.3	0.1	0.8	428	1.4	0.0	1.0	363	1.8	0.0	0.3	266	0.5	0.0	4.9	14	6.4	0.0
1/24/10 6:30	1.8	504	3.3	0.1	0.6	428	1.1	0.0	0.8	363	1.4	0.0	0.3	266	0.5	0.0	5.2	14	6.8	0.0
1/24/10 7:00	1.8	504	3.3	0.1	1.3	428	2.4	0.1	0.9	363	1.6	0.0	0.2	266	0.4	0.0	4.7	14	6.2	0.0
1/24/10 7:30	1.8	499	3.3	0.1	0.9	424	1.6	0.0	0.7	361	1.3	0.0	0.3	266	0.5	0.0	4.2	14	5.5	0.0
1/24/10 8:00	2.0	499	3.7	0.1	0.8	423	1.4	0.0	0.7	359	1.3	0.0	0.3	263	0.5	0.0	17.0	14	24.1	0.0
1/24/10 8:30	2.1	504	3.9	0.1	0.6	428	1.1	0.0	0.8	363	1.4	0.0	0.3	266	0.5	0.0	13.0	14	18.1	0.0
1/24/10 9:00	2.0	499	3.7	0.1	0.8	424	1.4	0.0	0.9	361	1.6	0.0	0.3	266	0.5	0.0	7.1	14	9.5	0.0
1/24/10 9:30	2.1	504	3.9	0.1	0.7	428	1.3	0.0	0.8	363	1.4	0.0	0.3	266	0.5	0.0	3.8	14	4.9	0.0
1/24/10 10:00	2.2	499	4.0	0.1	1.1	425	2.0	0.0	0.7	362	1.3	0.0	0.2	269	0.4	0.0	4.3	14	5.6	0.0
1/24/10 10:30	1.8	499	3.3	0.1	0.5	425	0.9	0.0	0.7	362	1.3	0.0	0.3	269	0.5	0.0	4.1	14	5.3	0.0
1/24/10 11:00	2.1	504	3.9	0.1	0.5	429	0.9	0.0	0.6	365	1.1	0.0	0.3	269	0.5	0.0	7.4	14	10.0	0.0
1/24/10 11:30	1.9	504	3.5	0.1	0.5	429	0.9	0.0	0.7	366	1.3	0.0	0.3	272	0.5	0.0	18.0	14	25.6	0.0
1/24/10 12:00	2.1	515	3.9	0.1	0.6	438	1.1	0.0	0.8	372	1.4	0.0	0.3	275	0.5	0.0	77.0	14	119.9	0.1
1/24/10 12:30	2.0	521	3.7	0.1	0.6	442	1.1	0.0	0.7	376	1.3	0.0	0.4	277	0.7	0.0	130.0	14	209.1	0.2
1/24/10 13:00	2.0	521	3.7	0.1	0.5	443	0.9	0.0	0.9	378	1.6	0.0	0.3	280	0.5	0.0	420.0	14	726.5	0.6
1/24/10 13:30	2.1	526	3.9	0.1	1.2	449	2.2	0.1	0.8	384	1.4	0.0	0.3	286	0.5	0.0	240.0	15	401.0	0.3
1/24/10 14:00	2.1	526	3.9	0.1	0.9	451	1.6	0.0	0.7	387	1.3	0.0	0.3	293	0.5	0.0	300.0	15	508.2	0.4
1/24/10 14:30	2.0	537	3.7	0.1	0.9	460	1.6	0.0	1.0	396	1.8	0.0	0.4	299	0.7	0.0	440.0	15	763.3	0.7
1/24/10 15:00	2.1	548	3.9	0.1	1.1	471	2.0	0.1	1.0	406	1.8	0.0	0.2	308	0.4	0.0	470.0	16	818.7	0.7
1/24/10 15:30	2.0	559	3.7	0.1	1.6	483	2.9	0.1	1.2	420	2.2	0.1	0.3	324	0.5	0.0	320.0	17	544.2	0.5
1/24/10 16:00	2.1	570	3.9	0.1	0.9	495	1.6	0.0	2.5	432	4.6	0.1	0.4	337	0.7	0.0	250.0	17	418.7	0.4
1/24/10 16:30	2.3	576	4.2	0.1	1.2	506	2.2	0.1	6.5	447	12.2	0.3	0.2	358	0.4	0.0	490.0	18	855.7	0.9
1/24/10 17:00	2.1	593	3.9	0.1	1.4	524	2.6	0.1	9.0	466	17.0	0.4	0.3	379	0.5	0.0	640.0	19	1136.4	1.2
1/24/10 17:30	2.4	605	4.4	0.2	2.2	540	4.0	0.1	10.5	486	19.9	0.5	0.3	404	0.5	0.0	570.0	20	1004.8	1.1
1/24/10 18:00	2.3	617	4.2	0.1	4.7	557	8.8	0.3	14.7	507	28.1	0.8	3.3	431	6.1	0.1	410.0	22	708.1	0.9
1/24/10 18:30	2.7	623	5.0	0.2	7.2	570	13.6	0.4	15.5	525	29.6	0.9	3.3	458	6.1	0.1	530.0	23	930.1	1.2
1/24/10 19:00	2.6	647	4.8	0.2	9.8	593	18.6	0.6	14.0	547	26.7	0.8	0.4	479	0.7	0.0	380.0	24	653.2	0.9
1/24/10 19:30	3.8	660	7.1	0.3	11.9	611	22.6	0.8	17.1	570	32.8	1.0	0.4	508	0.7	0.0	240.0	25	401.0	0.6
1/24/10 20:00	2.6	686	4.8	0.2	13.0	637	24.8	0.9	22.9	596	44.1	1.5	0.4	534	0.7	0.0	180.0	26	295.4	0.4
1/24/10 20:30	2.9	714	5.4	0.2	12.9	660	24.6	0.9	24.2	615	46.7	1.6	0.5	547	0.9	0.0	98.0	27	154.9	0.2
1/24/10 21:00	2.7	734	5.0	0.2	15.1	678	28.9	1.1	23.4	631	45.1	1.6	0.4	561	0.7	0.0	170.0	28	278.0	0.4
1/24/10 21:30	3.0	762	5.6	0.2	19.1	703	36.7	1.4	19.9	654	38.2	1.4	0.4	579	0.7	0.0	795.0	29	1430.7	2.3
1/24/10 22:00	3.2	799	5.9	0.3	19.4	731	37.3	1.5	17.0	674	32.6	1.2	0.4	588	0.7	0.0	350.0	29	598.6	1.0
1/24/10 22:30	3.6	813	6.7	0.3	18.4	745	35.3	1.5	11.7	688	22.2	0.9	0.4	602	0.7	0.0	120.0	30	192.0	0.3

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/24/10 23:00	4.9	843	9.2	0.4	16.1	767	30.8	1.3	7.1	703	13.4	0.5	0.5	607	0.9	0.0	120.0	30	192.0	0.3
1/24/10 23:30	7.2	859	13.6	0.7	12.9	781	24.6	1.1	8.8	715	16.6	0.7	0.4	617	0.7	0.0	150.0	30	243.4	0.4
1/25/10 0:00	8.2	882	15.5	0.8	10.7	800	20.3	0.9	22.3	730	42.9	1.8	0.5	626	0.9	0.0	96.0	31	151.5	0.3
1/25/10 0:30	10.0	897	19.0	1.0	5.9	812	11.1	0.5	19.7	740	37.8	1.6	0.4	631	0.7	0.0	86.0	31	134.8	0.2
1/25/10 1:00	10.0	921	19.0	1.0	11.2	833	21.3	1.0	9.0	758	17.0	0.7	0.4	646	0.7	0.0	110.0	32	175.1	0.3
1/25/10 1:30	12.0	929	22.8	1.2	19.8	838	38.0	1.8	5.8	761	10.9	0.5	0.4	646	0.7	0.0	170.0	32	278.0	0.5
1/25/10 2:00	15.0	937	28.7	1.5	14.3	847	27.3	1.3	5.8	770	10.9	0.5	0.3	656	0.5	0.0	64.0	32	98.5	0.2
1/25/10 2:30	15.0	937	28.7	1.5	8.1	848	15.3	0.7	4.6	773	8.6	0.4	0.5	661	0.9	0.0	190.0	32	312.9	0.6
1/25/10 3:00	15.0	945	28.7	1.5	6.1	854	11.4	0.5	4.0	777	7.4	0.3	0.6	661	1.1	0.0	140.0	32	226.2	0.4
1/25/10 3:30	13.0	962	24.8	1.3	5.2	866	9.7	0.5	5.0	786	9.3	0.4	0.4	666	0.7	0.0	100.0	33	158.2	0.3
1/25/10 4:00	10.0	978	19.0	1.0	4.4	882	8.2	0.4	4.7	802	8.8	0.4	0.4	681	0.7	0.0	355.0	33	607.7	1.1
1/25/10 4:30	9.5	986	18.0	1.0	4.4	890	8.2	0.4	3.7	808	6.9	0.3	0.4	686	0.7	0.0	250.0	33	418.7	0.8
1/25/10 5:00	8.5	986	16.1	0.9	4.0	898	7.4	0.4	4.8	824	9.0	0.4	0.5	712	0.9	0.0	78.0	35	121.5	0.2
1/25/10 5:30	12.0	1020	22.8	1.3	4.2	922	7.8	0.4	4.9	840	9.2	0.4	0.5	717	0.9	0.0	88.0	35	138.1	0.3
1/25/10 6:00	13.0	1020	24.8	1.4	4.4	928	8.2	0.4	9.0	850	17.0	0.8	0.4	733	0.7	0.0	390.0	36	671.5	1.3
1/25/10 6:30	10.0	1048	19.0	1.1	5.8	950	10.9	0.6	12.1	867	23.0	1.1	0.4	744	0.7	0.0	490.0	36	855.7	1.7
1/25/10 7:00	7.5	1048	14.1	0.8	6.5	959	12.2	0.7	7.1	884	13.4	0.7	0.5	771	0.9	0.0	920.0	37	1670.7	3.5
1/25/10 7:30	6.6	1067	12.4	0.7	10.1	975	19.1	1.0	4.1	898	7.6	0.4	0.4	782	0.7	0.0	140.0	38	226.2	0.5
1/25/10 8:00	5.6	1086	10.5	0.6	9.5	995	18.0	1.0	7.3	919	13.7	0.7	0.5	804	0.9	0.0	67.0	39	103.4	0.2
1/25/10 8:30	5.7	1077	10.7	0.6	5.6	989	10.5	0.6	13.6	915	25.9	1.3	0.3	804	0.5	0.0	45.0	39	67.8	0.1
1/25/10 9:00	6.5	1115	12.2	0.8	6.2	1021	11.6	0.7	26.2	941	50.6	2.7	1.7	821	3.1	0.1	150.0	40	243.4	0.5
1/25/10 9:30	5.0	1125	9.3	0.6	9.6	1029	18.2	1.1	16.2	948	31.0	1.7	0.3	827	0.5	0.0	60.0	40	92.0	0.2
1/25/10 10:00	5.5	1145	10.3	0.7	18.3	1048	35.1	2.1	5.5	966	10.3	0.6	0.6	844	1.1	0.1	56.0	41	85.5	0.2
1/25/10 10:30	6.2	1155	11.6	0.8	18.6	1055	35.7	2.1	3.4	971	6.3	0.3	0.4	844	0.7	0.0	45.0	41	67.8	0.2
1/25/10 11:00	6.3	1165	11.8	0.8	9.7	1062	18.4	1.1	3.7	975	6.9	0.4	0.6	844	1.1	0.1	48.0	41	72.6	0.2
1/25/10 11:30	8.4	1206	15.9	1.1	4.4	1089	8.2	0.5	3.2	991	5.9	0.3	0.4	844	0.7	0.0	50.0	41	75.8	0.2
1/25/10 12:00	8.0	1175	15.1	1.0	3.5	1070	6.5	0.4	2.7	982	5.0	0.3	0.3	850	0.5	0.0	41.0	41	61.4	0.1
1/25/10 12:30	6.2	1216	11.6	0.8	3.7	1096	6.9	0.4	2.4	995	4.4	0.2	0.3	844	0.5	0.0	33.0	41	48.7	0.1
1/25/10 13:00	7.3	1227	13.7	0.9	3.2	1102	5.9	0.4	2.8	996	5.2	0.3	0.3	838	0.5	0.0	38.0	40	56.6	0.1
1/25/10 13:30	9.8	1237	18.6	1.3	3.1	1109	5.7	0.4	2.2	1000	4.0	0.2	0.3	838	0.5	0.0	26.0	40	37.8	0.1
1/25/10 14:00	14.0	1227	26.7	1.8	2.4	1098	4.4	0.3	2.0	989	3.7	0.2	0.4	827	0.7	0.0	29.0	40	42.5	0.1
1/25/10 14:30	12.0	1237	22.8	1.6	2.8	1103	5.2	0.3	2.2	990	4.0	0.2	0.5	821	0.9	0.0	32.0	40	47.2	0.1
1/25/10 15:00	7.5	1216	14.1	1.0	2.2	1089	4.0	0.2	1.6	982	2.9	0.2	0.3	821	0.5	0.0	68.0	40	105.0	0.2
1/25/10 15:30	5.0	1216	9.3	0.6	2.2	1087	4.0	0.2	1.6	978	2.9	0.2	0.5	815	0.9	0.0	32.0	39	47.2	0.1
1/25/10 16:00	4.6	1258	8.6	0.6	2.0	1112	3.7	0.2	1.6	989	2.9	0.2	0.5	804	0.9	0.0	64.0	39	98.5	0.2
1/25/10 16:30	4.7	1227	8.8	0.6	1.7	1089	3.1	0.2	1.4	973	2.6	0.1	0.4	798	0.7	0.0	32.0	39	47.2	0.1
1/25/10 17:00	4.8	1227	9.0	0.6	1.9	1089	3.5	0.2	2.0	973	3.7	0.2	0.3	798	0.5	0.0	28.0	39	40.9	0.1
1/25/10 17:30	3.7	1185	6.9	0.5	1.6	1059	2.9	0.2	1.9	953	3.5	0.2	0.3	793	0.5	0.0	20.0	38	28.6	0.1
1/25/10 18:00	3.3	1206	6.1	0.4	2.4	1069	4.4	0.3	2.2	954	4.0	0.2	0.3	782	0.5	0.0	21.0	38	30.2	0.1
1/25/10 18:30	3.4	1196	6.3	0.4	1.9	1059	3.5	0.2	1.7	944	3.1	0.2	0.4	771	0.7	0.0	20.0	37	28.6	0.1
1/25/10 19:00	3.2	1196	5.9	0.4	2.4	1059	4.4	0.3	1.5	944	2.7	0.1	0.3	771	0.5	0.0	22.0	37	31.7	0.1
1/25/10 19:30	3.2	1206	5.9	0.4	2.7	1061	5.0	0.3	1.6	938	2.9	0.2	0.3	754	0.5	0.0	18.0	37	25.6	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/25/10 20:00	2.9	1175	5.4	0.4	2.0	1042	3.7	0.2	1.1	929	2.0	0.1	0.3	760	0.5	0.0	21.0	37	30.2	0.1
1/25/10 20:30	3.0	1185	5.6	0.4	1.9	1047	3.5	0.2	1.5	930	2.7	0.1	0.3	754	0.5	0.0	16.0	37	22.6	0.0
1/25/10 21:00	2.9	1165	5.4	0.4	2.0	1028	3.7	0.2	1.7	912	3.1	0.2	0.3	738	0.5	0.0	17.0	36	24.1	0.0
1/25/10 21:30	3.0	1175	5.6	0.4	1.8	1033	3.3	0.2	1.3	913	2.4	0.1	0.3	733	0.5	0.0	16.0	36	22.6	0.0
1/25/10 22:00	3.0	1155	5.6	0.4	1.5	1019	2.7	0.2	1.3	905	2.4	0.1	0.3	733	0.5	0.0	18.0	36	25.6	0.1
1/25/10 22:30	2.7	1155	5.0	0.3	1.8	1016	3.3	0.2	1.2	898	2.2	0.1	0.3	722	0.5	0.0	17.0	35	24.1	0.0
1/25/10 23:00	3.2	1125	5.9	0.4	1.5	992	2.7	0.2	1.0	880	1.8	0.1	0.6	712	1.1	0.0	15.0	35	21.1	0.0
1/25/10 23:30	2.9	1125	5.4	0.3	2.2	992	4.0	0.2	1.1	880	2.0	0.1	0.4	712	0.7	0.0	14.0	35	19.6	0.0
1/26/10 00:00	2.9	1125	5.4	0.3	1.7	990	3.1	0.2	1.0	877	1.8	0.1	0.3	707	0.5	0.0	13.0	34	18.1	0.0
1/26/10 03:00	2.6	1115	4.8	0.3	3.1	982	5.7	0.3	1.2	870	2.2	0.1	0.3	702	0.5	0.0	14.0	34	19.6	0.0
1/26/10 1:00	2.8	1096	5.2	0.3	1.9	969	3.5	0.2	1.0	862	1.8	0.1	0.3	702	0.5	0.0	18.0	34	25.6	0.0
1/26/10 1:30	2.4	1086	4.4	0.3	1.9	957	3.5	0.2	1.0	849	1.8	0.1	0.3	686	0.5	0.0	14.0	33	19.6	0.0
1/26/10 2:00	2.3	1077	4.2	0.3	1.3	951	2.4	0.1	1.0	845	1.8	0.1	0.4	686	0.7	0.0	17.0	33	24.1	0.0
1/26/10 2:30	2.3	1077	4.2	0.3	1.3	946	2.4	0.1	1.5	836	2.7	0.1	0.3	671	0.5	0.0	12.0	33	16.6	0.0
1/26/10 3:00	2.5	1067	4.6	0.3	1.6	939	2.9	0.2	0.9	832	1.6	0.1	0.3	671	0.5	0.0	10.0	33	13.7	0.0
1/26/10 3:30	3.2	1086	5.9	0.4	1.3	954	2.4	0.1	0.9	843	1.6	0.1	0.3	676	0.5	0.0	12.0	33	16.6	0.0
1/26/10 4:00	2.6	1067	4.8	0.3	1.6	938	2.9	0.2	1.1	829	2.0	0.1	0.4	666	0.7	0.0	12.0	33	16.6	0.0
1/26/10 4:30	2.2	1067	4.0	0.2	1.4	938	2.6	0.1	0.9	829	1.6	0.1	0.2	666	0.4	0.0	9.0	33	12.3	0.0
1/26/10 5:00	2.7	1048	5.0	0.3	2.3	920	4.2	0.2	1.3	812	2.4	0.1	0.3	651	0.5	0.0	9.1	32	12.4	0.0
1/26/10 5:30	2.3	1048	4.2	0.2	1.5	920	2.7	0.1	1.0	812	1.8	0.1	0.3	651	0.5	0.0	8.7	32	11.8	0.0
1/26/10 6:00	2.6	1029	4.8	0.3	1.5	907	2.7	0.1	1.7	805	3.1	0.1	0.3	651	0.5	0.0	10.0	32	13.7	0.0
1/26/10 6:30	2.2	1039	4.0	0.2	1.6	912	2.9	0.1	0.8	806	1.4	0.1	0.4	646	0.7	0.0	16.0	32	22.6	0.0
1/26/10 7:00	2.2	1029	4.0	0.2	1.5	903	2.7	0.1	1.0	796	1.8	0.1	0.5	636	0.9	0.0	140.0	31	226.2	0.4
1/26/10 7:30	2.2	1020	4.0	0.2	1.4	898	2.6	0.1	0.8	795	1.4	0.1	0.3	641	0.5	0.0	71.0	31	110.0	0.2
1/26/10 8:00	2.8	1039	5.2	0.3	2.0	909	3.7	0.2	0.9	799	1.6	0.1	0.3	635	0.5	0.0	36.0	31	53.5	0.1
1/26/10 8:30	2.1	1012	3.9	0.2	2.0	888	3.7	0.2	0.7	785	1.3	0.1	0.3	629	0.5	0.0	35.0	31	51.9	0.1
1/26/10 9:00	2.3	1012	4.2	0.2	1.4	886	2.6	0.1	1.3	780	2.4	0.1	0.2	622	0.4	0.0	43.0	31	64.6	0.1
1/26/10 9:30	2.0	1003	3.7	0.2	1.5	880	2.7	0.1	2.9	777	5.4	0.2	0.3	622	0.5	0.0	56.0	31	85.5	0.1
1/26/10 10:00	2.1	978	3.9	0.2	1.7	860	3.1	0.2	2.8	761	5.2	0.2	0.3	612	0.5	0.0	32.0	30	47.2	0.1
1/26/10 10:30	2.6	978	4.8	0.3	2.2	860	4.0	0.2	1.8	761	3.3	0.1	0.3	612	0.5	0.0	30.0	30	44.0	0.1
1/26/10 11:00	2.0	978	3.7	0.2	3.6	859	6.7	0.3	1.7	758	3.1	0.1	0.3	607	0.5	0.0	24.0	30	34.8	0.1
1/26/10 11:30	2.3	978	4.2	0.2	2.9	859	5.4	0.3	1.5	758	2.7	0.1	0.3	607	0.5	0.0	19.0	30	27.1	0.0
1/26/10 12:00	2.0	986	3.7	0.2	2.3	861	4.2	0.2	1.9	756	3.5	0.1	0.3	598	0.5	0.0	17.0	29	24.1	0.0
1/26/10 12:30	2.1	970	3.9	0.2	2.7	849	5.0	0.2	1.4	746	2.6	0.1	0.3	593	0.5	0.0	18.0	29	25.6	0.0
1/26/10 13:00	1.9	962	3.5	0.2	2.8	841	5.2	0.2	1.4	740	2.6	0.1	0.3	588	0.5	0.0	14.0	29	19.6	0.0
1/26/10 13:30	2.1	953	3.9	0.2	2.7	836	5.0	0.2	1.3	737	2.4	0.1	0.3	588	0.5	0.0	12.0	29	16.6	0.0
1/26/10 14:00	2.0	953	3.7	0.2	2.0	834	3.7	0.2	1.1	734	2.0	0.1	0.3	584	0.5	0.0	15.0	29	21.1	0.0
1/26/10 14:30	2.7	937	5.0	0.3	1.9	822	3.5	0.2	1.1	725	2.0	0.1	0.2	579	0.4	0.0	18.0	29	25.6	0.0
1/26/10 15:00	2.8	945	5.2	0.3	2.1	826	3.9	0.2	1.0	725	1.8	0.1	0.3	575	0.5	0.0	23.0	28	33.2	0.1
1/26/10 15:30	3.2	945	5.9	0.3	1.7	826	3.1	0.1	1.1	725	2.0	0.1	0.2	575	0.4	0.0	20.0	28	28.6	0.0
1/26/10 16:00	3.5	921	6.5	0.3	1.9	808	3.5	0.2	0.7	713	1.3	0.1	0.5	570	0.9	0.0	16.0	28	22.6	0.0
1/26/10 16:30	2.6	929	4.8	0.3	1.8	813	3.3	0.2	0.8	716	1.4	0.1	0.3	570	0.5	0.0	25.0	28	36.3	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/26/10 17:00	2.8	921	5.2	0.3	1.7	805	3.1	0.1	0.9	707	1.6	0.1	0.3	561	0.5	0.0	16.0	28	22.6	0.0
1/26/10 17:30	2.5	897	4.6	0.2	1.9	789	3.5	0.2	1.0	698	1.8	0.1	0.4	561	0.7	0.0	17.0	28	24.1	0.0
1/26/10 18:00	2.4	913	4.4	0.2	1.7	798	3.1	0.1	1.2	702	2.2	0.1	0.3	556	0.5	0.0	18.0	27	25.6	0.0
1/26/10 18:30	2.6	913	4.8	0.2	1.9	798	3.5	0.2	1.0	702	1.8	0.1	0.4	556	0.7	0.0	12.0	27	16.6	0.0
1/26/10 19:00	2.4	890	4.4	0.2	2.3	781	4.2	0.2	1.0	689	1.8	0.1	0.3	552	0.5	0.0	12.0	27	16.6	0.0
1/26/10 19:30	2.6	905	4.8	0.2	2.0	790	3.7	0.2	0.9	693	1.6	0.1	0.3	547	0.5	0.0	10.0	27	13.7	0.0
1/26/10 20:00	2.3	890	4.2	0.2	1.9	779	3.5	0.2	0.9	687	1.6	0.1	0.2	547	0.4	0.0	10.0	27	13.7	0.0
1/26/10 20:30	1.9	897	3.5	0.2	2.3	782	4.2	0.2	0.9	684	1.6	0.1	0.3	539	0.5	0.0	14.0	27	19.6	0.0
1/26/10 21:00	1.9	890	3.5	0.2	2.1	775	3.9	0.2	0.9	679	1.6	0.1	0.2	534	0.4	0.0	9.2	26	12.6	0.0
1/26/10 21:30	2.0	890	3.7	0.2	1.9	775	3.5	0.2	0.7	679	1.3	0.0	0.3	534	0.5	0.0	9.0	26	12.3	0.0
1/26/10 22:00	1.9	874	3.5	0.2	2.0	763	3.7	0.2	0.7	670	1.3	0.0	0.3	530	0.5	0.0	11.0	26	15.2	0.0
1/26/10 22:30	2.0	882	3.7	0.2	1.8	768	3.3	0.1	0.7	673	1.3	0.0	0.4	530	0.7	0.0	9.6	26	13.1	0.0
1/26/10 23:00	1.9	874	3.5	0.2	1.9	762	3.5	0.1	0.8	667	1.4	0.1	0.4	525	0.7	0.0	9.0	26	12.3	0.0
1/26/10 23:30	2.1	874	3.9	0.2	1.8	762	3.3	0.1	0.7	667	1.3	0.0	0.3	525	0.5	0.0	6.8	26	9.1	0.0
1/27/10 0:00	2.0	866	3.7	0.2	1.9	756	3.5	0.1	0.7	664	1.3	0.0	0.2	525	0.4	0.0	7.8	26	10.5	0.0
1/27/10 0:30	2.0	851	3.7	0.2	1.8	743	3.3	0.1	0.8	653	1.4	0.1	0.4	517	0.7	0.0	12.0	26	16.6	0.0
1/27/10 1:00	2.1	859	3.9	0.2	1.8	748	3.3	0.1	0.7	656	1.3	0.0	0.3	517	0.5	0.0	12.0	26	16.6	0.0
1/27/10 1:30	2.1	859	3.9	0.2	2.0	746	3.7	0.2	0.7	651	1.3	0.0	0.3	508	0.5	0.0	7.8	25	10.5	0.0
1/27/10 2:00	2.1	843	3.9	0.2	1.9	735	3.5	0.1	0.7	644	1.3	0.0	0.3	508	0.5	0.0	6.8	25	9.1	0.0
1/27/10 2:30	2.2	836	4.0	0.2	1.9	730	3.5	0.1	0.7	641	1.3	0.0	0.4	508	0.7	0.0	6.9	25	9.2	0.0
1/27/10 3:00	2.1	843	3.9	0.2	1.9	734	3.5	0.1	0.6	642	1.1	0.0	0.2	504	0.4	0.0	10.0	25	13.7	0.0
1/27/10 3:30	1.8	836	3.3	0.2	1.7	729	3.1	0.1	0.7	639	1.3	0.0	0.3	504	0.5	0.0	8.7	25	11.8	0.0
1/27/10 4:00	2.0	828	3.7	0.2	1.9	722	3.5	0.1	0.6	633	1.1	0.0	0.2	500	0.4	0.0	6.7	25	9.0	0.0
1/27/10 4:30	1.8	828	3.3	0.2	1.9	721	3.5	0.1	1.4	631	2.6	0.1	0.3	495	0.5	0.0	6.3	25	8.4	0.0
1/27/10 5:00	2.0	836	3.7	0.2	1.8	726	3.3	0.1	0.9	634	1.6	0.1	0.3	495	0.5	0.0	7.9	25	10.7	0.0
1/27/10 5:30	1.9	828	3.5	0.2	1.7	720	3.1	0.1	0.7	628	1.3	0.0	0.3	491	0.5	0.0	8.3	24	11.3	0.0
1/27/10 6:00	2.1	821	3.9	0.2	1.7	713	3.1	0.1	0.8	623	1.4	0.1	0.3	487	0.5	0.0	6.5	24	8.7	0.0
1/27/10 6:30	1.8	806	3.3	0.1	1.9	702	3.5	0.1	0.8	614	1.4	0.0	0.3	483	0.5	0.0	7.4	24	10.0	0.0
1/27/10 7:00	2.0	813	3.7	0.2	1.7	708	3.1	0.1	0.6	620	1.1	0.0	0.2	487	0.4	0.0	7.4	24	10.0	0.0
1/27/10 7:30	2.0	813	3.7	0.2	2.0	707	3.7	0.1	0.9	617	1.6	0.1	0.2	483	0.4	0.0	5.3	24	7.0	0.0
1/27/10 8:00	2.0	806	3.7	0.2	1.7	701	3.1	0.1	0.6	612	1.1	0.0	0.2	479	0.4	0.0	6.0	24	8.0	0.0
1/27/10 8:30	2.0	791	3.7	0.2	1.7	689	3.1	0.1	0.6	603	1.1	0.0	0.3	475	0.5	0.0	4.8	24	6.3	0.0
1/27/10 9:00	2.0	799	3.7	0.2	1.9	694	3.5	0.1	0.8	606	1.4	0.0	0.2	475	0.4	0.0	7.4	24	10.0	0.0
1/27/10 9:30	1.8	791	3.3	0.1	1.5	688	2.7	0.1	0.6	601	1.1	0.0	0.3	471	0.5	0.0	5.1	23	6.7	0.0
1/27/10 10:00	2.0	799	3.7	0.2	1.5	693	2.7	0.1	0.9	604	1.6	0.1	0.2	471	0.4	0.0	6.5	23	8.7	0.0
1/27/10 10:30	2.0	784	3.7	0.2	1.8	682	3.3	0.1	0.6	596	1.1	0.0	0.3	467	0.5	0.0	4.9	23	6.4	0.0
1/27/10 11:00	2.0	784	3.7	0.2	1.7	682	3.1	0.1	0.6	596	1.1	0.0	0.2	467	0.4	0.0	6.6	23	8.8	0.0
1/27/10 11:30	1.8	784	3.3	0.1	2.5	681	4.5	0.2	0.7	593	1.3	0.0	0.2	462	0.4	0.0	5.5	23	7.3	0.0
1/27/10 12:00	1.9	770	3.5	0.2	3.2	671	5.9	0.2	0.7	587	1.3	0.0	0.3	462	0.5	0.0	4.0	23	5.2	0.0
1/27/10 12:30	2.0	777	3.7	0.2	1.6	674	2.9	0.1	1.1	588	2.0	0.1	0.2	458	0.4	0.0	4.5	23	5.9	0.0
1/27/10 13:00	1.9	770	3.5	0.2	1.5	669	2.7	0.1	0.5	585	0.9	0.0	0.3	458	0.5	0.0	4.6	23	6.0	0.0
1/27/10 13:30	1.9	777	3.5	0.2	2.0	672	3.7	0.1	0.6	583	1.1	0.0	0.3	450	0.5	0.0	4.8	23	6.3	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/27/10 14:00	2.0	762	3.7	0.2	1.6	663	2.9	0.1	0.7	580	1.3	0.0	0.2	454	0.4	0.0	5.1	23	6.7	0.0
1/27/10 14:30	2.2	762	4.0	0.2	1.6	662	2.9	0.1	0.6	577	1.1	0.0	0.3	450	0.5	0.0	4.3	23	5.6	0.0
1/27/10 15:00	1.8	755	3.3	0.1	1.6	657	2.9	0.1	0.6	575	1.1	0.0	0.2	450	0.4	0.0	4.2	23	5.5	0.0
1/27/10 15:30	1.8	762	3.3	0.1	1.5	661	2.7	0.1	0.8	575	1.4	0.0	0.3	447	0.5	0.0	4.5	22	5.9	0.0
1/27/10 16:00	1.8	755	3.3	0.1	1.6	656	2.9	0.1	0.8	572	1.4	0.0	0.3	447	0.5	0.0	3.8	22	4.9	0.0
1/27/10 16:30	2.0	755	3.7	0.2	1.7	656	3.1	0.1	0.6	572	1.1	0.0	0.3	447	0.5	0.0	3.3	22	4.2	0.0
1/27/10 17:00	2.0	748	3.7	0.2	1.6	650	2.9	0.1	0.7	567	1.3	0.0	0.2	443	0.4	0.0	2.3	22	2.9	0.0
1/27/10 17:30	2.1	741	3.9	0.2	1.7	645	3.1	0.1	0.5	564	0.9	0.0	0.3	443	0.5	0.0	3.4	22	4.4	0.0
1/27/10 18:00	2.0	748	3.7	0.2	1.7	649	3.1	0.1	0.5	565	0.9	0.0	0.2	439	0.4	0.0	4.2	22	5.5	0.0
1/27/10 18:30	2.0	748	3.7	0.2	1.7	647	3.1	0.1	0.6	562	1.1	0.0	0.3	435	0.5	0.0	3.8	22	4.9	0.0
1/27/10 19:00	1.9	741	3.5	0.1	1.9	643	3.5	0.1	0.4	559	0.7	0.0	0.2	435	0.4	0.0	3.1	22	4.0	0.0
1/27/10 19:30	1.8	727	3.3	0.1	2.1	629	3.9	0.1	0.4	547	0.7	0.0	0.3	423	0.5	0.0	4.9	21	6.4	0.0
1/27/10 20:00	1.9	741	3.5	0.1	2.3	641	4.2	0.2	0.8	557	1.4	0.0	0.2	431	0.4	0.0	2.7	22	3.4	0.0
1/27/10 20:30	2.0	734	3.7	0.2	1.9	635	3.5	0.1	0.7	552	1.3	0.0	0.6	427	1.1	0.0	3.8	21	4.9	0.0
1/27/10 21:00	1.9	727	3.5	0.1	2.1	629	3.9	0.1	0.6	547	1.1	0.0	0.3	423	0.5	0.0	3.3	21	4.2	0.0
1/27/10 21:30	1.9	720	3.5	0.1	1.7	625	3.1	0.1	0.7	544	1.3	0.0	0.3	423	0.5	0.0	3.8	21	4.9	0.0
1/27/10 22:00	1.6	727	2.9	0.1	1.6	629	2.9	0.1	0.5	547	0.9	0.0	0.3	423	0.5	0.0	2.4	21	3.0	0.0
1/27/10 22:30	2.3	720	4.2	0.2	1.6	623	2.9	0.1	0.5	542	0.9	0.0	0.2	419	0.4	0.0	3.5	21	4.5	0.0
1/27/10 23:00	1.9	720	3.5	0.1	1.7	623	3.1	0.1	0.9	542	1.6	0.0	0.3	419	0.5	0.0	2.3	21	2.9	0.0
1/27/10 23:30	1.9	720	3.5	0.1	1.7	622	3.1	0.1	0.6	540	1.1	0.0	0.2	416	0.4	0.0	3.1	21	4.0	0.0
1/28/10 0:00	1.7	707	3.1	0.1	2.2	613	4.0	0.1	0.6	534	1.1	0.0	0.5	416	0.9	0.0	4.2	21	5.5	0.0
1/28/10 0:30	2.0	707	3.7	0.1	1.8	612	3.3	0.1	0.5	532	0.9	0.0	0.4	412	0.7	0.0	2.5	21	3.1	0.0
1/28/10 1:00	3.1	707	5.7	0.2	1.5	611	2.7	0.1	0.6	530	1.1	0.0	0.3	408	0.5	0.0	2.8	21	3.5	0.0
1/28/10 1:30	1.9	707	3.5	0.1	1.7	609	3.1	0.1	0.6	527	0.9	0.0	0.3	404	0.5	0.0	3.8	20	4.9	0.0
1/28/10 2:00	1.9	700	3.5	0.1	1.9	606	3.5	0.1	0.6	527	1.1	0.0	0.2	408	0.4	0.0	3.7	21	4.8	0.0
1/28/10 2:30	1.9	693	3.5	0.1	3.0	600	5.6	0.2	0.7	522	1.3	0.0	0.2	404	0.4	0.0	2.4	20	3.0	0.0
1/28/10 3:00	2.0	700	3.7	0.1	2.1	605	3.9	0.1	0.7	525	1.3	0.0	0.3	404	0.5	0.0	2.2	20	2.7	0.0
1/28/10 3:30	1.9	693	3.5	0.1	1.9	600	3.5	0.1	0.5	522	0.9	0.0	0.2	404	0.4	0.0	3.0	20	3.8	0.0
1/28/10 4:00	1.7	693	3.1	0.1	2.0	599	3.7	0.1	0.5	520	0.9	0.0	0.3	401	0.5	0.0	2.0	20	2.5	0.0
1/28/10 4:30	1.7	686	3.1	0.1	1.6	593	2.9	0.1	0.5	515	0.9	0.0	1.8	397	3.3	0.1	2.0	20	2.5	0.0
1/28/10 5:00	1.8	693	3.3	0.1	1.6	598	2.9	0.1	0.4	517	0.7	0.0	0.2	397	0.4	0.0	2.8	20	3.5	0.0
1/28/10 5:30	1.7	686	3.1	0.1	1.7	593	3.1	0.1	0.5	515	0.9	0.0	0.2	397	0.4	0.0	2.3	20	2.9	0.0
1/28/10 6:00	1.7	693	3.1	0.1	2.0	598	3.7	0.1	0.6	517	1.1	0.0	0.2	397	0.4	0.0	1.8	20	2.2	0.0
1/28/10 6:30	1.7	680	3.1	0.1	1.7	588	3.1	0.1	0.6	510	1.1	0.0	0.4	393	0.7	0.0	2.4	20	3.0	0.0
1/28/10 7:00	1.7	680	3.1	0.1	1.7	586	3.1	0.1	0.4	508	0.7	0.0	0.2	390	0.4	0.0	2.4	20	3.0	0.0
1/28/10 7:30	1.9	673	3.5	0.1	1.7	582	3.1	0.1	0.4	505	0.7	0.0	0.2	390	0.4	0.0	2.6	20	3.3	0.0
1/28/10 8:00	1.9	667	3.5	0.1	3.1	577	5.7	0.2	0.5	502	0.9	0.0	0.2	390	0.4	0.0	2.8	20	3.5	0.0
1/28/10 8:30	1.8	667	3.3	0.1	1.6	576	2.9	0.1	0.5	500	0.9	0.0	0.3	386	0.5	0.0	2.7	19	3.4	0.0
1/28/10 9:00	1.9	673	3.5	0.1	1.7	580	3.1	0.1	0.6	501	1.1	0.0	0.2	382	0.4	0.0	2.7	19	3.4	0.0
1/28/10 9:30	1.8	667	3.3	0.1	2.2	575	4.0	0.1	0.6	498	1.1	0.0	0.3	382	0.5	0.0	2.1	19	2.6	0.0
1/28/10 10:00	1.7	660	3.1	0.1	1.7	571	3.1	0.1	0.4	495	0.7	0.0	0.2	382	0.4	0.0	2.7	19	3.4	0.0
1/28/10 10:30	1.9	660	3.5	0.1	1.7	571	3.1	0.1	0.6	495	1.1	0.0	0.3	382	0.5	0.0	2.3	19	2.9	0.0

Date & Time	Station 1					Station 2					Station 3					Station 4					Station 5				
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)		Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)		Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)		Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)		Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	
1/28/10 11:00	1.9	660	3.5	0.1		1.7	571	3.1	0.1		0.5	495	0.9	0.0		0.2	382	0.4	0.0		1.9	19	2.4	0.0	
1/28/10 11:30	1.6	660	2.9	0.1		1.9	569	3.5	0.1		0.6	493	1.1	0.0		0.2	379	0.4	0.0		2.0	19	2.5	0.0	
1/28/10 12:00	1.8	660	3.3	0.1		1.9	569	3.5	0.1		0.4	493	0.7	0.0		0.5	379	0.9	0.0		2.3	19	2.9	0.0	
1/28/10 12:30	1.8	653	3.3	0.1		1.7	564	3.1	0.1		0.4	488	0.7	0.0		0.2	375	0.4	0.0		1.7	19	2.1	0.0	
1/28/10 13:00	1.8	653	3.3	0.1		2.1	563	3.9	0.1		0.4	486	0.7	0.0		0.2	372	0.4	0.0		1.7	19	2.1	0.0	
1/28/10 13:30	1.6	653	2.9	0.1		1.8	563	3.3	0.1		0.5	486	0.9	0.0		0.3	372	0.5	0.0		2.0	19	2.5	0.0	
1/28/10 14:00	1.8	647	3.3	0.1		2.0	558	3.7	0.1		0.5	484	0.9	0.0		0.2	372	0.4	0.0		2.9	19	3.7	0.0	
1/28/10 14:30	1.7	647	3.1	0.1		2.3	558	4.2	0.1		0.4	484	0.7	0.0		0.2	372	0.4	0.0		2.0	19	2.5	0.0	
1/28/10 15:00	1.8	647	3.3	0.1		2.0	557	3.7	0.1		0.7	482	1.3	0.0		0.3	368	0.5	0.0		1.9	19	2.4	0.0	
1/28/10 15:30	1.5	641	2.7	0.1		2.0	553	3.7	0.1		0.5	479	0.9	0.0		0.2	368	0.4	0.0		1.9	19	2.4	0.0	
1/28/10 16:00	2.0	641	3.7	0.1		2.0	553	3.7	0.1		0.4	479	0.7	0.0		0.2	368	0.4	0.0		2.8	19	3.5	0.0	
1/28/10 16:30	1.8	641	3.3	0.1		2.3	552	4.2	0.1		0.4	477	0.7	0.0		0.2	365	0.4	0.0		3.6	18	4.6	0.0	
1/28/10 17:00	1.9	635	3.5	0.1		2.2	548	4.0	0.1		0.9	475	1.6	0.0		0.2	365	0.4	0.0		2.5	18	3.1	0.0	
1/28/10 17:30	2.2	641	4.0	0.1		2.4	551	4.4	0.1		0.4	475	0.7	0.0		0.2	361	0.4	0.0		3.6	18	4.6	0.0	
1/28/10 18:00	1.6	635	2.9	0.1		2.3	547	4.2	0.1		1.1	473	2.0	0.1		0.2	361	0.4	0.0		2.4	18	3.0	0.0	
1/28/10 18:30	1.7	635	3.1	0.1		2.3	547	4.2	0.1		0.4	473	0.7	0.0		0.3	361	0.5	0.0		2.2	18	2.7	0.0	
1/28/10 19:00	1.7	635	3.1	0.1		2.5	547	4.6	0.1		0.4	473	0.7	0.0		0.2	361	0.4	0.0		2.0	18	2.5	0.0	
1/28/10 19:30	1.6	629	2.9	0.1		2.4	542	4.4	0.1		0.4	468	0.7	0.0		0.3	358	0.5	0.0		2.2	18	2.7	0.0	
1/28/10 20:00	1.9	623	3.5	0.1		2.3	537	4.2	0.1		0.4	466	0.7	0.0		0.3	358	0.5	0.0		2.7	18	3.4	0.0	
1/28/10 20:30	1.9	629	3.5	0.1		2.4	540	4.4	0.1		0.6	466	1.1	0.0		0.3	354	0.5	0.0		1.9	18	2.4	0.0	
1/28/10 21:00	1.6	623	2.9	0.1		2.4	536	4.4	0.1		0.4	464	0.7	0.0		0.2	354	0.4	0.0		2.1	18	2.6	0.0	
1/28/10 21:30	1.6	629	2.9	0.1		2.5	540	4.6	0.1		0.4	466	0.7	0.0		0.2	354	0.4	0.0		1.6	18	2.0	0.0	
1/28/10 22:00	1.7	623	3.1	0.1		2.6	535	4.8	0.1		0.6	461	1.1	0.0		0.3	351	0.5	0.0		2.4	18	3.0	0.0	
1/28/10 22:30	1.9	611	3.5	0.1		2.8	526	5.2	0.2		0.6	455	1.1	0.0		0.2	347	0.4	0.0		2.1	18	2.6	0.0	
1/28/10 23:00	1.8	617	3.3	0.1		2.8	530	5.2	0.2		1.3	457	2.4	0.1		0.3	347	0.5	0.0		1.4	18	1.7	0.0	
1/28/10 23:30	1.7	617	3.1	0.1		2.4	530	4.4	0.1		0.6	457	1.1	0.0		0.3	347	0.5	0.0		1.9	18	2.4	0.0	
1/29/10 0:00	1.9	617	3.5	0.1		2.5	530	4.6	0.1		0.5	457	0.9	0.0		0.3	347	0.5	0.0		3.1	18	4.0	0.0	
1/29/10 0:30	1.8	611	3.3	0.1		2.5	525	4.6	0.1		0.9	453	1.6	0.0		0.2	344	0.4	0.0		2.3	17	2.9	0.0	
1/29/10 1:00	1.8	605	3.3	0.1		2.5	521	4.6	0.1		0.6	450	1.1	0.0		0.5	344	0.9	0.0		1.7	17	2.1	0.0	
1/29/10 1:30	1.9	611	3.5	0.1		2.7	524	5.0	0.1		0.6	451	1.1	0.0		0.2	341	0.4	0.0		1.9	17	2.4	0.0	
1/29/10 2:00	1.7	605	3.1	0.1		2.7	520	5.0	0.1		0.5	448	0.9	0.0		0.2	341	0.4	0.0		1.4	17	1.7	0.0	
1/29/10 2:30	1.9	605	3.5	0.1		2.7	520	5.0	0.1		0.5	448	0.9	0.0		0.2	341	0.4	0.0		1.6	17	2.0	0.0	
1/29/10 3:00	1.7	605	3.1	0.1		2.5	519	4.6	0.1		0.5	446	0.9	0.0		0.2	337	0.4	0.0		2.5	17	3.1	0.0	
1/29/10 3:30	1.8	599	3.3	0.1		2.5	515	4.6	0.1		0.6	444	1.1	0.0		0.2	337	0.4	0.0		1.1	17	1.3	0.0	
1/29/10 4:00	1.9	605	3.5	0.1		2.4	519	4.4	0.1		0.5	446	0.9	0.0		0.3	337	0.5	0.0		2.8	17	3.5	0.0	
1/29/10 4:30	1.9	605	3.5	0.1		2.9	518	5.4	0.2		0.4	444	0.7	0.0		0.5	334	0.9	0.0		1.4	17	1.7	0.0	
1/29/10 5:00	1.9	593	3.5	0.1		3.6	510	6.7	0.2		0.4	440	0.7	0.0		0.2	334	0.4	0.0		1.3	17	1.6	0.0	
1/29/10 5:30	1.6	593	2.9	0.1		2.7	510	5.0	0.1		0.5	440	0.9	0.0		0.2	334	0.4	0.0		1.6	17	2.0	0.0	
1/29/10 6:00	1.6	593	2.9	0.1		2.6	510	4.8	0.1		0.6	440	1.1	0.0		0.3	334	0.5	0.0		4.2	17	5.5	0.0	
1/29/10 6:30	1.8	588	3.3	0.1		2.8	506	5.2	0.1		0.5	437	0.9	0.0		0.3	334	0.5	0.0		1.4	17	1.7	0.0	
1/29/10 7:00	1.9	588	3.5	0.1		2.5	505	4.6	0.1		0.5	435	0.9	0.0		0.3	331	0.5	0.0		1.4	17	1.7	0.0	
1/29/10 7:30	2.5	588	4.6	0.2		2.9	505	5.4	0.2		0.4	435	0.7	0.0		0.2	331	0.4	0.0		1.7	17	2.1	0.0	

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/29/10 8:00	1.7	582	3.1	0.1	2.7	501	5.0	0.1	0.6	433	1.1	0.0	0.2	331	0.4	0.0	2.4	17	3.0	0.0
1/29/10 8:30	1.8	582	3.3	0.1	2.7	500	5.0	0.1	0.4	431	0.7	0.0	0.3	327	0.5	0.0	2.1	17	2.6	0.0
1/29/10 9:00	1.7	576	3.1	0.1	2.7	496	5.0	0.1	0.4	429	0.7	0.0	0.2	327	0.4	0.0	1.7	17	2.1	0.0
1/29/10 9:30	1.7	576	3.1	0.1	2.8	495	5.2	0.1	0.5	427	0.9	0.0	0.2	324	0.4	0.0	1.5	324	1.8	0.0
1/29/10 10:00	1.8	576	3.3	0.1	2.8	495	5.2	0.1	0.4	427	0.7	0.0	0.2	324	0.4	0.0	0.8	17	0.9	0.0
1/29/10 10:30	1.7	582	3.1	0.1	2.8	499	5.2	0.1	0.5	429	0.9	0.0	0.3	324	0.5	0.0	1.1	17	1.3	0.0
1/29/10 11:00	1.6	570	2.9	0.1	3.4	491	6.3	0.2	0.4	424	0.7	0.0	0.3	324	0.5	0.0	0.9	17	1.1	0.0
1/29/10 11:30	1.8	576	3.3	0.1	3.0	495	5.6	0.2	0.4	427	0.7	0.0	0.3	324	0.5	0.0	2.8	17	3.5	0.0
1/29/10 12:00	1.7	570	3.1	0.1	2.7	491	5.0	0.1	0.5	424	0.9	0.0	0.2	324	0.4	0.0	1.3	17	1.6	0.0
1/29/10 12:30	1.7	576	3.1	0.1	2.8	495	5.2	0.1	0.5	427	0.9	0.0	0.3	324	0.5	0.0	2.4	17	3.0	0.0
1/29/10 13:00	2.0	570	3.7	0.1	2.8	491	5.2	0.1	0.4	424	0.7	0.0	1.2	324	2.2	0.0	4.4	17	5.7	0.0
1/29/10 13:30	1.9	570	3.5	0.1	3.0	491	5.6	0.2	0.4	424	0.7	0.0	0.3	324	0.5	0.0	15.0	17	21.1	0.0
1/29/10 14:00	2.1	570	3.9	0.1	3.0	490	5.6	0.2	0.4	422	0.7	0.0	0.3	321	0.5	0.0	12.0	16	16.6	0.0
1/29/10 14:30	1.7	570	3.1	0.1	3.0	490	5.6	0.2	0.4	422	0.7	0.0	0.3	321	0.5	0.0	5.3	16	7.0	0.0
1/29/10 15:00	1.7	565	3.1	0.1	3.0	486	5.6	0.2	0.4	420	0.7	0.0	0.2	321	0.5	0.0	6.1	16	8.1	0.0
1/29/10 15:30	1.8	559	3.3	0.1	2.9	482	5.4	0.1	0.4	418	0.7	0.0	0.2	321	0.4	0.0	4.7	16	6.2	0.0
1/29/10 16:00	1.5	559	2.7	0.1	3.1	481	5.7	0.2	0.6	416	1.1	0.0	0.3	318	0.5	0.0	7.8	16	10.5	0.0
1/29/10 16:30	1.8	565	3.3	0.1	3.1	485	5.7	0.2	0.4	418	0.7	0.0	0.2	318	0.4	0.0	3.9	16	5.0	0.0
1/29/10 17:00	1.7	559	3.1	0.1	3.0	481	5.6	0.2	0.6	416	1.1	0.0	1.0	318	1.8	0.0	2.5	16	3.1	0.0
1/29/10 17:30	1.7	559	3.1	0.1	3.1	481	5.7	0.2	0.7	416	1.3	0.0	0.3	318	0.5	0.0	2.5	16	3.1	0.0
1/29/10 18:00	2.1	559	3.9	0.1	3.0	480	5.6	0.1	0.7	414	1.3	0.0	0.2	314	0.4	0.0	1.7	16	2.1	0.0
1/29/10 18:30	1.7	559	3.1	0.1	3.5	480	6.5	0.2	0.6	414	1.1	0.0	0.3	314	0.5	0.0	2.0	16	2.5	0.0
1/29/10 19:00	1.5	559	2.7	0.1	3.2	480	5.9	0.2	0.6	414	1.1	0.0	0.3	314	0.5	0.0	2.2	16	2.7	0.0
1/29/10 19:30	1.9	559	3.5	0.1	3.6	480	6.7	0.2	0.6	414	1.1	0.0	0.2	314	0.4	0.0	3.2	16	4.1	0.0
1/29/10 20:00	1.7	553	3.1	0.1	3.2	475	5.9	0.2	0.6	410	1.1	0.0	0.4	311	0.7	0.0	3.6	16	4.6	0.0
1/29/10 20:30	1.9	553	3.5	0.1	3.4	475	6.3	0.2	0.5	410	0.9	0.0	0.3	311	0.5	0.0	3.9	16	5.0	0.0
1/29/10 21:00	2.0	553	3.7	0.1	3.5	475	6.5	0.2	0.6	410	1.1	0.0	0.2	311	0.4	0.0	6.2	16	8.3	0.0
1/29/10 21:30	1.7	553	3.1	0.1	3.3	475	6.1	0.2	0.6	410	1.1	0.0	0.5	311	0.9	0.0	13.0	16	18.1	0.0
1/29/10 22:00	1.6	548	2.9	0.1	3.5	472	6.5	0.2	1.0	408	1.8	0.0	0.3	311	0.5	0.0	20.0	16	28.6	0.0
1/29/10 22:30	2.5	553	4.6	0.1	3.3	474	6.1	0.2	0.5	408	0.9	0.0	0.2	308	0.4	0.0	7.0	16	9.4	0.0
1/29/10 23:00	1.7	548	3.1	0.1	3.5	471	6.5	0.2	0.6	406	1.1	0.0	0.3	308	0.5	0.0	5.0	16	6.6	0.0
1/29/10 23:30	1.9	553	3.5	0.1	3.3	474	6.1	0.2	0.5	408	0.9	0.0	1.0	308	1.8	0.0	10.0	16	13.7	0.0
1/30/10 0:00	1.6	553	2.9	0.1	3.3	474	6.1	0.2	0.6	408	1.1	0.0	0.3	308	0.5	0.0	5.1	16	6.7	0.0
1/30/10 0:30	1.9	553	3.5	0.1	3.5	474	6.5	0.2	0.4	408	0.7	0.0	0.4	308	0.7	0.0	4.6	16	6.0	0.0
1/30/10 1:00	1.9	548	3.5	0.1	5.0	471	9.3	0.2	0.7	406	1.3	0.0	0.2	308	0.4	0.0	3.1	16	4.0	0.0
1/30/10 1:30	1.7	548	3.1	0.1	3.3	471	6.1	0.2	0.7	406	1.3	0.0	0.3	308	0.5	0.0	4.8	16	6.3	0.0
1/30/10 2:00	1.9	553	3.5	0.1	3.5	474	6.5	0.2	0.8	408	1.4	0.0	0.3	308	0.5	0.0	14.0	16	19.6	0.0
1/30/10 2:30	2.1	553	3.9	0.1	3.6	474	6.7	0.2	0.7	408	1.3	0.0	0.3	308	0.5	0.0	42.0	16	63.0	0.1
1/30/10 3:00	1.9	553	3.5	0.1	4.4	474	8.2	0.2	0.7	408	1.3	0.0	0.2	308	0.4	0.0	35.0	16	51.9	0.0
1/30/10 3:30	2.0	548	3.7	0.1	3.9	471	7.3	0.2	0.7	406	1.3	0.0	0.3	308	0.5	0.0	38.0	16	56.6	0.1
1/30/10 4:00	1.9	548	3.5	0.1	3.6	471	6.7	0.2	0.7	406	1.3	0.0	0.3	308	0.5	0.0	44.0	16	66.2	0.1
1/30/10 4:30	1.6	553	2.9	0.1	3.8	474	7.1	0.2	0.7	408	1.3	0.0	0.4	308	0.7	0.0	86.0	16	134.8	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/30/10 5:00	2.0	548	3.7	0.1	4.0	471	7.4	0.2	0.5	406	0.9	0.0	0.2	308	0.4	0.0	100.0	16	158.2	0.1
1/30/10 5:30	2.5	542	4.6	0.1	3.6	467	6.7	0.2	0.6	403	1.1	0.0	0.2	308	0.4	0.0	74.0	16	114.9	0.1
1/30/10 6:00	1.9	548	3.5	0.1	3.6	471	6.7	0.2	0.9	406	1.6	0.0	0.4	308	0.7	0.0	31.0	16	45.6	0.0
1/30/10 6:30	1.9	548	3.5	0.1	3.7	471	6.9	0.2	1.4	406	2.6	0.1	0.7	308	1.3	0.0	18.0	16	25.6	0.0
1/30/10 7:00	2.2	548	4.0	0.1	4.0	471	7.4	0.2	1.5	406	2.7	0.1	0.2	308	0.4	0.0	14.0	16	19.6	0.0
1/30/10 7:30	2.0	542	3.7	0.1	3.7	467	6.9	0.2	1.6	403	2.9	0.1	0.2	308	0.4	0.0	10.0	16	13.7	0.0
1/30/10 8:00	1.9	548	3.5	0.1	4.1	470	7.6	0.2	1.9	404	3.5	0.1	0.4	305	0.7	0.0	7.9	16	10.7	0.0
1/30/10 8:30	3.1	548	5.7	0.2	4.3	470	8.0	0.2	3.3	404	6.1	0.1	0.4	305	0.7	0.0	12.0	16	16.6	0.0
1/30/10 9:00	1.8	542	3.3	0.1	4.1	466	7.6	0.2	3.0	402	5.6	0.1	0.3	305	0.5	0.0	13.0	16	18.1	0.0
1/30/10 9:30	2.1	542	3.9	0.1	4.4	465	8.2	0.2	2.7	400	5.0	0.1	0.2	302	0.4	0.0	27.0	15	39.4	0.0
1/30/10 10:00	2.1	537	3.9	0.1	4.9	461	9.2	0.2	1.9	397	3.5	0.1	0.3	302	0.5	0.0	25.0	15	36.3	0.0
1/30/10 10:30	2.0	542	3.7	0.1	5.0	465	9.3	0.2	1.5	400	2.7	0.1	0.2	302	0.4	0.0	13.0	15	18.1	0.0
1/30/10 11:00	1.8	537	3.3	0.1	5.1	461	9.5	0.2	1.7	397	3.1	0.1	0.4	302	0.7	0.0	6.7	15	9.0	0.0
1/30/10 11:30	2.0	537	3.7	0.1	5.3	461	9.9	0.3	0.9	397	1.6	0.0	0.2	302	0.4	0.0	6.3	15	8.4	0.0
1/30/10 12:00	1.9	531	3.5	0.1	4.9	456	9.2	0.2	0.8	393	1.4	0.0	0.2	299	0.4	0.0	8.3	15	11.3	0.0
1/30/10 12:30	1.9	537	3.5	0.1	4.3	460	8.0	0.2	0.9	396	1.6	0.0	0.2	299	0.4	0.0	5.2	15	6.8	0.0
1/30/10 13:00	2.1	531	3.9	0.1	4.2	456	7.8	0.2	0.7	393	1.3	0.0	0.2	299	0.4	0.0	5.9	15	7.8	0.0
1/30/10 13:30	2.4	537	4.4	0.1	4.0	460	7.4	0.2	1.0	396	1.8	0.0	0.3	299	0.5	0.0	6.7	15	9.0	0.0
1/30/10 14:00	2.0	531	3.7	0.1	3.9	456	7.3	0.2	1.0	393	1.8	0.0	0.4	299	0.7	0.0	12.0	15	16.6	0.0
1/30/10 14:30	2.2	526	4.0	0.1	3.9	453	7.3	0.2	0.7	391	1.3	0.0	0.2	299	0.4	0.0	14.0	15	19.6	0.0
1/30/10 15:00	2.4	526	4.4	0.1	3.8	452	7.1	0.2	0.7	389	1.3	0.0	0.2	296	0.4	0.0	9.5	15	13.0	0.0
1/30/10 15:30	2.4	526	4.4	0.1	4.4	452	8.2	0.2	0.8	389	1.4	0.0	0.2	296	0.4	0.0	15.0	15	21.1	0.0
1/30/10 16:00	2.7	526	5.0	0.1	4.1	452	7.6	0.2	0.6	389	1.1	0.0	0.2	296	0.4	0.0	14.0	15	19.6	0.0
1/30/10 16:30	3.3	521	6.1	0.2	3.9	448	7.3	0.2	0.6	387	1.1	0.0	0.2	296	0.4	0.0	40.0	15	59.8	0.1
1/30/10 17:00	2.9	526	5.4	0.2	3.9	452	7.3	0.2	0.6	389	1.1	0.0	0.2	296	0.4	0.0	180.0	15	295.4	0.3
1/30/10 17:30	2.8	521	5.2	0.2	3.8	448	7.1	0.2	0.6	387	1.1	0.0	0.2	296	0.4	0.0	100.0	15	158.2	0.1
1/30/10 18:00	2.8	526	5.2	0.2	3.9	452	7.3	0.2	0.7	389	1.3	0.0	0.3	296	0.5	0.0	69.0	15	106.7	0.1
1/30/10 18:30	2.4	515	4.4	0.1	3.9	444	7.3	0.2	0.8	385	1.4	0.0	0.3	296	0.5	0.0	360.0	15	616.8	0.5
1/30/10 19:00	2.3	526	4.2	0.1	4.2	452	7.8	0.2	0.7	389	1.3	0.0	0.2	296	0.4	0.0	240.0	15	401.0	0.3
1/30/10 19:30	2.4	521	4.4	0.1	4.1	448	7.6	0.2	0.8	387	1.4	0.0	0.2	296	0.4	0.0	160.0	15	260.7	0.2
1/30/10 20:00	2.4	521	4.4	0.1	4.0	448	7.4	0.2	0.9	387	1.6	0.0	0.2	296	0.4	0.0	170.0	15	278.0	0.2
1/30/10 20:30	2.3	521	4.2	0.1	4.0	449	7.4	0.2	1.9	389	3.5	0.1	0.2	299	0.4	0.0	140.0	15	226.2	0.2
1/30/10 21:00	2.1	526	3.9	0.1	4.0	453	7.4	0.2	3.1	391	5.7	0.1	0.3	299	0.5	0.0	210.0	15	347.9	0.3
1/30/10 21:30	2.2	526	4.0	0.1	4.1	453	7.6	0.2	3.3	391	6.1	0.1	0.2	299	0.4	0.0	230.0	15	383.2	0.3
1/30/10 22:00	2.3	526	4.2	0.1	4.4	453	8.2	0.2	4.6	391	8.6	0.2	0.2	299	0.4	0.0	150.0	15	243.4	0.2
1/30/10 22:30	2.4	526	4.4	0.1	5.2	453	9.7	0.2	7.1	391	13.4	0.3	0.3	299	0.5	0.0	230.0	15	383.2	0.3
1/30/10 23:00	2.3	526	4.2	0.1	6.0	453	11.3	0.3	7.3	391	13.7	0.3	0.2	299	0.4	0.0	84.0	15	131.5	0.1
1/30/10 23:30	3.3	531	6.1	0.2	6.5	457	12.2	0.3	6.9	395	13.0	0.3	0.3	302	0.5	0.0	76.0	15	118.2	0.1
1/31/10 0:00	2.1	531	3.9	0.1	7.6	457	14.3	0.4	6.2	395	11.6	0.3	0.2	302	0.4	0.0	250.0	15	418.7	0.4
1/31/10 0:30	2.0	531	3.7	0.1	8.7	457	16.4	0.4	6.1	395	11.4	0.3	0.2	302	0.4	0.0	210.0	15	347.9	0.3
1/31/10 1:00	1.7	531	3.1	0.1	9.5	458	18.0	0.5	6.7	397	12.6	0.3	0.3	305	0.5	0.0	240.0	16	401.0	0.4
1/31/10 1:30	1.9	531	3.5	0.1	9.4	459	17.8	0.5	6.6	399	12.4	0.3	0.3	308	0.5	0.0	170.0	16	278.0	0.2

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/31/10 2:00	1.9	531	3.5	0.1	8.5	459	16.1	0.4	6.5	399	12.2	0.3	0.2	308	0.4	0.0	160.0	16	260.7	0.2
1/31/10 2:30	2.1	531	3.9	0.1	8.6	460	16.3	0.4	5.8	401	10.9	0.2	0.2	311	0.4	0.0	66.0	16	101.8	0.1
1/31/10 3:00	2.1	537	3.9	0.1	9.1	463	17.2	0.4	5.0	401	9.3	0.2	0.3	308	0.5	0.0	63.0	16	96.9	0.1
1/31/10 3:30	1.9	537	3.5	0.1	9.1	463	17.2	0.4	4.6	401	8.6	0.2	0.7	308	1.3	0.0	57.0	16	87.1	0.1
1/31/10 4:00	2.1	537	3.9	0.1	9.1	464	17.2	0.4	6.1	403	11.4	0.3	0.2	311	0.4	0.0	61.0	16	93.6	0.1
1/31/10 4:30	2.6	542	4.8	0.1	8.2	469	15.5	0.4	7.1	407	13.4	0.3	0.6	314	1.1	0.0	79.0	16	123.2	0.1
1/31/10 5:00	3.1	537	5.7	0.2	7.6	465	14.3	0.4	7.2	405	13.6	0.3	0.2	314	0.4	0.0	41.0	16	61.4	0.1
1/31/10 5:30	3.5	542	6.5	0.2	7.9	470	14.9	0.4	6.6	409	12.4	0.3	0.4	318	0.7	0.0	37.0	16	55.0	0.1
1/31/10 6:00	4.1	537	7.6	0.2	8.5	465	16.1	0.4	5.8	405	10.9	0.2	0.2	314	0.4	0.0	98.0	16	154.9	0.1
1/31/10 6:30	4.7	542	8.8	0.3	9.3	469	17.6	0.5	3.8	407	7.1	0.2	0.7	314	1.3	0.0	220.0	16	365.6	0.3
1/31/10 7:00	5.1	542	9.5	0.3	9.2	469	17.4	0.5	2.9	407	5.4	0.1	0.2	314	0.4	0.0	110.0	16	175.1	0.2
1/31/10 7:30	5.1	542	9.5	0.3	8.6	469	16.3	0.4	2.6	407	4.8	0.1	0.8	314	1.4	0.0	100.0	16	158.2	0.1
1/31/10 8:00	4.7	537	8.8	0.3	8.0	465	15.1	0.4	2.5	405	4.6	0.1	0.3	314	0.5	0.0	110.0	16	175.1	0.2
1/31/10 8:30	5.0	537	9.3	0.3	6.7	465	12.6	0.3	2.4	405	4.4	0.1	0.2	314	0.4	0.0	74.0	16	114.9	0.1
1/31/10 9:00	4.8	537	9.0	0.3	6.0	465	11.3	0.3	2.0	405	3.7	0.1	0.2	314	0.4	0.0	55.0	16	83.9	0.1
1/31/10 9:30	5.3	542	9.9	0.3	5.6	469	10.5	0.3	2.5	407	4.6	0.1	0.2	314	0.4	0.0	32.0	16	47.2	0.0
1/31/10 10:00	5.0	537	9.3	0.3	5.6	465	10.5	0.3	3.8	405	7.1	0.2	0.2	314	0.4	0.0	30.0	16	44.0	0.0
1/31/10 10:30	4.6	542	8.6	0.3	5.5	469	10.3	0.3	4.6	407	8.6	0.2	0.2	314	0.4	0.0	30.0	16	44.0	0.0
1/31/10 11:00	4.2	542	7.8	0.2	5.2	469	9.7	0.3	4.5	407	8.4	0.2	0.2	311	0.4	0.0	23.0	16	33.2	0.0
1/31/10 11:30	4.4	542	8.2	0.3	6.2	468	11.6	0.3	3.8	405	7.1	0.2	0.2	311	0.4	0.0	37.0	16	55.0	0.0
1/31/10 12:00	4.7	537	8.8	0.3	6.7	465	12.6	0.3	3.5	405	6.5	0.1	0.2	314	0.4	0.0	26.0	16	37.8	0.0
1/31/10 12:30	4.8	537	9.0	0.3	7.2	464	13.6	0.4	3.0	403	5.6	0.1	0.2	311	0.4	0.0	52.0	16	79.0	0.1
1/31/10 13:00	5.4	542	10.1	0.3	7.1	468	13.4	0.4	2.4	405	4.4	0.1	0.2	311	0.4	0.0	34.0	16	50.3	0.0
1/31/10 13:30	4.8	537	9.0	0.3	6.6	464	12.4	0.3	1.8	403	3.3	0.1	0.3	311	0.5	0.0	47.0	16	71.0	0.1
1/31/10 14:00	4.3	537	8.0	0.2	6.3	464	11.8	0.3	1.5	403	2.7	0.1	0.3	311	0.5	0.0	41.0	16	61.4	0.1
1/31/10 14:30	3.5	531	6.5	0.2	6.0	460	11.3	0.3	1.5	401	2.7	0.1	0.5	311	0.9	0.0	23.0	16	33.2	0.0
1/31/10 15:00	3.0	537	5.6	0.2	5.5	464	10.3	0.3	1.5	403	2.7	0.1	0.2	311	0.4	0.0	28.0	16	40.9	0.0
1/31/10 15:30	2.8	531	5.2	0.2	5.2	460	9.7	0.3	1.4	401	2.6	0.1	0.4	311	0.7	0.0	19.0	16	27.1	0.0
1/31/10 16:00	2.7	531	5.0	0.1	5.2	460	9.7	0.3	1.4	401	2.6	0.1	1.0	311	1.8	0.0	16.0	16	22.6	0.0
1/31/10 16:30	2.7	531	5.0	0.1	4.7	459	8.8	0.2	1.5	399	2.7	0.1	0.3	308	0.5	0.0	13.0	16	18.1	0.0
1/31/10 17:00	2.8	531	5.2	0.2	4.8	459	9.0	0.2	1.5	399	2.7	0.1	0.2	308	0.4	0.0	12.0	16	16.6	0.0
1/31/10 18:00	3.5	526	6.5	0.2	5.3	456	9.9	0.3	1.6	397	2.9	0.1	0.2	308	0.4	0.0	15.0	16	21.1	0.0
1/31/10 18:30	3.4	531	6.3	0.2	4.9	459	9.2	0.2	1.4	399	2.6	0.1	0.3	308	0.5	0.0	9.3	16	12.7	0.0
1/31/10 19:00	3.5	526	6.5	0.2	5.0	455	9.3	0.2	1.1	395	2.0	0.0	0.5	305	0.9	0.0	11.0	16	15.2	0.0
1/31/10 19:30	3.2	526	5.9	0.2	3.7	455	6.9	0.2	1.1	395	2.0	0.0	0.2	305	0.4	0.0	10.0	16	13.7	0.0
1/31/10 20:00	3.3	526	6.1	0.2	3.0	455	5.6	0.1	0.9	395	1.6	0.0	0.5	305	0.9	0.0	11.0	16	15.2	0.0
1/31/10 20:30	2.8	521	5.2	0.2	2.9	451	5.4	0.1	0.9	393	1.6	0.0	0.2	305	0.4	0.0	9.8	16	13.4	0.0
1/31/10 21:00	2.8	521	5.2	0.2	3.8	451	7.1	0.2	0.7	393	1.3	0.0	0.2	305	0.4	0.0	11.0	16	15.2	0.0
1/31/10 21:30	2.4	526	4.4	0.1	2.7	454	5.0	0.1	0.7	393	1.3	0.0	0.3	302	0.5	0.0	10.0	15	13.7	0.0
1/31/10 22:00	2.3	526	4.2	0.1	2.5	454	4.6	0.1	0.8	393	1.4	0.0	0.2	302	0.4	0.0	13.0	15	18.1	0.0
1/31/10 22:30	3.4	515	6.3	0.2	2.8	446	5.2	0.1	1.1	389	2.0	0.0	0.2	302	0.4	0.0	7.8	15	10.5	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
1/31/10 23:00	2.4	521	4.4	0.1	2.7	450	5.0	0.1	0.7	391	1.3	0.0	0.2	302	0.4	0.0	7.2	15	9.7	0.0
1/31/10 23:30	2.1	521	3.9	0.1	2.4	450	4.4	0.1	0.7	391	1.3	0.0	0.3	302	0.5	0.0	8.0	15	10.8	0.0
2/1/10 0:00	2.5	521	4.6	0.1	2.5	449	4.6	0.1	0.7	389	1.3	0.0	0.2	299	0.4	0.0	7.9	15	10.7	0.0
2/1/10 0:30	2.3	510	4.2	0.1	2.3	442	4.2	0.1	0.7	385	1.3	0.0	0.4	299	0.7	0.0	6.0	15	8.0	0.0
2/1/10 1:00	2.3	510	4.2	0.1	2.3	442	4.2	0.1	1.1	385	2.0	0.0	0.2	299	0.4	0.0	5.8	15	7.7	0.0
2/1/10 1:30	2.3	510	4.2	0.1	2.2	442	4.0	0.1	0.6	385	1.1	0.0	0.2	299	0.4	0.0	5.6	15	7.4	0.0
2/1/10 2:00	2.1	515	3.9	0.1	2.0	445	3.7	0.1	0.6	387	1.1	0.0	0.3	299	0.5	0.0	9.4	15	12.8	0.0
2/1/10 2:30	2.3	515	4.2	0.1	2.2	445	4.0	0.1	0.6	387	1.1	0.0	0.2	299	0.4	0.0	7.3	15	9.8	0.0
2/1/10 3:00	2.0	510	3.7	0.1	2.0	441	3.7	0.1	0.6	383	1.1	0.0	0.2	296	0.4	0.0	6.2	15	8.3	0.0
2/1/10 3:30	2.3	510	4.2	0.1	2.1	441	3.9	0.1	0.6	383	1.1	0.0	0.2	296	0.4	0.0	6.0	15	8.0	0.0
2/1/10 4:00	2.1	510	3.9	0.1	2.9	441	5.4	0.1	0.6	383	1.1	0.0	0.2	296	0.4	0.0	5.6	15	7.4	0.0
2/1/10 4:30	2.5	504	4.6	0.1	1.9	437	3.5	0.1	0.5	381	0.9	0.0	0.3	296	0.5	0.0	5.4	15	7.1	0.0
2/1/10 5:00	1.9	504	3.5	0.1	2.1	437	3.9	0.1	0.6	381	1.1	0.0	0.2	296	0.4	0.0	4.9	15	6.4	0.0
2/1/10 5:30	1.8	510	3.3	0.1	2.0	440	3.7	0.1	0.7	381	1.3	0.0	0.2	293	0.4	0.0	4.3	15	5.6	0.0
2/1/10 6:00	1.8	504	3.3	0.1	1.9	436	3.5	0.1	0.6	379	1.1	0.0	0.2	293	0.4	0.0	4.9	15	6.4	0.0
2/1/10 6:30	1.8	499	3.3	0.1	2.2	433	4.0	0.1	0.6	377	1.1	0.0	0.2	293	0.4	0.0	6.6	15	8.8	0.0
2/1/10 7:00	1.8	504	3.3	0.1	1.9	436	3.5	0.1	0.5	379	0.9	0.0	0.2	293	0.4	0.0	4.8	15	6.3	0.0
2/1/10 7:30	1.8	499	3.3	0.1	2.2	433	4.0	0.1	0.6	377	1.1	0.0	0.2	293	0.4	0.0	4.9	15	6.4	0.0
2/1/10 8:00	2.3	499	4.2	0.1	2.4	432	4.4	0.1	0.6	375	1.1	0.0	0.3	290	0.5	0.0	7.5	15	10.1	0.0
2/1/10 8:30	1.8	504	3.3	0.1	2.2	435	4.0	0.1	0.6	377	1.1	0.0	0.2	290	0.4	0.0	6.2	15	8.3	0.0
2/1/10 9:00	1.7	499	3.1	0.1	1.9	432	3.5	0.1	0.5	375	0.9	0.0	0.2	290	0.4	0.0	8.5	15	11.5	0.0
2/1/10 9:30	1.8	499	3.3	0.1	1.9	432	3.5	0.1	0.4	375	0.7	0.0	0.3	290	0.5	0.0	8.8	15	12.0	0.0
2/1/10 10:00	1.9	494	3.5	0.1	2.0	428	3.7	0.1	1.0	373	1.8	0.0	0.2	290	0.4	0.0	8.0	15	10.8	0.0
2/1/10 10:30	1.7	494	3.1	0.1	1.8	427	3.3	0.1	0.4	371	0.7	0.0	0.3	286	0.5	0.0	6.2	15	8.3	0.0
2/1/10 11:00	1.7	494	3.1	0.1	1.9	428	3.5	0.1	0.5	373	0.9	0.0	0.2	290	0.4	0.0	6.0	15	8.0	0.0
2/1/10 11:30	1.7	494	3.1	0.1	1.9	427	3.5	0.1	0.5	371	0.9	0.0	0.2	286	0.4	0.0	8.7	15	11.8	0.0
2/1/10 12:00	1.7	494	3.1	0.1	1.9	427	3.5	0.1	0.5	371	0.9	0.0	0.2	286	0.4	0.0	5.2	15	6.8	0.0
2/1/10 12:30	1.9	494	3.5	0.1	2.0	427	3.7	0.1	0.4	371	0.7	0.0	0.2	286	0.4	0.0	4.6	15	6.0	0.0
2/1/10 13:00	1.7	494	3.1	0.1	2.0	427	3.7	0.1	0.6	371	1.1	0.0	0.2	286	0.4	0.0	4.5	15	5.9	0.0
2/1/10 13:30	1.6	494	2.9	0.1	2.2	427	4.0	0.1	0.7	371	1.3	0.0	0.2	286	0.4	0.0	5.1	15	6.7	0.0
2/1/10 14:00	1.5	499	2.7	0.1	2.2	431	4.0	0.1	0.6	373	1.1	0.0	0.2	286	0.4	0.0	4.5	15	5.9	0.0
2/1/10 14:30	1.7	499	3.1	0.1	2.4	431	4.4	0.1	0.5	373	0.9	0.0	0.2	286	0.4	0.0	5.3	15	7.0	0.0
2/1/10 15:00	1.6	494	2.9	0.1	2.2	428	4.0	0.1	0.6	373	1.1	0.0	0.2	290	0.4	0.0	6.5	15	8.7	0.0
2/1/10 15:30	1.8	504	3.3	0.1	2.4	435	4.4	0.1	0.6	377	1.1	0.0	0.2	290	0.4	0.0	6.1	15	8.1	0.0
2/1/10 16:00	1.8	499	3.3	0.1	2.5	432	4.6	0.1	0.7	375	1.3	0.0	0.2	290	0.4	0.0	10.0	15	13.7	0.0
2/1/10 16:30	1.7	504	3.1	0.1	2.5	436	4.6	0.1	0.6	379	1.1	0.0	0.2	293	0.4	0.0	10.0	15	13.7	0.0
2/1/10 17:00	1.6	510	2.9	0.1	2.6	440	4.8	0.1	0.7	381	1.3	0.0	0.2	293	0.4	0.0	48.0	15	72.6	0.1
2/1/10 17:30	3.4	510	6.3	0.2	2.5	441	4.6	0.1	0.5	383	0.9	0.0	0.3	296	0.5	0.0	120.0	15	192.0	0.2
2/1/10 18:00	1.9	521	3.5	0.1	2.5	449	4.6	0.1	0.6	389	1.1	0.0	0.2	299	0.4	0.0	200.0	15	330.4	0.3
2/1/10 18:30	1.9	521	3.5	0.1	2.7	450	5.0	0.1	0.6	391	1.1	0.0	0.3	302	0.5	0.0	180.0	15	295.4	0.3
2/1/10 19:00	2.0	521	3.7	0.1	2.9	450	5.4	0.1	0.8	391	1.4	0.0	0.3	302	0.5	0.0	420.0	15	726.5	0.6
2/1/10 19:30	2.1	526	3.9	0.1	2.8	455	5.2	0.1	0.6	395	1.1	0.0	0.3	305	0.5	0.0	460.0	16	800.2	0.7

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/1/10 20:00	2.0	526	3.7	0.1	3.0	456	5.6	0.1	0.7	397	1.3	0.0	1.0	308	1.8	0.0	230.0	16	383.2	0.3
2/1/10 20:30	1.8	531	3.3	0.1	2.8	459	5.2	0.1	0.9	399	1.6	0.0	0.2	308	0.4	0.0	280.0	16	472.3	0.4
2/1/10 21:00	1.8	537	3.3	0.1	3.0	464	5.6	0.1	1.8	403	3.3	0.1	0.2	311	0.4	0.0	360.0	16	616.8	0.6
2/1/10 21:30	2.0	537	3.7	0.1	2.7	465	5.0	0.1	3.2	405	5.9	0.1	0.2	314	0.4	0.0	440.0	16	763.3	0.7
2/1/10 22:00	1.8	542	3.3	0.1	2.9	470	5.4	0.1	4.8	409	9.0	0.2	0.3	318	0.5	0.0	340.0	16	580.4	0.5
2/1/10 22:30	1.9	548	3.5	0.1	3.6	474	6.7	0.2	7.1	411	13.4	0.3	0.3	318	0.5	0.0	740.0	16	1325.8	1.2
2/1/10 23:00	2.3	548	4.2	0.1	4.4	474	8.2	0.2	10.2	411	19.3	0.4	0.3	318	0.5	0.0	310.0	16	526.2	0.5
2/1/10 23:30	1.9	548	3.5	0.1	5.3	475	9.9	0.3	11.1	413	21.1	0.5	0.2	321	0.4	0.0	190.0	16	312.9	0.3
2/2/10 00:00	2.0	548	3.7	0.1	7.0	475	13.2	0.4	10.2	413	19.3	0.4	0.2	321	0.4	0.0	130.0	16	209.1	0.2
2/2/10 00:30	2.3	548	4.2	0.1	8.8	475	16.6	0.4	11.1	413	21.1	0.5	0.2	321	0.4	0.0	58.0	16	88.7	0.1
2/2/10 1:00	1.9	553	3.5	0.1	11.0	480	20.9	0.6	11.9	417	22.6	0.5	0.2	324	0.4	0.0	56.0	17	85.5	0.1
2/2/10 1:30	2.0	553	3.7	0.1	12.0	480	22.8	0.6	13.4	417	25.5	0.6	0.2	324	0.4	0.0	39.0	17	58.2	0.1
2/2/10 2:00	1.9	559	3.5	0.1	11.0	483	20.9	0.6	15.5	420	29.6	0.7	0.2	324	0.4	0.0	85.0	17	133.1	0.1
2/2/10 2:30	1.9	559	3.5	0.1	11.1	483	21.1	0.6	15.7	420	30.0	0.7	0.2	324	0.4	0.0	79.0	17	123.2	0.1
2/2/10 3:00	2.0	559	3.7	0.1	12.2	483	23.2	0.6	11.9	420	22.6	0.5	0.2	324	0.4	0.0	54.0	17	82.2	0.1
2/2/10 3:30	2.1	559	3.9	0.1	13.3	483	25.4	0.7	8.5	420	16.1	0.4	0.2	324	0.4	0.0	32.0	17	47.2	0.0
2/2/10 4:00	2.3	559	4.2	0.1	14.2	483	27.1	0.7	5.6	420	10.5	0.2	0.2	324	0.4	0.0	25.0	17	36.3	0.0
2/2/10 4:30	2.5	559	4.6	0.1	13.3	483	25.4	0.7	3.7	420	6.9	0.2	0.2	324	0.4	0.0	120.0	17	192.0	0.2
2/2/10 5:00	2.7	559	5.0	0.2	11.3	483	21.5	0.6	2.7	420	5.0	0.1	0.3	324	0.5	0.0	49.0	17	74.2	0.1
2/2/10 5:30	3.6	559	6.7	0.2	9.2	483	17.4	0.5	2.5	420	4.6	0.1	0.2	324	0.4	0.0	30.0	17	44.0	0.0
2/2/10 6:00	5.7	565	10.7	0.3	7.1	487	13.4	0.4	2.5	422	4.6	0.1	0.6	324	1.1	0.0	37.0	17	55.0	0.1
2/2/10 6:30	5.8	559	10.9	0.3	5.5	483	10.3	0.3	2.4	420	4.4	0.1	0.2	324	0.4	0.0	25.0	17	36.3	0.0
2/2/10 7:00	6.5	559	12.2	0.4	5.2	483	9.7	0.3	1.8	420	3.3	0.1	0.5	324	0.9	0.0	25.0	17	36.3	0.0
2/2/10 7:30	7.1	565	13.4	0.4	5.0	487	9.3	0.3	2.1	422	3.9	0.1	0.2	324	0.4	0.0	23.0	17	33.2	0.0
2/2/10 8:00	7.1	565	13.4	0.4	5.0	487	9.3	0.3	2.0	422	3.7	0.1	0.2	324	0.4	0.0	22.0	17	31.7	0.0
2/2/10 8:30	7.3	559	13.7	0.4	4.6	483	8.6	0.2	2.3	420	4.2	0.1	0.3	324	0.5	0.0	18.0	17	25.6	0.0
2/2/10 9:00	8.1	559	15.3	0.5	4.2	483	7.8	0.2	1.9	420	3.5	0.1	0.2	324	0.4	0.0	18.0	17	25.6	0.0
2/2/10 9:30	8.9	559	16.8	0.5	5.5	483	10.3	0.3	1.7	420	3.1	0.1	0.3	324	0.5	0.0	16.0	17	22.6	0.0
2/2/10 10:00	8.9	559	16.8	0.5	4.5	483	8.4	0.2	1.5	420	2.7	0.1	0.2	324	0.4	0.0	16.0	17	22.6	0.0
2/2/10 10:30	8.5	559	16.1	0.5	4.6	483	8.6	0.2	1.4	420	2.6	0.1	0.2	324	0.4	0.0	18.0	17	25.6	0.0
2/2/10 11:00	7.3	553	13.7	0.4	4.5	479	8.4	0.2	1.1	416	2.0	0.0	0.2	321	0.4	0.0	23.0	16	33.2	0.0
2/2/10 11:30	6.7	553	12.6	0.4	4.4	480	8.2	0.2	1.0	417	1.8	0.0	0.2	324	0.4	0.0	16.0	17	22.6	0.0
2/2/10 12:00	4.6	559	8.6	0.3	3.9	482	7.3	0.2	1.0	418	1.8	0.0	0.2	321	0.4	0.0	15.0	16	21.1	0.0
2/2/10 12:30	3.6	559	6.7	0.2	3.8	482	7.1	0.2	1.0	418	1.8	0.0	0.2	321	0.4	0.0	14.0	16	19.6	0.0
2/2/10 13:00	3.2	559	5.9	0.2	3.7	482	6.9	0.2	0.9	418	1.6	0.0	0.3	321	0.5	0.0	16.0	16	22.6	0.0
2/2/10 13:30	4.0	553	7.4	0.2	3.8	479	7.1	0.2	0.9	416	1.6	0.0	0.2	321	0.4	0.0	14.0	16	19.6	0.0
2/2/10 14:00	3.0	553	5.6	0.2	3.6	479	6.7	0.2	0.9	416	1.6	0.0	0.5	321	0.9	0.0	16.0	16	22.6	0.0
2/2/10 14:30	3.8	548	7.1	0.2	3.8	475	7.1	0.2	0.9	413	1.6	0.0	0.2	321	0.4	0.0	12.0	16	16.6	0.0
2/2/10 15:00	3.1	553	5.7	0.2	3.6	478	6.7	0.2	0.9	414	1.6	0.0	0.5	318	0.9	0.0	9.5	16	16.6	0.0
2/2/10 15:30	2.5	553	4.6	0.1	3.6	479	6.7	0.2	0.9	416	1.6	0.0	0.2	321	0.4	0.0	12.0	16	13.0	0.0
2/2/10 16:00	2.5	553	4.6	0.1	3.8	478	7.1	0.2	0.7	414	1.3	0.0	0.2	318	0.4	0.0	12.0	16	16.6	0.0
2/2/10 16:30	2.6	548	4.8	0.1	4.0	474	7.4	0.2	0.9	411	1.6	0.0	0.3	318	0.5	0.0	9.9	16	13.6	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/2/10 17:00	3.2	548	5.9	0.2	3.8	474	7.1	0.2	0.9	411	1.6	0.0	0.4	318	0.7	0.0	9.5	16	13.0	0.0
2/2/10 17:30	2.4	548	4.4	0.1	3.8	474	7.1	0.2	0.7	411	1.3	0.0	0.2	318	0.4	0.0	11.0	16	15.2	0.0
2/2/10 18:00	2.4	542	4.4	0.1	4.1	470	7.6	0.2	0.7	409	1.3	0.0	0.2	318	0.4	0.0	10.0	16	13.7	0.0
2/2/10 18:30	2.3	548	4.2	0.1	3.8	474	7.1	0.2	1.2	411	2.2	0.1	0.4	318	0.7	0.0	8.3	16	11.3	0.0
2/2/10 19:00	2.2	548	4.0	0.1	3.6	474	6.7	0.2	0.9	411	1.6	0.0	0.3	318	0.5	0.0	6.9	16	9.2	0.0
2/2/10 19:30	2.1	553	3.9	0.1	3.9	476	7.3	0.2	0.7	412	1.3	0.0	0.3	314	0.5	0.0	7.9	16	10.7	0.0
2/2/10 20:00	2.2	553	4.0	0.1	4.2	476	7.8	0.2	0.6	412	1.1	0.0	0.2	314	0.4	0.0	5.9	16	7.8	0.0
2/2/10 20:30	2.0	553	3.7	0.1	3.8	476	7.1	0.2	1.0	412	1.8	0.0	0.3	314	0.5	0.0	7.1	16	9.5	0.0
2/2/10 21:00	1.9	542	3.5	0.1	4.2	469	7.8	0.2	0.7	407	1.3	0.0	0.2	314	0.4	0.0	11.0	16	15.2	0.0
2/2/10 21:30	1.9	542	3.5	0.1	3.8	469	7.1	0.2	0.7	407	1.3	0.0	0.2	314	0.4	0.0	8.6	16	11.7	0.0
2/2/10 22:00	1.9	542	3.5	0.1	3.8	469	7.1	0.2	0.7	407	1.3	0.0	0.2	314	0.4	0.0	7.4	16	10.0	0.0
2/2/10 22:30	2.2	542	4.0	0.1	3.8	468	7.1	0.2	0.6	405	1.1	0.0	0.3	311	0.5	0.0	7.1	16	9.5	0.0
2/2/10 23:00	2.0	537	3.7	0.1	4.2	464	7.8	0.2	0.6	403	1.1	0.0	0.2	311	0.4	0.0	5.7	16	7.5	0.0
2/2/10 23:30	1.9	542	3.5	0.1	4.5	468	8.4	0.2	0.6	405	1.1	0.0	0.2	311	0.4	0.0	6.6	16	8.8	0.0
2/3/10 0:00	2.0	537	3.7	0.1	3.8	464	7.1	0.2	0.6	403	1.1	0.0	0.4	311	0.7	0.0	7.1	16	9.5	0.0
2/3/10 0:30	1.9	542	3.5	0.1	3.8	468	7.1	0.2	0.6	405	1.1	0.0	0.3	311	0.5	0.0	6.4	16	8.5	0.0
2/3/10 1:00	2.3	537	4.2	0.1	3.8	463	7.1	0.2	1.0	401	1.8	0.0	0.2	308	0.4	0.0	5.5	16	7.3	0.0
2/3/10 1:30	2.0	531	3.7	0.1	3.7	460	6.9	0.2	0.6	401	1.1	0.0	0.3	311	0.5	0.0	6.4	16	8.5	0.0
2/3/10 2:00	2.4	531	4.4	0.1	3.8	459	7.1	0.2	0.7	399	1.3	0.0	0.4	308	0.7	0.0	6.1	16	8.1	0.0
2/3/10 2:30	1.9	531	3.5	0.1	3.7	459	6.9	0.2	0.6	399	1.1	0.0	0.2	308	0.4	0.0	6.0	16	8.0	0.0
2/3/10 3:00	1.9	537	3.5	0.1	3.7	463	6.9	0.2	0.7	401	1.3	0.0	0.2	308	0.4	0.0	4.8	16	6.3	0.0
2/3/10 3:30	1.9	537	3.5	0.1	3.6	463	6.7	0.2	0.6	401	1.1	0.0	0.2	308	0.4	0.0	5.2	16	6.8	0.0
2/3/10 4:00	1.9	537	3.5	0.1	3.8	463	7.1	0.2	0.6	401	1.1	0.0	0.5	308	0.9	0.0	5.3	16	7.0	0.0
2/3/10 4:30	1.8	537	3.3	0.1	3.8	463	7.1	0.2	0.5	401	0.9	0.0	0.2	308	0.4	0.0	6.0	16	8.0	0.0
2/3/10 5:00	1.7	526	3.1	0.1	3.8	457	7.1	0.2	0.6	399	1.1	0.0	0.2	311	0.4	0.0	5.2	16	6.8	0.0
2/3/10 5:30	1.7	526	3.1	0.1	4.1	456	7.6	0.2	0.6	397	1.1	0.0	0.3	308	0.5	0.0	5.1	16	6.7	0.0
2/3/10 6:00	1.9	537	3.5	0.1	4.0	463	7.4	0.2	0.6	401	1.1	0.0	0.2	308	0.4	0.0	5.6	16	7.4	0.0
2/3/10 6:30	1.9	526	3.5	0.1	3.8	456	7.1	0.2	0.6	397	1.1	0.0	0.4	308	0.7	0.0	6.0	16	8.0	0.0
2/3/10 7:00	1.8	531	3.3	0.1	3.8	459	7.1	0.2	0.6	399	1.1	0.0	0.3	308	0.5	0.0	66.0	16	101.8	0.1
2/3/10 7:30	2.1	526	3.9	0.1	3.8	456	7.1	0.2	0.6	397	1.1	0.0	0.2	308	0.4	0.0	260.0	16	436.5	0.4
2/3/10 8:00	1.9	526	3.5	0.1	3.8	455	7.1	0.2	0.5	395	0.9	0.0	0.2	305	0.4	0.0	64.0	16	98.5	0.1
2/3/10 8:30	1.9	531	3.5	0.1	3.8	458	7.1	0.2	0.6	397	1.1	0.0	0.2	305	0.4	0.0	20.0	16	28.6	0.0
2/3/10 9:00	1.9	526	3.5	0.1	3.9	455	7.3	0.2	0.5	395	0.9	0.0	0.4	305	0.7	0.0	12.0	16	16.6	0.0
2/3/10 9:30	1.9	526	3.5	0.1	4.1	455	7.6	0.2	0.6	395	1.1	0.0	0.2	305	0.4	0.0	9.4	16	12.8	0.0
2/3/10 10:00	1.9	526	3.5	0.1	4.1	455	7.6	0.2	0.8	395	1.4	0.0	0.2	305	0.4	0.0	8.7	16	11.8	0.0
2/3/10 10:30	1.7	531	3.1	0.1	3.8	458	7.1	0.2	0.9	397	1.6	0.0	0.2	305	0.4	0.0	7.6	16	10.2	0.0
2/3/10 11:00	1.8	526	3.3	0.1	3.8	455	7.1	0.2	2.5	395	4.6	0.1	0.2	305	0.4	0.0	10.0	16	13.7	0.0
2/3/10 11:30	2.0	526	3.7	0.1	3.9	455	7.3	0.2	3.6	395	6.7	0.1	0.2	305	0.4	0.0	7.5	16	10.1	0.0
2/3/10 12:00	2.0	526	3.7	0.1	4.2	455	7.8	0.2	3.1	395	5.7	0.1	0.4	305	0.7	0.0	6.9	16	9.2	0.0
2/3/10 12:30	1.8	526	3.3	0.1	4.4	455	8.2	0.2	2.2	395	4.0	0.1	0.2	305	0.4	0.0	7.0	16	9.4	0.0
2/3/10 13:00	1.8	526	3.3	0.1	5.9	455	11.1	0.3	1.4	395	2.6	0.1	0.2	305	0.4	0.0	6.7	16	9.0	0.0
2/3/10 13:30	1.8	521	3.3	0.1	6.9	451	13.0	0.3	0.9	393	1.6	0.0	0.2	305	0.4	0.0	5.3	16	7.0	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/3/10 14:00	2.2	521	4.0	0.1	6.1	451	11.4	0.3	0.7	393	1.3	0.0	0.2	305	0.4	0.0	5.9	16	7.8	0.0
2/3/10 14:30	1.9	521	3.5	0.1	5.2	451	9.7	0.2	0.6	393	1.1	0.0	0.2	305	0.4	0.0	65.0	16	100.1	0.1
2/3/10 15:00	1.8	521	3.3	0.1	4.7	450	8.8	0.2	0.5	391	0.9	0.0	0.2	302	0.4	0.0	150.0	15	243.4	0.2
2/3/10 15:30	2.1	515	3.9	0.1	5.0	447	9.3	0.2	0.5	390	0.9	0.0	0.2	305	0.4	0.0	45.0	16	67.8	0.1
2/3/10 16:00	1.7	526	3.1	0.1	4.5	455	8.4	0.2	0.5	395	0.9	0.0	0.2	305	0.4	0.0	73.0	16	113.3	0.1
2/3/10 16:30	2.2	521	4.0	0.1	4.4	452	8.2	0.2	0.6	395	1.1	0.0	0.2	308	0.4	0.0	43.0	16	64.6	0.1
2/3/10 17:00	1.6	521	2.9	0.1	6.3	452	11.8	0.3	0.6	395	1.1	0.0	0.3	308	0.5	0.0	59.0	16	90.3	0.1
2/3/10 17:30	1.7	521	3.1	0.1	4.4	453	8.2	0.2	0.6	396	1.1	0.0	0.2	311	0.4	0.0	80.0	16	124.8	0.1
2/3/10 18:00	1.8	526	3.3	0.1	4.2	458	7.8	0.2	1.0	400	1.8	0.0	0.5	314	0.9	0.0	200.0	16	330.4	0.3
2/3/10 18:30	2.2	526	4.0	0.1	5.1	459	9.5	0.2	2.4	402	4.4	0.1	0.3	318	0.5	0.0	110.0	16	175.1	0.2
2/3/10 19:00	2.7	531	5.0	0.1	4.6	464	8.6	0.2	2.8	407	5.2	0.1	0.3	321	0.5	0.0	130.0	16	209.1	0.2
2/3/10 19:30	3.1	537	5.7	0.2	5.1	469	9.4	0.2	2.6	413	4.8	0.1	1.1	327	2.0	0.0	440.0	17	763.3	0.7
2/3/10 20:00	3.0	537	5.6	0.2	5.5	470	10.3	0.3	2.2	415	4.0	0.1	0.4	331	0.7	0.0	230.0	17	383.2	0.4
2/3/10 20:30	2.7	537	5.0	0.2	6.1	473	11.4	0.3	2.1	418	3.9	0.1	0.2	337	0.4	0.0	580.0	17	1023.6	1.0
2/3/10 21:00	2.5	542	4.6	0.1	6.3	477	11.8	0.3	2.3	423	4.2	0.1	0.4	341	0.7	0.0	520.0	17	911.5	0.9
2/3/10 21:30	2.2	548	4.0	0.1	6.3	483	11.8	0.3	3.6	429	6.7	0.2	0.2	347	0.4	0.0	710.0	18	1268.8	1.3
2/3/10 22:00	2.2	553	4.0	0.1	5.9	488	11.1	0.3	4.5	433	8.4	0.2	0.3	351	0.5	0.0	950.0	18	1728.7	1.7
2/3/10 22:30	1.9	565	3.5	0.1	6.3	497	11.8	0.3	5.2	440	9.7	0.2	0.2	354	0.4	0.0	600.0	18	1061.1	1.1
2/3/10 23:00	2.2	565	4.0	0.1	6.6	499	12.4	0.3	8.4	444	15.9	0.4	0.2	361	0.4	0.0	270.0	18	454.4	0.5
2/3/10 23:30	2.0	570	3.7	0.1	7.5	504	14.1	0.4	10.5	448	19.9	0.5	0.3	365	0.5	0.0	110.0	18	175.1	0.2
2/4/10 00:00	2.2	576	4.0	0.1	8.3	508	15.7	0.4	14.5	451	27.7	0.7	0.3	365	0.5	0.0	250.0	18	418.7	0.4
2/4/10 00:30	2.1	588	3.9	0.1	9.6	517	18.2	0.5	19.1	457	36.7	0.9	0.2	368	0.4	0.0	130.0	19	209.1	0.2
2/4/10 1:00	2.5	593	4.6	0.2	11.1	522	21.1	0.6	22.5	462	43.3	1.1	0.2	372	0.4	0.0	140.0	19	226.2	0.2
2/4/10 1:30	2.4	599	4.4	0.1	13.3	526	25.4	0.7	25.8	464	49.8	1.3	0.3	372	0.5	0.0	190.0	19	312.9	0.3
2/4/10 2:00	2.7	599	5.0	0.2	17.2	527	33.0	1.0	24.2	466	46.7	1.2	0.3	375	0.5	0.0	210.0	19	347.9	0.4
2/4/10 2:30	3.3	599	6.1	0.2	19.8	527	38.0	1.1	14.6	466	27.9	0.7	0.3	375	0.5	0.0	90.0	19	141.5	0.2
2/4/10 3:00	3.2	611	5.9	0.2	21.8	535	42.0	1.3	8.8	471	16.6	0.4	0.2	375	0.4	0.0	51.0	19	77.4	0.1
2/4/10 3:30	3.2	611	5.9	0.2	23.3	535	44.9	1.4	7.5	471	14.1	0.4	0.2	375	0.4	0.0	45.0	19	67.8	0.1
2/4/10 4:00	3.2	617	5.9	0.2	18.5	540	35.5	1.1	6.2	476	11.6	0.3	0.2	379	0.4	0.0	41.0	19	61.4	0.1
2/4/10 4:30	3.2	611	5.9	0.2	13.7	536	26.1	0.8	5.5	473	10.3	0.3	0.2	379	0.4	0.0	33.0	19	48.7	0.1
2/4/10 5:00	3.7	617	6.9	0.2	11.1	540	21.1	0.6	6.7	476	12.6	0.3	0.2	379	0.4	0.0	30.0	19	44.0	0.0
2/4/10 5:30	4.2	617	7.8	0.3	10.3	540	19.5	0.6	5.7	476	10.7	0.3	0.2	379	0.4	0.0	36.0	19	53.5	0.1
2/4/10 6:00	5.2	617	9.7	0.3	9.3	540	17.6	0.5	4.3	476	8.0	0.2	0.2	379	0.4	0.0	31.0	19	45.6	0.0
2/4/10 6:30	6.6	623	12.4	0.4	9.1	544	17.2	0.5	3.3	478	6.1	0.2	1.9	379	3.5	0.1	33.0	19	48.7	0.1
2/4/10 7:00	7.4	617	13.9	0.5	9.3	540	17.6	0.5	2.1	476	3.9	0.1	0.2	379	0.4	0.0	40.0	19	59.8	0.1
2/4/10 7:30	9.9	617	18.8	0.7	8.2	540	15.5	0.5	1.9	476	3.5	0.1	0.3	379	0.5	0.0	29.0	19	42.5	0.0
2/4/10 8:00	11.0	617	20.9	0.7	7.3	540	13.7	0.4	1.6	476	2.9	0.1	0.2	379	0.4	0.0	25.0	19	36.3	0.0
2/4/10 8:30	13.0	623	24.8	0.9	6.3	544	11.8	0.4	2.5	478	4.6	0.1	0.2	379	0.4	0.0	380.0	19	653.2	0.7
2/4/10 9:00	14.0	617	26.7	0.9	6.1	540	11.4	0.3	1.5	476	2.7	0.1	0.2	379	0.4	0.0	160.0	19	260.7	0.3
2/4/10 9:30	12.0	617	22.8	0.8	5.5	540	10.3	0.3	1.5	476	2.7	0.1	0.2	379	0.4	0.0	82.0	19	128.2	0.1
2/4/10 10:00	9.1	617	17.2	0.6	6.0	540	11.3	0.3	1.3	476	2.4	0.1	0.2	379	0.4	0.0	57.0	19	87.1	0.1
2/4/10 10:30	7.4	617	13.9	0.5	5.3	539	9.9	0.3	1.6	474	2.9	0.1	0.2	375	0.4	0.0	50.0	19	75.8	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/4/10 11:00	6.1	617	11.4	0.4	5.7	539	10.7	0.3	1.5	474	2.7	0.1	0.2	375	0.4	0.0	37.0	19	55.0	0.1
2/4/10 11:30	5.3	617	9.9	0.3	5.6	539	10.5	0.3	3.0	474	5.6	0.1	0.2	375	0.4	0.0	34.0	19	50.3	0.1
2/4/10 12:00	4.8	617	9.0	0.3	5.5	539	10.3	0.3	6.7	474	12.6	0.3	0.2	375	0.4	0.0	27.0	19	39.4	0.0
2/4/10 12:30	5.3	617	9.9	0.3	6.1	539	11.4	0.3	5.6	474	10.5	0.3	0.2	375	0.5	0.0	26.0	19	37.8	0.0
2/4/10 13:00	4.6	617	8.6	0.3	6.1	539	11.4	0.3	3.8	474	7.1	0.2	0.2	375	0.4	0.0	23.0	19	33.2	0.0
2/4/10 13:30	3.7	617	6.9	0.2	8.1	539	15.3	0.5	2.6	474	4.8	0.1	0.3	375	0.5	0.0	20.0	19	28.6	0.0
2/4/10 14:00	3.2	617	5.9	0.2	8.9	539	16.8	0.5	2.0	474	3.7	0.1	0.2	375	0.4	0.0	40.0	19	59.8	0.1
2/4/10 14:30	3.3	617	6.1	0.2	8.0	539	15.1	0.5	1.7	474	3.1	0.1	0.3	375	0.5	0.0	33.0	19	48.7	0.1
2/4/10 15:00	2.4	617	4.4	0.2	7.7	538	14.5	0.4	2.7	471	5.0	0.1	0.2	372	0.4	0.0	19.0	19	27.1	0.0
2/4/10 15:30	2.5	617	4.6	0.2	6.6	539	12.4	0.4	1.3	474	2.4	0.1	0.2	375	0.4	0.0	15.0	19	21.1	0.0
2/4/10 16:00	2.4	617	4.4	0.2	6.1	539	11.4	0.3	1.3	474	2.4	0.1	0.3	375	0.5	0.0	15.0	19	21.1	0.0
2/4/10 16:30	2.4	617	4.4	0.2	5.9	539	11.1	0.3	1.2	474	2.2	0.1	0.3	375	0.5	0.0	18.0	19	25.6	0.0
2/4/10 17:00	2.4	617	4.4	0.2	5.2	540	11.1	0.3	1.2	476	2.2	0.1	0.2	379	0.4	0.0	17.0	19	24.1	0.0
2/4/10 17:30	2.4	617	4.4	0.2	5.7	541	10.7	0.3	1.5	478	2.7	0.1	0.3	382	0.5	0.0	23.0	19	33.2	0.0
2/4/10 18:00	2.6	611	4.8	0.2	6.0	537	11.3	0.3	1.3	475	2.4	0.1	0.2	382	0.4	0.0	46.0	19	69.4	0.1
2/4/10 18:30	3.0	611	5.6	0.2	5.7	540	10.7	0.3	2.1	480	3.9	0.1	0.2	390	0.4	0.0	480.0	20	837.2	0.9
2/4/10 19:00	3.7	617	6.9	0.2	6.3	545	11.8	0.4	1.1	484	2.0	0.1	0.2	393	0.4	0.0	430.0	20	744.9	0.8
2/4/10 19:30	3.9	617	7.3	0.3	6.0	545	11.3	0.3	0.9	484	1.6	0.0	0.3	393	0.5	0.0	990.0	20	1806.1	2.0
2/4/10 20:00	4.2	617	7.8	0.3	5.8	546	10.9	0.3	1.6	486	2.9	0.1	0.2	397	0.4	0.0	410.0	20	708.1	0.8
2/4/10 20:30	3.7	623	6.9	0.2	6.1	552	11.4	0.4	1.1	493	2.0	0.1	0.2	404	0.4	0.0	240.0	20	401.0	0.5
2/4/10 21:00	3.6	629	6.7	0.2	6.1	557	11.4	0.4	1.6	496	2.9	0.1	0.2	404	0.4	0.0	180.0	20	295.4	0.3
2/4/10 21:30	3.1	623	5.7	0.2	5.7	555	10.7	0.3	8.2	498	15.5	0.4	0.7	412	1.3	0.0	80.0	21	124.8	0.1
2/4/10 22:00	2.7	623	5.0	0.2	5.6	556	10.5	0.3	18.3	500	35.1	1.0	0.6	416	1.1	0.0	69.0	21	106.7	0.1
2/4/10 22:30	2.5	623	4.6	0.2	6.1	557	11.4	0.4	25.0	502	48.3	1.4	0.2	419	0.4	0.0	50.0	21	75.8	0.1
2/4/10 23:00	2.6	635	4.8	0.2	9.0	567	17.0	0.5	26.0	509	50.2	1.4	1.4	423	2.6	0.1	43.0	21	64.6	0.1
2/4/10 23:30	2.2	635	4.0	0.1	15.3	568	29.2	0.9	17.4	512	33.3	1.0	0.2	427	0.4	0.0	37.0	21	55.0	0.1
2/5/10 0:00	2.2	635	4.0	0.1	21.5	568	41.4	1.3	10.9	512	20.7	0.6	0.2	427	0.4	0.0	32.0	21	47.2	0.1
2/5/10 0:30	2.4	647	4.4	0.2	26.0	576	50.2	1.6	6.0	517	11.3	0.3	0.2	427	0.4	0.0	42.0	21	63.0	0.1
2/5/10 1:00	2.1	647	3.9	0.1	21.0	576	40.4	1.3	4.3	517	8.0	0.2	0.3	427	0.5	0.0	79.0	21	123.2	0.1
2/5/10 1:30	2.1	641	3.9	0.1	14.6	571	27.9	0.9	2.7	512	5.0	0.1	0.3	423	0.5	0.0	110.0	21	175.1	0.2
2/5/10 2:00	2.3	653	4.2	0.2	11.8	581	22.4	0.7	2.2	519	4.0	0.1	0.1	427	0.2	0.0	160.0	21	260.7	0.3
2/5/10 2:30	2.1	660	3.9	0.1	8.9	586	16.8	0.6	1.7	524	3.1	0.1	0.2	431	0.4	0.0	260.0	22	436.5	0.5
2/5/10 3:00	2.1	653	3.9	0.1	7.6	583	14.3	0.5	1.5	524	2.7	0.1	0.3	435	0.5	0.0	610.0	22	1079.9	1.3
2/5/10 3:30	2.3	660	4.2	0.2	7.1	587	13.4	0.4	1.6	526	2.9	0.1	0.2	435	0.4	0.0	300.0	22	508.2	0.6
2/5/10 4:00	3.2	660	5.9	0.2	6.6	589	12.4	0.4	2.0	529	3.7	0.1	0.2	439	0.4	0.0	150.0	22	243.4	0.3
2/5/10 4:30	5.3	660	9.9	0.4	6.5	589	12.2	0.4	3.1	529	5.7	0.2	0.6	439	1.1	0.0	430.0	22	744.9	0.9
2/5/10 5:00	9.1	667	17.2	0.6	6.6	594	12.4	0.4	4.1	534	7.6	0.2	0.3	443	0.5	0.0	140.0	22	226.2	0.3
2/5/10 5:30	12.0	660	22.8	0.8	6.6	590	12.4	0.4	6.4	531	12.0	0.4	0.2	443	0.4	0.0	76.0	22	118.2	0.1
2/5/10 6:00	14.0	667	26.7	1.0	7.1	594	13.1	0.4	10.4	534	19.7	0.6	0.3	443	0.5	0.0	53.0	22	80.6	0.1
2/5/10 6:30	11.0	667	20.9	0.8	8.0	594	15.1	0.5	10.5	534	19.9	0.6	0.3	443	0.5	0.0	36.0	22	53.5	0.1
2/5/10 7:00	8.4	667	15.9	0.6	9.4	596	17.8	0.6	8.1	536	15.3	0.5	0.3	447	0.5	0.0	30.0	22	44.0	0.1
2/5/10 7:30	6.2	667	11.6	0.4	12.9	597	24.6	0.8	8.0	538	15.1	0.5	0.3	450	0.5	0.0	300.0	23	508.2	0.6

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/5/10 8:00	5.5	667	10.3	0.4	13.8	596	26.3	0.9	7.2	536	13.6	0.4	0.3	447	0.5	0.0	160.0	22	260.7	0.3
2/5/10 8:30	3.7	667	6.9	0.3	12.5	596	23.8	0.8	4.6	536	8.6	0.3	0.2	447	0.4	0.0	180.0	22	295.4	0.4
2/5/10 9:00	3.1	673	5.7	0.2	12.5	599	23.8	0.8	3.2	536	5.9	0.2	0.2	443	0.4	0.0	63.0	22	96.9	0.1
2/5/10 9:30	3.0	673	5.6	0.2	11.3	601	21.5	0.7	2.0	541	3.7	0.1	0.2	450	0.4	0.0	60.0	23	92.0	0.1
2/5/10 10:00	3.1	667	5.7	0.2	10.1	597	19.1	0.6	2.1	538	3.9	0.1	0.2	450	0.4	0.0	80.0	23	124.8	0.2
2/5/10 10:30	2.6	673	4.8	0.2	7.6	600	14.3	0.5	4.2	539	7.8	0.2	0.2	447	0.4	0.0	43.0	22	64.6	0.1
2/5/10 11:00	2.8	680	5.2	0.2	7.1	606	13.4	0.5	5.1	544	9.5	0.3	0.2	450	0.4	0.0	28.0	23	40.9	0.1
2/5/10 11:30	3.7	680	6.9	0.3	6.6	605	12.4	0.4	4.5	541	8.4	0.3	0.3	447	0.5	0.0	26.0	22	37.8	0.0
2/5/10 12:00	4.1	680	7.6	0.3	7.9	605	14.9	0.5	3.3	541	6.1	0.2	0.2	447	0.4	0.0	21.0	22	30.2	0.0
2/5/10 12:30	5.5	673	10.3	0.4	9.0	600	17.0	0.6	2.8	539	5.2	0.2	0.2	447	0.4	0.0	28.0	22	40.9	0.1
2/5/10 13:00	6.9	673	13.0	0.5	11.1	600	21.1	0.7	2.7	539	5.0	0.2	0.3	447	0.5	0.0	23.0	22	33.2	0.0
2/5/10 13:30	6.8	673	12.8	0.5	8.3	599	15.7	0.5	2.0	536	3.7	0.1	0.3	443	0.5	0.0	20.0	22	28.6	0.0
2/5/10 14:00	6.7	673	12.6	0.5	7.3	600	13.7	0.5	1.5	539	2.7	0.1	1.1	447	2.0	0.1	23.0	22	33.2	0.0
2/5/10 14:30	6.2	673	11.6	0.4	8.2	599	15.5	0.5	1.6	536	2.9	0.1	0.4	443	0.7	0.0	18.0	22	25.6	0.0
2/5/10 15:00	5.7	673	10.7	0.4	7.1	599	13.4	0.4	1.2	536	2.2	0.1	0.3	443	0.5	0.0	18.0	22	25.6	0.0
2/5/10 15:30	4.6	660	8.6	0.3	6.6	590	12.4	0.4	1.2	531	2.2	0.1	0.2	443	0.4	0.0	15.0	22	21.1	0.0
2/5/10 16:00	3.6	673	6.7	0.3	6.4	599	12.0	0.4	1.2	536	2.2	0.1	0.2	443	0.4	0.0	16.0	22	22.6	0.0
2/5/10 16:30	3.2	667	5.9	0.2	6.3	593	11.8	0.4	1.0	531	1.8	0.1	0.2	439	0.4	0.0	15.0	22	21.1	0.0
2/5/10 17:00	3.2	667	5.9	0.2	6.1	593	11.4	0.4	1.0	531	1.8	0.1	0.2	439	0.4	0.0	16.0	22	22.6	0.0
2/5/10 17:30	3.9	667	7.3	0.3	6.6	593	12.4	0.4	1.0	531	1.8	0.1	0.2	439	0.4	0.0	14.0	22	19.6	0.0
2/5/10 18:00	5.2	667	9.7	0.4	6.1	593	11.4	0.4	0.9	531	1.6	0.0	0.2	439	0.4	0.0	13.0	22	18.1	0.0
2/5/10 18:30	4.2	667	7.8	0.3	6.5	593	12.2	0.4	0.8	531	1.4	0.0	0.2	439	0.4	0.0	12.0	22	16.6	0.0
2/5/10 19:00	3.7	667	6.9	0.3	6.0	592	11.3	0.4	0.7	529	1.3	0.0	0.2	435	0.4	0.0	12.0	22	16.6	0.0
2/5/10 19:30	3.2	667	5.9	0.2	6.6	591	12.4	0.4	1.7	527	3.1	0.1	0.2	431	0.4	0.0	14.0	22	19.6	0.0
2/5/10 20:00	3.2	660	5.9	0.2	6.0	587	11.3	0.4	0.9	526	1.6	0.0	0.2	435	0.4	0.0	12.0	22	16.6	0.0
2/5/10 20:30	3.0	660	5.6	0.2	6.1	586	11.4	0.4	0.9	524	1.6	0.0	0.2	431	0.4	0.0	13.0	22	18.1	0.0
2/5/10 21:00	2.4	660	4.4	0.2	5.8	585	10.9	0.4	1.0	522	1.8	0.1	0.3	427	0.5	0.0	12.0	21	16.6	0.0
2/5/10 21:30	2.6	653	4.8	0.2	6.1	581	11.4	0.4	0.9	519	1.6	0.0	0.2	427	0.4	0.0	9.9	21	13.6	0.0
2/5/10 22:00	2.1	660	3.9	0.1	6.1	585	11.4	0.4	0.9	522	1.6	0.0	0.2	427	0.4	0.0	13.0	21	18.1	0.0
2/5/10 22:30	2.3	653	4.2	0.2	6.1	579	11.4	0.4	0.9	517	1.6	0.0	0.3	423	0.5	0.0	13.0	21	18.1	0.0
2/5/10 23:00	2.3	647	4.2	0.2	6.0	575	11.3	0.4	1.0	514	1.8	0.1	0.2	423	0.4	0.0	13.0	21	18.1	0.0
2/5/10 23:30	2.1	653	3.9	0.1	6.1	578	11.4	0.4	1.0	515	1.8	0.1	0.2	419	0.4	0.0	11.0	21	15.2	0.0
2/6/10 0:00	2.1	653	3.9	0.1	6.3	578	11.8	0.4	0.9	515	1.6	0.0	0.2	419	0.4	0.0	11.0	21	15.2	0.0
2/6/10 0:30	2.1	647	3.9	0.1	6.0	574	11.3	0.4	1.2	512	1.3	0.0	0.4	419	0.7	0.0	8.6	21	11.7	0.0
2/6/10 1:00	2.0	641	3.7	0.1	6.3	570	11.8	0.4	1.2	510	2.2	0.1	0.3	419	0.5	0.0	10.0	21	13.7	0.0
2/6/10 1:30	2.1	647	3.9	0.1	5.9	572	11.1	0.4	0.8	510	1.4	0.0	0.2	416	0.4	0.0	9.6	21	13.1	0.0
2/6/10 2:00	2.2	641	4.0	0.1	5.9	567	11.1	0.4	0.8	505	1.4	0.0	0.8	412	1.4	0.0	9.7	21	13.3	0.0
2/6/10 2:30	2.6	641	4.8	0.2	5.7	567	10.7	0.3	0.7	505	1.3	0.0	0.2	412	0.4	0.0	9.5	21	13.0	0.0
2/6/10 3:00	2.6	641	4.8	0.2	6.0	567	11.3	0.4	0.7	505	1.3	0.0	0.3	412	0.5	0.0	11.0	21	15.2	0.0
2/6/10 3:30	2.1	635	3.9	0.1	5.9	562	11.1	0.3	0.6	500	1.1	0.0	0.2	408	0.4	0.0	12.0	21	16.6	0.0
2/6/10 4:00	2.1	635	3.9	0.1	6.0	563	11.3	0.4	1.3	503	2.4	0.1	0.2	412	0.4	0.0	10.0	21	13.7	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/6/10 4:30	2.0	635	3.7	0.1	5.8	562	10.9	0.3	0.6	500	1.1	0.0	0.2	408	0.4	0.0	9.5	21	13.0	0.0
2/6/10 5:00	2.1	635	3.9	0.1	5.9	562	11.1	0.3	0.8	500	1.4	0.0	0.3	408	0.5	0.0	8.7	21	11.8	0.0
2/6/10 5:30	2.5	629	4.6	0.2	5.8	557	10.9	0.3	0.8	496	1.4	0.0	0.3	404	0.5	0.0	8.3	20	11.3	0.0
2/6/10 6:00	2.1	629	3.9	0.1	6.3	557	11.8	0.4	0.7	496	1.3	0.0	0.2	404	0.4	0.0	11.0	20	15.2	0.0
2/6/10 6:30	2.0	629	3.7	0.1	5.9	557	11.1	0.3	0.6	496	1.1	0.0	0.2	404	0.4	0.0	7.8	20	10.5	0.0
2/6/10 7:00	2.1	629	3.9	0.1	6.4	555	12.0	0.4	0.7	493	1.3	0.0	0.2	401	0.4	0.0	7.5	20	10.1	0.0
2/6/10 7:30	2.3	629	4.2	0.1	6.0	555	11.3	0.4	0.7	493	1.3	0.0	0.2	401	0.4	0.0	8.7	20	11.8	0.0
2/6/10 8:00	2.2	623	4.0	0.1	6.2	550	11.6	0.4	0.6	489	1.1	0.0	0.2	397	0.4	0.0	8.6	20	11.7	0.0
2/6/10 8:30	2.2	623	4.0	0.1	6.3	550	11.8	0.4	0.7	489	1.3	0.0	0.2	397	0.4	0.0	8.1	20	11.0	0.0
2/6/10 9:00	2.1	623	3.9	0.1	6.0	550	11.3	0.3	0.9	489	1.6	0.0	0.2	397	0.4	0.0	7.1	20	9.5	0.0
2/6/10 9:30	1.8	617	3.3	0.1	6.0	545	11.3	0.3	0.8	484	1.4	0.0	0.2	393	0.4	0.0	6.6	20	8.8	0.0
2/6/10 10:00	2.0	611	3.7	0.1	6.0	541	11.3	0.3	1.0	482	1.8	0.0	0.3	393	0.5	0.0	6.8	20	9.1	0.0
2/6/10 10:30	1.9	617	3.5	0.1	6.0	544	11.3	0.3	0.7	482	1.3	0.0	0.2	390	0.4	0.0	6.6	20	8.8	0.0
2/6/10 11:00	3.4	611	6.3	0.2	6.5	540	12.2	0.4	1.0	480	1.8	0.0	0.2	390	0.4	0.0	7.2	20	9.7	0.0
2/6/10 11:30	2.0	611	3.7	0.1	6.0	540	11.3	0.3	0.9	480	1.6	0.0	0.2	390	0.4	0.0	7.8	20	10.5	0.0
2/6/10 12:00	2.0	611	3.7	0.1	5.7	538	10.7	0.3	0.9	478	1.6	0.0	0.2	386	0.4	0.0	6.9	19	9.2	0.0
2/6/10 12:30	2.0	605	3.7	0.1	5.7	536	10.7	0.3	1.0	477	1.8	0.0	0.2	390	0.4	0.0	6.9	20	9.2	0.0
2/6/10 13:00	1.9	611	3.5	0.1	6.8	538	12.8	0.4	0.9	478	1.6	0.0	0.3	386	0.5	0.0	8.7	19	11.8	0.0
2/6/10 13:30	2.0	605	3.7	0.1	6.4	533	12.0	0.4	0.7	473	1.3	0.0	0.2	382	0.4	0.0	8.0	19	10.8	0.0
2/6/10 14:00	2.1	605	3.9	0.1	6.0	533	11.3	0.3	0.6	473	1.1	0.0	0.2	382	0.4	0.0	7.6	19	10.2	0.0
2/6/10 14:30	2.1	605	3.9	0.1	6.1	533	11.4	0.3	1.4	473	2.6	0.1	0.2	382	0.4	0.0	6.9	19	9.2	0.0
2/6/10 15:00	1.9	605	3.5	0.1	5.9	533	11.1	0.3	0.8	473	1.4	0.0	0.2	382	0.4	0.0	6.5	19	8.7	0.0
2/6/10 15:30	2.1	599	3.9	0.1	6.3	529	11.8	0.4	0.7	471	1.3	0.0	0.2	382	0.4	0.0	6.9	19	9.2	0.0
2/6/10 16:00	2.0	599	3.7	0.1	5.9	528	11.1	0.3	0.9	468	1.6	0.0	0.2	379	0.4	0.0	7.5	19	10.1	0.0
2/6/10 16:30	2.3	599	4.2	0.1	6.0	528	11.3	0.3	0.7	468	1.3	0.0	0.2	379	0.4	0.0	9.4	19	12.8	0.0
2/6/10 17:00	2.2	599	4.0	0.1	6.3	528	11.8	0.4	0.7	468	1.3	0.0	0.9	379	1.6	0.0	12.0	19	16.6	0.0
2/6/10 17:30	1.8	599	3.3	0.1	6.3	528	11.8	0.4	1.3	468	2.4	0.1	0.2	379	0.4	0.0	22.0	19	31.7	0.0
2/6/10 18:00	1.9	599	3.5	0.1	6.0	528	11.3	0.3	1.9	468	3.5	0.1	0.2	379	0.4	0.0	64.0	19	98.5	0.1
2/6/10 18:30	1.9	593	3.5	0.1	6.4	524	12.0	0.4	0.6	466	1.1	0.0	0.3	379	0.5	0.0	46.0	19	69.4	0.1
2/6/10 19:00	2.0	599	3.7	0.1	6.2	527	11.6	0.3	0.7	466	1.3	0.0	0.2	375	0.4	0.0	56.0	19	85.5	0.1
2/6/10 19:30	1.9	593	3.5	0.1	5.9	522	11.1	0.3	0.7	462	1.3	0.0	0.3	372	0.5	0.0	56.0	19	85.5	0.1
2/6/10 20:00	2.0	599	3.7	0.1	6.0	527	11.3	0.3	0.7	466	1.3	0.0	0.2	375	0.4	0.0	28.0	19	40.9	0.0
2/6/10 20:30	2.0	599	3.7	0.1	6.0	526	11.3	0.3	0.8	464	1.4	0.0	0.2	372	0.4	0.0	19.0	19	27.1	0.0
2/6/10 21:00	1.9	593	3.5	0.1	6.2	522	11.6	0.3	1.1	462	2.0	0.1	0.2	372	0.4	0.0	18.0	19	25.6	0.0
2/6/10 21:30	2.0	593	3.7	0.1	6.1	522	11.4	0.3	1.6	462	2.9	0.1	0.3	372	0.5	0.0	29.0	19	42.5	0.0
2/6/10 22:00	2.0	593	3.7	0.1	6.2	521	11.6	0.3	1.7	460	3.1	0.1	0.3	368	0.5	0.0	23.0	19	33.2	0.0
2/6/10 22:30	2.0	588	3.7	0.1	6.6	517	12.4	0.4	1.8	457	3.3	0.1	0.2	368	0.4	0.0	17.0	19	24.1	0.0
2/6/10 23:00	2.0	593	3.7	0.1	6.9	520	13.0	0.4	1.9	458	3.5	0.1	0.2	365	0.4	0.0	24.0	18	34.8	0.0
2/6/10 23:30	2.0	588	3.7	0.1	7.2	517	13.6	0.4	1.8	457	3.3	0.1	0.2	368	0.4	0.0	20.0	19	28.6	0.0
2/7/10 0:00	2.0	582	3.7	0.1	7.5	512	14.1	0.4	1.2	453	2.2	0.1	0.2	365	0.4	0.0	15.0	18	21.1	0.0
2/7/10 0:30	2.0	582	3.7	0.1	7.1	511	13.4	0.4	0.9	451	1.6	0.0	0.2	361	0.4	0.0	15.0	18	21.1	0.0
2/7/10 1:00	1.9	582	3.5	0.1	7.4	511	13.9	0.4	1.1	451	2.0	0.1	0.2	361	0.4	0.0	11.0	18	15.2	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/7/10 1:30	2.0	576	3.7	0.1	6.9	507	13.0	0.4	1.0	449	1.8	0.0	0.2	361	0.4	0.0	10.0	18	13.7	0.0
2/7/10 2:00	2.0	576	3.7	0.1	7.1	507	13.4	0.4	0.9	449	1.6	0.0	0.2	361	0.4	0.0	9.8	18	13.4	0.0
2/7/10 2:30	1.9	576	3.5	0.1	6.9	506	13.0	0.4	0.9	447	1.6	0.0	0.2	358	0.4	0.0	10.0	18	13.7	0.0
2/7/10 3:00	2.0	570	3.7	0.1	7.1	502	13.4	0.4	0.9	444	1.6	0.0	0.2	358	0.4	0.0	9.5	18	13.0	0.0
2/7/10 3:30	2.3	565	4.2	0.1	6.6	497	12.4	0.3	0.9	440	1.6	0.0	0.2	354	0.4	0.0	13.0	18	18.1	0.0
2/7/10 4:00	2.1	570	3.9	0.1	6.7	501	12.6	0.4	1.3	442	2.4	0.1	0.2	354	0.4	0.0	15.0	18	21.1	0.0
2/7/10 4:30	2.2	565	4.0	0.1	6.8	496	12.8	0.4	0.7	438	1.3	0.0	0.3	351	0.5	0.0	13.0	18	18.1	0.0
2/7/10 5:00	2.5	570	4.6	0.1	6.8	500	12.8	0.4	0.6	440	1.1	0.0	0.2	351	0.4	0.0	11.0	18	15.2	0.0
2/7/10 5:30	2.8	565	5.2	0.2	6.9	496	13.0	0.4	0.7	438	1.3	0.0	0.2	351	0.4	0.0	10.0	18	13.7	0.0
2/7/10 6:00	2.5	565	4.6	0.1	6.8	496	12.8	0.4	0.7	438	1.3	0.0	0.2	351	0.4	0.0	8.0	18	10.8	0.0
2/7/10 6:30	2.7	559	5.0	0.2	6.7	492	12.6	0.3	0.7	436	1.3	0.0	0.2	351	0.4	0.0	12.0	18	16.6	0.0
2/7/10 7:00	2.5	565	4.6	0.1	6.5	495	12.2	0.3	0.6	436	1.1	0.0	0.2	347	0.4	0.0	13.0	18	18.1	0.0
2/7/10 7:30	2.4	559	4.4	0.1	6.6	491	12.4	0.3	0.8	434	1.4	0.0	0.2	347	0.4	0.0	12.0	18	16.6	0.0
2/7/10 8:00	2.5	559	4.6	0.1	6.6	490	12.4	0.3	0.8	432	1.4	0.0	0.3	344	0.4	0.0	11.0	17	15.2	0.0
2/7/10 8:30	2.3	559	4.2	0.1	6.3	490	11.8	0.3	0.7	432	1.3	0.0	0.2	344	0.4	0.0	9.3	17	12.7	0.0
2/7/10 9:00	2.5	559	4.6	0.1	6.5	490	12.2	0.3	0.7	432	1.3	0.0	0.2	344	0.5	0.0	7.2	17	9.7	0.0
2/7/10 9:30	2.3	553	4.2	0.1	6.3	486	11.8	0.3	0.8	429	1.4	0.0	0.3	344	0.5	0.0	8.5	17	11.5	0.0
2/7/10 10:00	2.3	553	4.2	0.1	6.5	486	12.2	0.3	0.7	429	1.3	0.0	0.2	344	0.4	0.0	11.0	17	15.2	0.0
2/7/10 10:30	2.0	553	3.7	0.1	6.4	485	12.0	0.3	0.7	427	1.3	0.0	0.2	341	0.4	0.0	8.5	17	11.5	0.0
2/7/10 11:00	2.1	553	3.9	0.1	6.8	485	12.8	0.3	0.7	427	1.3	0.0	0.2	341	0.4	0.0	6.9	17	9.2	0.0
2/7/10 11:30	2.2	548	4.0	0.1	6.6	481	12.4	0.3	0.7	425	1.3	0.0	0.2	341	0.4	0.0	6.5	17	8.7	0.0
2/7/10 12:00	2.0	548	3.7	0.1	7.0	481	13.2	0.4	0.7	425	1.3	0.0	0.2	337	0.4	0.0	17.0	17	24.1	0.0
2/7/10 12:30	2.0	548	3.7	0.1	6.8	480	12.8	0.3	0.6	423	1.1	0.0	0.2	337	0.4	0.0	17.0	17	24.1	0.0
2/7/10 13:00	2.1	548	3.9	0.1	6.6	480	12.4	0.3	0.7	423	1.3	0.0	0.2	337	0.4	0.0	55.0	17	83.9	0.1
2/7/10 13:30	2.2	548	4.0	0.1	6.2	480	11.6	0.3	0.7	423	1.3	0.0	0.2	337	0.4	0.0	43.0	17	64.6	0.1
2/7/10 14:00	2.0	542	3.7	0.1	6.8	476	12.8	0.3	0.6	421	1.1	0.0	0.3	337	0.5	0.0	300.0	17	508.2	0.5
2/7/10 14:30	2.0	542	3.7	0.1	6.8	476	12.8	0.3	0.6	421	1.1	0.0	0.2	337	0.4	0.0	160.0	17	260.7	0.3
2/7/10 15:00	2.0	531	3.7	0.1	6.6	468	12.4	0.3	0.9	414	1.6	0.0	0.2	334	0.4	0.0	140.0	17	226.2	0.2
2/7/10 15:30	2.0	537	3.7	0.1	7.0	472	13.2	0.3	0.5	417	0.9	0.0	0.5	334	0.9	0.0	150.0	17	243.4	0.2
2/7/10 16:00	2.2	537	4.0	0.1	6.5	472	12.2	0.3	0.7	417	1.3	0.0	0.2	334	0.4	0.0	80.0	17	124.8	0.1
2/7/10 16:30	1.9	537	3.5	0.1	6.6	470	12.4	0.3	1.2	415	2.2	0.1	0.3	331	0.5	0.0	32.0	17	47.2	0.0
2/7/10 17:00	2.0	542	3.7	0.1	6.5	475	12.2	0.3	1.7	419	3.1	0.1	0.3	334	0.5	0.0	26.0	17	37.8	0.0
2/7/10 17:30	1.9	537	3.5	0.1	6.2	472	11.6	0.3	3.4	417	6.3	0.1	0.2	334	0.4	0.0	46.0	17	69.4	0.1
2/7/10 18:00	2.0	531	3.7	0.1	7.1	468	13.4	0.4	4.8	414	9.0	0.2	0.3	334	0.5	0.0	20.0	17	28.6	0.0
2/7/10 18:30	2.1	542	3.9	0.1	6.8	474	12.8	0.3	4.8	417	9.0	0.2	0.2	331	0.5	0.0	14.0	17	19.6	0.0
2/7/10 19:00	1.9	537	3.5	0.1	7.7	469	14.5	0.4	4.4	413	8.2	0.2	0.2	327	0.4	0.0	12.0	17	16.6	0.0
2/7/10 19:30	1.9	531	3.5	0.1	8.9	466	16.8	0.4	4.0	410	7.4	0.2	0.3	327	0.5	0.0	15.0	17	21.1	0.0
2/7/10 20:00	2.2	537	4.0	0.1	10.1	469	19.1	0.5	3.0	413	5.6	0.1	0.2	327	0.4	0.0	20.0	17	28.6	0.0
2/7/10 20:30	2.0	531	3.7	0.1	9.7	466	18.4	0.5	2.2	410	4.0	0.1	0.2	327	0.4	0.0	21.0	17	30.2	0.0
2/7/10 21:00	2.0	537	3.7	0.1	9.8	469	18.6	0.5	1.7	413	3.1	0.1	0.2	327	0.4	0.0	16.0	17	22.6	0.0
2/7/10 21:30	2.1	531	3.9	0.1	9.1	465	17.2	0.4	1.4	408	2.6	0.1	0.2	324	0.4	0.0	14.0	17	19.6	0.0
2/7/10 22:00	2.0	531	3.7	0.1	8.8	465	16.6	0.4	1.1	408	2.0	0.0	0.2	324	0.4	0.0	14.0	17	19.6	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/7/10 22:30	2.3	526	4.2	0.1	7.9	460	14.9	0.4	0.9	404	1.6	0.0	0.3	321	0.5	0.0	13.0	16	18.1	0.0
2/7/10 23:00	2.0	526	3.7	0.1	7.3	460	13.7	0.4	1.0	404	1.8	0.0	0.2	321	0.4	0.0	12.0	16	16.6	0.0
2/7/10 23:30	2.0	521	3.7	0.1	7.2	455	13.6	0.3	0.9	400	1.6	0.0	0.3	318	0.5	0.0	16.0	16	22.6	0.0
2/8/10 0:00	1.9	526	3.5	0.1	7.0	459	13.2	0.3	0.9	402	1.6	0.0	0.2	318	0.4	0.0	11.0	16	15.2	0.0
2/8/10 0:30	2.8	521	5.2	0.2	6.7	455	12.6	0.3	0.9	400	1.6	0.0	0.3	318	0.5	0.0	13.0	16	18.1	0.0
2/8/10 1:00	3.5	521	6.5	0.2	6.6	455	12.4	0.3	0.8	400	1.4	0.0	0.2	318	0.4	0.0	12.0	16	16.6	0.0
2/8/10 1:30	4.0	515	7.4	0.2	6.8	451	12.8	0.3	0.9	396	1.6	0.0	0.2	314	0.4	0.0	9.4	16	12.8	0.0
2/8/10 2:00	5.0	515	9.3	0.3	7.0	451	13.2	0.3	0.7	396	1.3	0.0	0.2	314	0.4	0.0	8.4	16	11.4	0.0
2/8/10 2:30	5.3	515	9.9	0.3	10.5	451	19.9	0.5	0.7	396	1.3	0.0	0.2	314	0.4	0.0	9.3	16	12.7	0.0
2/8/10 3:00	4.9	515	9.2	0.3	6.8	449	12.8	0.3	0.9	394	1.6	0.0	0.2	311	0.4	0.0	8.5	16	11.5	0.0
2/8/10 3:30	4.6	510	8.6	0.2	6.8	446	12.8	0.3	0.7	392	1.3	0.0	0.2	311	0.4	0.0	9.2	16	12.6	0.0
2/8/10 4:00	4.3	510	8.0	0.2	6.7	446	12.6	0.3	0.9	392	1.6	0.0	0.4	311	0.7	0.0	11.0	16	15.2	0.0
2/8/10 4:30	3.8	515	7.1	0.2	6.2	449	12.4	0.3	0.9	394	1.6	0.0	0.2	311	0.4	0.0	8.9	16	12.1	0.0
2/8/10 5:00	4.2	510	7.8	0.2	6.3	445	11.8	0.3	0.7	390	1.3	0.0	0.2	308	0.4	0.0	6.7	16	9.0	0.0
2/8/10 5:30	3.1	510	5.7	0.2	6.1	445	11.4	0.3	0.6	390	1.1	0.0	0.2	308	0.4	0.0	6.3	16	8.4	0.0
2/8/10 6:00	2.9	504	5.4	0.2	6.5	441	12.2	0.3	0.6	388	1.1	0.0	0.2	308	0.4	0.0	5.7	16	7.5	0.0
2/8/10 6:30	2.9	504	5.4	0.2	6.6	441	12.4	0.3	0.6	388	1.1	0.0	0.3	308	0.5	0.0	6.8	16	9.1	0.0
2/8/10 7:00	3.3	499	6.1	0.2	6.2	437	11.6	0.3	0.6	384	1.1	0.0	0.4	305	0.7	0.0	8.0	16	10.8	0.0
2/8/10 7:30	2.7	504	5.0	0.1	6.1	441	11.4	0.3	0.9	388	1.6	0.0	0.2	308	0.4	0.0	6.5	16	8.7	0.0
2/8/10 8:00	2.6	499	4.8	0.1	6.0	437	11.3	0.3	0.6	384	1.1	0.0	0.2	305	0.4	0.0	6.7	16	9.0	0.0
2/8/10 8:30	2.6	499	4.8	0.1	6.4	437	12.0	0.3	0.6	384	1.1	0.0	0.2	305	0.4	0.0	6.9	16	9.2	0.0
2/8/10 9:00	3.0	499	5.6	0.2	6.7	436	12.6	0.3	0.6	382	1.1	0.0	0.2	302	0.4	0.0	6.7	15	9.0	0.0
2/8/10 9:30	2.9	499	5.4	0.2	6.5	436	12.2	0.3	1.6	382	2.9	0.1	0.5	302	0.9	0.0	5.6	15	7.4	0.0
2/8/10 10:00	2.9	494	5.4	0.1	6.3	432	11.8	0.3	0.7	380	1.3	0.0	1.7	302	3.1	0.1	6.4	15	8.5	0.0
2/8/10 10:30	2.8	499	5.2	0.1	6.4	436	12.0	0.3	0.7	382	1.3	0.0	0.3	302	0.5	0.0	7.1	15	9.5	0.0
2/8/10 11:00	2.8	494	5.2	0.1	6.3	431	11.8	0.3	0.7	378	1.3	0.0	0.2	299	0.4	0.0	6.1	15	8.1	0.0
2/8/10 11:30	2.8	494	5.2	0.1	6.5	431	12.2	0.3	0.6	378	1.1	0.0	0.2	299	0.4	0.0	5.4	15	7.1	0.0
2/8/10 12:00	2.8	494	5.2	0.1	6.0	431	11.3	0.3	0.6	378	1.1	0.0	0.2	299	0.4	0.0	6.2	15	8.3	0.0
2/8/10 12:30	3.0	489	5.6	0.2	6.0	428	11.3	0.3	0.6	376	1.1	0.0	0.2	299	0.4	0.0	5.3	15	7.0	0.0
2/8/10 13:00	2.8	494	5.2	0.1	6.0	431	11.3	0.3	0.6	378	1.1	0.0	0.2	299	0.4	0.0	6.9	15	9.2	0.0
2/8/10 13:30	2.5	484	4.6	0.1	6.0	423	11.3	0.3	0.6	372	1.1	0.0	0.2	296	0.4	0.0	8.9	15	12.1	0.0
2/8/10 14:00	2.5	494	4.6	0.1	7.1	430	13.4	0.3	0.5	376	0.9	0.0	0.2	296	0.4	0.0	8.0	15	10.8	0.0
2/8/10 14:30	2.7	484	5.0	0.1	6.3	423	11.8	0.3	0.6	372	1.1	0.0	0.2	296	0.4	0.0	9.5	15	13.0	0.0
2/8/10 15:00	2.5	489	4.6	0.1	6.1	426	11.4	0.3	0.5	372	0.9	0.0	0.3	293	0.5	0.0	10.0	15	13.7	0.0
2/8/10 15:30	2.8	489	5.2	0.1	6.4	426	12.0	0.3	0.6	372	1.1	0.0	0.2	293	0.4	0.0	11.0	15	15.2	0.0
2/8/10 16:00	2.6	489	4.8	0.1	6.3	426	11.8	0.3	0.4	372	0.7	0.0	0.2	293	0.4	0.0	11.0	15	15.2	0.0
2/8/10 16:30	2.6	484	4.8	0.1	6.7	422	12.6	0.3	0.5	370	0.9	0.0	0.2	293	0.4	0.0	10.0	15	13.7	0.0
2/8/10 17:00	2.8	484	5.2	0.1	6.5	422	12.2	0.3	0.6	370	1.1	0.0	0.2	293	0.4	0.0	8.7	15	11.8	0.0
2/8/10 17:30	2.5	478	4.6	0.1	6.9	419	13.0	0.3	0.6	368	1.1	0.0	0.2	293	0.4	0.0	11.0	15	15.2	0.0
2/8/10 18:00	2.4	478	4.4	0.1	6.3	418	11.8	0.3	0.7	366	1.3	0.0	0.3	290	0.5	0.0	10.0	15	13.7	0.0
2/8/10 18:30	2.9	478	5.4	0.1	6.3	418	11.8	0.3	0.6	366	1.1	0.0	0.2	290	0.4	0.0	7.0	15	9.4	0.0
2/8/10 19:00	2.6	478	4.8	0.1	6.3	417	11.8	0.3	0.6	365	1.1	0.0	0.2	286	0.4	0.0	7.6	15	10.2	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/8/10 19:30	2.6	478	4.8	0.1	6.5	417	12.2	0.3	0.6	365	1.1	0.0	0.3	286	0.5	0.0	12.0	15	16.6	0.0
2/8/10 20:00	2.8	478	5.2	0.1	6.7	417	12.6	0.3	0.6	365	1.1	0.0	0.2	286	0.4	0.0	27.0	15	39.4	0.0
2/8/10 20:30	2.7	473	5.0	0.1	6.6	413	12.4	0.3	0.7	362	1.3	0.0	0.2	286	0.4	0.0	12.0	15	16.6	0.0
2/8/10 21:00	2.6	473	4.8	0.1	6.9	412	13.0	0.3	0.6	361	1.1	0.0	0.3	283	0.5	0.0	7.3	15	9.8	0.0
2/8/10 21:30	2.6	473	4.8	0.1	6.8	412	12.8	0.3	0.6	361	1.1	0.0	0.2	283	0.4	0.0	7.4	15	10.0	0.0
2/8/10 22:00	2.7	473	5.0	0.1	5.9	412	11.1	0.3	0.6	361	1.1	0.0	0.2	283	0.4	0.0	7.7	15	10.4	0.0
2/8/10 22:30	2.5	473	4.6	0.1	7.3	412	13.7	0.3	0.8	361	1.4	0.0	0.2	283	0.4	0.0	7.8	15	10.5	0.0
2/8/10 23:00	2.6	468	4.8	0.1	1.4	408	2.6	0.1	1.2	357	2.2	0.0	0.2	280	0.4	0.0	6.8	14	9.1	0.0
2/8/10 23:30	2.6	463	4.8	0.1	1.2	404	2.2	0.0	0.7	355	1.3	0.0	0.2	280	0.4	0.0	7.9	14	10.7	0.0
2/9/10 0:00	2.4	468	4.4	0.1	1.3	408	2.4	0.1	0.9	357	1.6	0.0	0.2	280	0.4	0.0	8.5	14	11.5	0.0
2/9/10 0:30	2.6	463	4.8	0.1	1.5	404	2.7	0.1	0.8	355	1.4	0.0	0.2	280	0.4	0.0	7.0	14	9.4	0.0
2/9/10 1:00	2.7	468	5.0	0.1	1.3	408	2.4	0.1	1.1	357	2.0	0.0	0.3	280	0.5	0.0	6.1	14	8.1	0.0
2/9/10 1:30	2.5	468	4.6	0.1	1.8	407	3.3	0.1	0.6	355	1.1	0.0	0.2	277	0.4	0.0	5.8	14	7.7	0.0
2/9/10 2:00	2.8	463	5.2	0.1	1.5	403	2.7	0.1	0.6	353	1.1	0.0	0.2	277	0.4	0.0	6.3	14	8.4	0.0
2/9/10 2:30	2.7	463	5.0	0.1	2.3	403	4.2	0.1	1.0	353	1.8	0.0	0.2	277	0.4	0.0	5.9	14	7.8	0.0
2/9/10 3:00	2.7	463	5.0	0.1	1.5	403	2.7	0.1	0.6	353	1.1	0.0	0.2	277	0.4	0.0	5.2	14	6.8	0.0
2/9/10 3:30	2.6	458	4.8	0.1	1.6	399	2.9	0.1	0.6	349	1.1	0.0	0.2	275	0.4	0.0	4.9	14	6.4	0.0
2/9/10 4:00	2.7	463	5.0	0.1	1.4	402	2.6	0.1	1.2	351	2.2	0.0	0.2	275	0.4	0.0	5.8	14	7.7	0.0
2/9/10 4:30	2.7	453	5.0	0.1	1.6	396	2.9	0.1	0.6	347	1.1	0.0	0.2	275	0.4	0.0	4.6	14	6.0	0.0
2/9/10 5:00	2.8	453	5.2	0.1	1.4	395	2.6	0.1	0.5	345	0.9	0.0	0.2	272	0.4	0.0	5.3	14	7.0	0.0
2/9/10 5:30	2.6	453	4.8	0.1	1.4	395	2.6	0.1	0.7	345	1.3	0.0	0.3	272	0.5	0.0	5.3	14	7.0	0.0
2/9/10 6:00	2.9	453	5.4	0.1	1.5	395	2.7	0.1	0.6	345	1.1	0.0	0.4	272	0.7	0.0	6.3	14	8.4	0.0
2/9/10 6:30	2.7	453	5.0	0.1	1.4	395	2.6	0.1	0.5	345	0.9	0.0	0.2	272	0.4	0.0	6.2	14	8.3	0.0
2/9/10 7:00	2.6	453	4.8	0.1	1.2	395	2.2	0.0	0.5	345	0.9	0.0	0.2	272	0.4	0.0	6.1	14	8.1	0.0
2/9/10 7:30	2.9	448	5.4	0.1	1.9	390	3.5	0.1	0.6	342	1.1	0.0	0.2	269	0.4	0.0	5.1	14	6.7	0.0
2/9/10 8:00	2.8	453	5.2	0.1	1.2	394	2.2	0.0	0.7	344	1.3	0.0	0.4	269	0.4	0.0	5.3	14	7.0	0.0
2/9/10 8:30	2.7	448	5.0	0.1	1.1	390	2.0	0.0	0.6	342	1.1	0.0	0.2	269	0.4	0.0	5.8	14	7.7	0.0
2/9/10 9:00	3.3	448	6.1	0.2	1.0	390	1.8	0.0	0.5	342	0.9	0.0	0.2	269	0.4	0.0	5.2	14	6.8	0.0
2/9/10 9:30	2.9	448	5.4	0.1	1.3	390	2.4	0.1	0.8	342	1.4	0.0	0.9	269	1.6	0.0	5.4	14	7.1	0.0
2/9/10 10:00	2.8	443	5.2	0.1	1.0	386	1.8	0.0	0.5	338	0.9	0.0	0.2	266	0.4	0.0	3.9	14	5.0	0.0
2/9/10 10:30	2.6	443	4.8	0.1	1.0	386	1.8	0.0	0.6	338	1.1	0.0	0.2	266	0.4	0.0	4.5	14	5.9	0.0
2/9/10 11:00	2.8	443	5.2	0.1	1.1	386	2.0	0.0	0.5	338	0.9	0.0	0.2	266	0.4	0.0	4.1	14	5.3	0.0
2/9/10 11:30	2.8	443	5.2	0.1	0.8	385	1.4	0.0	0.6	336	1.1	0.0	0.2	263	0.4	0.0	4.8	14	6.3	0.0
2/9/10 12:00	2.5	438	4.6	0.1	2.9	383	5.4	0.1	0.5	336	0.9	0.0	0.3	266	0.5	0.0	4.0	14	5.2	0.0
2/9/10 12:30	2.8	443	5.2	0.1	1.1	385	2.0	0.0	0.4	336	0.7	0.0	0.4	263	0.7	0.0	4.1	14	5.3	0.0
2/9/10 13:00	2.6	443	4.8	0.1	1.2	384	2.2	0.0	0.6	335	1.1	0.0	0.7	260	1.3	0.0	4.2	13	5.5	0.0
2/9/10 13:30	2.7	438	5.0	0.1	1.2	382	2.2	0.0	0.6	334	1.1	0.0	0.2	263	0.4	0.0	4.6	14	6.0	0.0
2/9/10 14:00	2.6	438	4.8	0.1	1.1	382	2.0	0.0	0.6	334	1.1	0.0	0.2	263	0.4	0.0	6.6	14	8.8	0.0
2/9/10 14:30	2.9	433	5.4	0.1	1.9	378	3.5	0.1	0.5	331	0.9	0.0	0.2	260	0.4	0.0	5.2	13	6.8	0.0
2/9/10 15:00	2.5	438	4.6	0.1	1.3	381	2.4	0.1	0.4	333	0.7	0.0	0.2	260	0.4	0.0	4.3	13	5.6	0.0
2/9/10 15:30	2.7	438	5.0	0.1	1.4	381	2.6	0.1	0.4	333	0.7	0.0	0.4	260	0.7	0.0	4.6	13	6.0	0.0
2/9/10 16:00	2.7	433	5.0	0.1	1.5	377	2.7	0.1	0.4	329	0.7	0.0	0.2	257	0.4	0.0	4.6	13	6.0	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/9/10 16:30	2.7	433	5.0	0.1	1.6	377	2.9	0.1	0.4	329	0.7	0.0	0.2	257	0.4	0.0	4.4	13	5.7	0.0
2/9/10 17:00	2.4	433	4.4	0.1	1.6	377	2.9	0.1	0.6	329	1.1	0.0	0.3	257	0.5	0.0	4.0	13	5.2	0.0
2/9/10 17:30	2.4	429	4.4	0.1	1.9	373	3.5	0.1	0.5	327	0.9	0.0	0.2	257	0.4	0.0	8.2	13	11.1	0.0
2/9/10 18:00	2.6	433	4.8	0.1	1.5	376	2.7	0.1	0.4	327	0.7	0.0	0.2	254	0.4	0.0	8.3	13	11.3	0.0
2/9/10 18:30	2.5	429	4.6	0.1	1.6	373	2.9	0.1	0.4	325	0.7	0.0	0.2	254	0.4	0.0	4.7	13	6.2	0.0
2/9/10 19:00	2.7	429	5.0	0.1	4.3	373	8.0	0.2	0.4	325	0.7	0.0	0.2	254	0.4	0.0	4.4	13	5.7	0.0
2/9/10 19:30	2.8	429	5.2	0.1	1.6	373	2.9	0.1	0.8	325	1.4	0.0	0.3	254	0.5	0.0	4.4	13	5.7	0.0
2/9/10 20:00	2.6	429	4.8	0.1	1.5	373	2.7	0.1	0.6	325	1.1	0.0	0.2	254	0.4	0.0	3.8	13	4.9	0.0
2/9/10 20:30	2.7	429	5.0	0.1	1.7	372	3.1	0.1	0.4	324	0.7	0.0	0.2	252	0.4	0.0	4.4	13	5.7	0.0
2/9/10 21:00	2.6	424	4.8	0.1	1.9	368	3.5	0.1	0.4	322	0.7	0.0	0.2	252	0.4	0.0	4.5	13	5.9	0.0
2/9/10 21:30	2.6	419	4.8	0.1	1.9	365	3.5	0.1	0.5	320	0.9	0.0	0.2	252	0.4	0.0	4.5	13	5.9	0.0
2/9/10 22:00	2.6	419	4.8	0.1	1.5	365	2.7	0.1	0.4	320	0.7	0.0	0.4	252	0.7	0.0	4.4	13	5.7	0.0
2/9/10 22:30	2.8	419	5.2	0.1	1.7	365	3.1	0.1	0.6	320	1.1	0.0	0.6	252	1.1	0.0	4.0	13	5.2	0.0
2/9/10 23:00	2.7	419	5.0	0.1	1.6	364	2.9	0.1	0.5	318	0.9	0.0	0.4	249	0.7	0.0	4.6	13	6.0	0.0
2/9/10 23:30	2.5	419	4.6	0.1	1.6	364	2.9	0.1	0.4	318	0.7	0.0	0.5	249	0.9	0.0	5.1	13	6.7	0.0
2/10/10 0:00	3.4	424	6.3	0.2	1.5	367	2.7	0.1	0.4	320	0.7	0.0	0.3	249	0.5	0.0	3.8	13	4.9	0.0
2/10/10 0:30	2.6	414	4.8	0.1	1.9	360	3.5	0.1	0.5	314	0.9	0.0	0.3	246	0.5	0.0	3.8	13	4.9	0.0
2/10/10 1:00	2.4	419	4.4	0.1	2.3	363	4.2	0.1	0.7	316	1.3	0.0	0.2	246	0.4	0.0	4.0	13	5.2	0.0
2/10/10 1:30	2.6	419	4.8	0.1	1.8	363	3.3	0.1	0.5	316	0.9	0.0	0.2	246	0.4	0.0	3.4	13	4.4	0.0
2/10/10 2:00	2.5	414	4.6	0.1	1.5	360	2.7	0.1	0.4	314	0.7	0.0	0.2	246	0.4	0.0	3.5	13	4.5	0.0
2/10/10 2:30	2.6	414	4.8	0.1	3.8	360	7.1	0.1	0.4	314	0.7	0.0	0.2	246	0.4	0.0	3.2	13	4.1	0.0
2/10/10 3:00	2.6	414	4.8	0.1	1.6	360	2.9	0.1	0.4	314	0.7	0.0	0.2	246	0.4	0.0	4.0	13	5.2	0.0
2/10/10 3:30	2.5	410	4.6	0.1	1.5	356	2.7	0.1	1.9	311	3.5	0.1	0.2	243	0.4	0.0	3.1	13	4.0	0.0
2/10/10 4:00	2.9	410	5.4	0.1	1.4	356	2.6	0.1	0.5	311	0.9	0.0	0.2	243	0.4	0.0	3.6	13	4.6	0.0
2/10/10 4:30	2.8	410	5.2	0.1	1.6	356	2.9	0.1	0.5	311	0.9	0.0	0.2	243	0.4	0.0	4.1	13	5.3	0.0
2/10/10 5:00	3.3	405	6.1	0.1	1.8	353	3.3	0.1	0.4	309	0.7	0.0	0.2	243	0.4	0.0	3.2	13	4.1	0.0
2/10/10 5:30	2.7	405	5.0	0.1	1.5	352	2.7	0.1	0.5	307	0.9	0.0	0.2	241	0.4	0.0	5.0	12	6.6	0.0
2/10/10 6:00	2.7	410	5.0	0.1	1.5	355	2.7	0.1	0.5	309	0.9	0.0	0.2	241	0.4	0.0	4.1	12	5.3	0.0
2/10/10 6:30	2.6	405	4.8	0.1	1.4	352	2.6	0.1	0.4	307	0.7	0.0	0.3	241	0.5	0.0	4.4	12	5.7	0.0
2/10/10 7:00	2.7	405	5.0	0.1	1.5	352	2.7	0.1	0.7	307	1.3	0.0	0.2	241	0.4	0.0	3.5	12	4.5	0.0
2/10/10 7:30	2.7	405	5.0	0.1	1.6	352	2.9	0.1	0.4	307	0.7	0.0	0.2	241	0.4	0.0	3.6	12	4.6	0.0
2/10/10 8:00	2.8	405	5.2	0.1	1.3	351	2.4	0.0	0.4	306	0.7	0.0	0.2	238	0.4	0.0	5.1	12	6.7	0.0
2/10/10 8:30	2.6	400	4.8	0.1	1.3	348	2.4	0.0	0.4	304	0.7	0.0	0.2	238	0.4	0.0	3.8	12	4.9	0.0
2/10/10 9:00	2.6	400	4.8	0.1	1.4	348	2.6	0.0	0.4	304	0.7	0.0	0.2	238	0.4	0.0	3.3	12	4.2	0.0
2/10/10 9:30	2.7	400	5.0	0.1	1.7	348	3.1	0.1	0.4	304	0.7	0.0	0.2	238	0.4	0.0	5.6	12	7.4	0.0
2/10/10 10:00	2.8	400	5.2	0.1	1.3	348	2.4	0.0	0.5	304	0.9	0.0	0.5	238	0.9	0.0	3.2	12	4.1	0.0
2/10/10 10:30	2.8	400	5.2	0.1	1.3	347	2.4	0.0	0.5	302	0.9	0.0	0.2	235	0.4	0.0	3.7	12	4.8	0.0
2/10/10 11:00	2.8	400	5.2	0.1	1.3	348	2.4	0.0	0.4	304	0.7	0.0	0.3	238	0.5	0.0	3.4	12	4.4	0.0
2/10/10 11:30	2.9	400	5.4	0.1	1.3	348	2.4	0.0	0.5	304	0.9	0.0	0.2	238	0.4	0.0	2.9	12	3.7	0.0
2/10/10 12:00	2.6	396	4.8	0.1	1.5	345	2.7	0.1	0.4	302	0.7	0.0	0.2	238	0.4	0.0	3.3	12	4.2	0.0
2/10/10 12:30	2.5	400	4.6	0.1	1.4	348	2.6	0.0	0.6	304	1.1	0.0	0.2	238	0.4	0.0	3.0	12	3.8	0.0
2/10/10 13:00	2.5	400	4.6	0.1	1.3	348	2.4	0.0	0.4	304	0.7	0.0	0.2	238	0.4	0.0	2.9	12	3.7	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/10/10 13:30	2.7	400	5.0	0.1	1.6	348	2.9	0.1	0.3	304	0.5	0.0	0.2	238	0.4	0.0	8.0	12	10.8	0.0
2/10/10 14:00	2.7	400	5.0	0.1	1.3	348	2.4	0.0	0.4	304	0.7	0.0	0.2	238	0.4	0.0	14.0	12	19.6	0.0
2/10/10 14:30	3.1	400	5.7	0.1	1.5	349	2.7	0.1	0.4	306	0.7	0.0	0.2	241	0.4	0.0	18.0	12	25.6	0.0
2/10/10 15:00	2.6	400	4.8	0.1	1.5	349	2.7	0.1	0.5	306	0.9	0.0	0.2	241	0.4	0.0	10.0	12	13.7	0.0
2/10/10 15:30	2.7	400	5.0	0.1	1.6	349	2.9	0.1	0.7	306	1.3	0.0	0.2	241	0.4	0.0	8.9	12	12.1	0.0
2/10/10 16:00	2.8	405	5.2	0.1	1.6	352	2.9	0.1	0.4	307	0.7	0.0	0.3	241	0.5	0.0	9.5	12	13.0	0.0
2/10/10 16:30	2.7	405	5.0	0.1	1.7	352	3.1	0.1	0.4	307	0.7	0.0	0.2	241	0.4	0.0	7.5	12	10.1	0.0
2/10/10 17:00	2.6	400	4.8	0.1	1.6	349	2.9	0.1	0.4	306	0.7	0.0	0.2	241	0.4	0.0	6.2	12	8.3	0.0
2/10/10 17:30	2.8	405	5.2	0.1	1.7	352	3.1	0.1	0.6	307	1.1	0.0	0.3	241	0.5	0.0	11.0	12	15.2	0.0
2/10/10 18:00	2.9	405	5.4	0.1	1.8	353	3.3	0.1	0.7	309	1.3	0.0	0.2	243	0.4	0.0	43.0	13	64.6	0.0
2/10/10 18:30	2.6	410	4.8	0.1	2.3	356	4.2	0.1	0.6	311	1.1	0.0	0.6	243	1.1	0.0	40.0	13	59.8	0.0
2/10/10 19:00	2.6	400	4.8	0.1	1.7	350	3.1	0.1	0.7	307	1.3	0.0	0.3	243	0.5	0.0	22.0	13	31.7	0.0
2/10/10 19:30	2.6	405	4.8	0.1	1.7	353	3.1	0.1	0.7	309	1.3	0.0	0.2	243	0.4	0.0	19.0	13	27.1	0.0
2/10/10 20:00	2.8	405	5.2	0.1	2.5	353	4.6	0.1	1.2	309	2.2	0.0	0.2	243	0.4	0.0	31.0	13	45.6	0.0
2/10/10 20:30	2.7	405	5.0	0.1	1.8	353	3.3	0.1	0.7	309	1.3	0.0	0.2	243	0.4	0.0	51.0	13	77.4	0.1
2/10/10 21:00	2.8	410	5.2	0.1	1.9	357	3.5	0.1	0.6	313	1.1	0.0	0.2	246	0.4	0.0	44.0	13	66.2	0.0
2/10/10 21:30	2.6	405	4.8	0.1	2.3	354	4.2	0.1	0.7	311	1.3	0.0	0.2	246	0.4	0.0	54.0	13	82.2	0.1
2/10/10 22:00	2.6	405	4.8	0.1	2.0	354	3.7	0.1	0.7	311	1.3	0.0	0.6	246	1.1	0.0	75.0	13	116.6	0.1
2/10/10 22:30	2.4	405	4.4	0.1	1.9	354	3.5	0.1	1.0	311	1.8	0.0	0.2	246	0.4	0.0	44.0	13	66.2	0.0
2/10/10 23:00	2.8	400	5.2	0.1	1.9	351	3.5	0.1	1.2	310	2.2	0.0	0.2	249	0.4	0.0	63.0	13	96.9	0.1
2/10/10 23:30	2.6	405	4.8	0.1	2.0	355	3.7	0.1	2.5	312	4.6	0.1	0.2	249	0.4	0.0	74.0	13	114.9	0.1
2/11/10 0:00	2.7	410	5.0	0.1	1.9	359	3.5	0.1	3.1	316	5.7	0.1	0.4	252	0.7	0.0	37.0	13	55.0	0.0
2/11/10 0:30	2.6	405	4.8	0.1	2.3	357	4.2	0.1	1.2	317	2.2	0.0	0.2	257	0.4	0.0	20.0	13	28.6	0.0
2/11/10 1:00	2.7	405	5.0	0.1	2.6	358	4.8	0.1	1.5	319	2.7	0.0	0.2	260	0.4	0.0	20.0	13	28.6	0.0
2/11/10 1:30	3.0	405	5.6	0.1	2.6	359	4.8	0.1	1.7	321	3.1	0.1	0.2	263	0.4	0.0	39.0	14	58.2	0.0
2/11/10 2:00	2.6	410	4.8	0.1	2.5	364	4.6	0.1	1.9	326	3.5	0.1	0.2	269	0.4	0.0	57.0	14	87.1	0.1
2/11/10 2:30	2.2	410	4.0	0.1	2.6	366	4.8	0.1	2.0	329	3.7	0.1	0.2	275	0.4	0.0	150.0	14	243.4	0.2
2/11/10 3:00	2.7	414	5.0	0.1	2.7	371	5.0	0.1	1.9	335	3.5	0.1	0.2	280	0.4	0.0	200.0	14	330.4	0.3
2/11/10 3:30	2.5	414	4.6	0.1	3.0	374	5.6	0.1	2.2	340	4.0	0.1	0.3	290	0.5	0.0	300.0	15	508.2	0.4
2/11/10 4:00	2.7	424	5.0	0.1	3.4	384	6.3	0.1	2.2	350	4.0	0.1	0.9	299	1.6	0.0	600.0	15	1061.1	0.9
2/11/10 4:30	3.2	424	5.9	0.1	3.4	387	6.3	0.1	1.8	355	3.3	0.1	0.4	308	0.7	0.0	690.0	16	1230.9	1.1
2/11/10 5:00	2.9	429	5.0	0.1	3.6	393	6.7	0.1	1.8	363	3.3	0.1	0.2	318	0.4	0.0	360.0	16	616.8	0.6
2/11/10 5:30	2.9	433	5.4	0.1	3.4	399	6.3	0.1	1.8	371	3.3	0.1	0.4	327	0.7	0.0	390.0	17	671.5	0.6
2/11/10 6:00	2.8	443	5.2	0.1	3.7	410	6.9	0.2	2.1	382	3.9	0.1	0.3	341	0.5	0.0	270.0	17	454.4	0.4
2/11/10 6:30	2.8	453	5.2	0.1	3.5	421	6.5	0.2	3.6	394	6.7	0.1	0.3	354	0.5	0.0	880.0	18	1593.7	1.6
2/11/10 7:00	3.1	458	5.7	0.1	3.2	430	5.9	0.1	6.1	407	11.4	0.3	0.4	372	0.7	0.0	1000.0	19	1825.5	1.9
2/11/10 7:30	3.2	468	5.9	0.2	3.6	443	6.7	0.2	12.4	422	23.6	0.6	0.3	390	0.5	0.0	990.0	20	1806.1	2.0
2/11/10 8:00	3.2	478	5.9	0.2	4.3	455	8.0	0.2	19.2	434	36.9	0.9	0.3	404	0.5	0.0	620.0	20	1098.7	1.3
2/11/10 8:30	3.1	494	5.7	0.2	5.9	470	11.1	0.3	16.8	450	32.2	0.8	0.3	419	0.5	0.0	720.0	21	1287.8	1.5
2/11/10 9:00	3.3	504	6.1	0.2	9.6	481	18.2	0.5	15.0	461	28.7	0.7	0.4	431	0.7	0.0	990.0	22	1806.1	2.2
2/11/10 9:30	3.4	521	6.3	0.2	14.1	495	26.9	0.7	19.3	474	37.1	1.0	0.3	443	0.5	0.0	190.0	22	312.9	0.4
2/11/10 10:00	4.1	537	7.6	0.2	16.0	512	30.6	0.9	31.4	490	60.9	1.7	0.4	458	0.7	0.0	150.0	23	243.4	0.3

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/11/10 10:30	3.8	548	7.1	0.2	15.0	523	28.7	0.8	42.6	502	83.1	2.3	0.3	471	0.5	0.0	86.0	23	134.8	0.2
2/11/10 11:00	4.2	565	7.8	0.2	15.8	537	30.2	0.9	38.3	514	74.6	2.2	0.3	479	0.5	0.0	79.0	24	123.2	0.2
2/11/10 11:30	3.8	588	7.1	0.2	23.6	554	45.5	1.4	31.7	525	61.5	1.8	0.3	483	0.5	0.0	76.0	24	118.2	0.2
2/11/10 12:00	4.1	611	7.6	0.3	33.0	572	64.1	2.1	21.8	540	42.0	1.3	0.3	491	0.5	0.0	55.0	24	83.9	0.1
2/11/10 12:30	3.9	623	7.3	0.3	32.2	580	62.5	2.0	12.7	545	24.2	0.7	0.3	491	0.5	0.0	44.0	24	66.2	0.1
2/11/10 13:00	4.3	641	8.0	0.3	26.8	594	51.8	1.7	7.6	555	14.3	0.4	0.3	495	0.5	0.0	38.0	25	56.6	0.1
2/11/10 13:30	6.8	653	12.8	0.5	22.0	601	42.4	1.4	5.1	557	9.5	0.3	0.3	491	0.5	0.0	40.0	24	59.8	0.1
2/11/10 14:00	6.6	667	12.4	0.5	14.3	613	27.3	0.9	4.0	568	7.4	0.2	0.3	500	0.5	0.0	41.0	25	61.4	0.1
2/11/10 14:30	8.8	673	16.6	0.6	9.8	615	18.6	0.6	3.1	565	5.7	0.2	0.3	491	0.5	0.0	33.0	24	48.7	0.1
2/11/10 15:00	12.0	673	22.8	0.9	7.2	615	13.6	0.5	2.7	565	5.0	0.2	0.2	491	0.4	0.0	30.0	24	44.0	0.1
2/11/10 15:30	13.0	693	24.8	1.0	5.6	629	10.5	0.4	2.3	576	4.2	0.1	1.0	495	1.8	0.1	26.0	25	37.8	0.1
2/11/10 16:00	13.0	693	24.8	1.0	5.1	628	9.5	0.3	1.8	573	3.3	0.1	0.2	491	0.4	0.0	28.0	24	40.9	0.1
2/11/10 16:30	17.0	700	32.6	1.3	4.3	631	8.0	0.3	1.8	574	3.3	0.1	0.2	487	0.4	0.0	31.0	24	45.6	0.1
2/11/10 17:00	24.0	700	46.3	1.8	4.8	630	9.0	0.3	1.5	571	2.7	0.1	0.3	483	0.5	0.0	30.0	24	44.0	0.1
2/11/10 17:30	25.0	686	48.3	1.9	4.1	621	7.6	0.3	1.7	566	3.1	0.1	0.3	483	0.5	0.0	30.0	24	44.0	0.1
2/11/10 18:00	24.0	693	46.3	1.8	3.7	625	6.9	0.2	1.4	568	2.6	0.1	0.2	483	0.4	0.0	26.0	24	37.8	0.1
2/11/10 18:30	21.0	693	40.4	1.6	3.6	624	6.7	0.2	1.4	566	2.6	0.1	0.3	479	0.5	0.0	26.0	24	37.8	0.1
2/11/10 19:00	16.0	700	30.6	1.2	3.4	627	6.3	0.2	1.4	566	2.6	0.1	0.3	475	0.5	0.0	22.0	24	31.7	0.0
2/11/10 19:30	12.0	693	22.8	0.9	3.8	624	7.1	0.2	2.2	566	4.0	0.1	0.3	479	0.5	0.0	22.0	24	31.7	0.0
2/11/10 20:00	8.3	686	15.7	0.6	3.8	618	7.1	0.2	1.8	561	3.3	0.1	0.3	475	0.5	0.0	24.0	24	34.8	0.0
2/11/10 20:30	7.9	700	14.9	0.6	3.5	629	6.5	0.2	1.3	569	2.4	0.1	0.6	479	1.1	0.0	24.0	24	34.8	0.0
2/11/10 21:00	5.8	693	10.9	0.4	3.5	624	6.5	0.2	1.2	566	2.2	0.1	0.3	479	0.5	0.0	30.0	24	44.0	0.1
2/11/10 21:30	5.0	693	9.3	0.4	3.4	623	6.3	0.2	1.2	564	2.2	0.1	0.3	475	0.5	0.0	190.0	24	312.9	0.4
2/11/10 22:00	4.5	700	8.4	0.3	3.5	630	6.5	0.2	1.4	571	2.6	0.1	0.3	483	0.5	0.0	350.0	24	598.6	0.8
2/11/10 22:30	4.2	693	7.8	0.3	3.8	624	7.1	0.2	1.1	566	2.0	0.1	0.3	479	0.5	0.0	1000.0	24	1825.5	2.4
2/11/10 23:00	3.9	693	7.3	0.3	3.4	627	6.3	0.2	1.8	571	3.3	0.1	0.3	487	0.5	0.0	230.0	24	383.2	0.5
2/12/10 0:00	3.7	693	6.9	0.3	3.5	629	6.5	0.2	1.5	576	2.7	0.1	0.4	495	0.7	0.0	190.0	25	312.9	0.4
2/12/10 0:30	3.8	693	7.1	0.3	3.6	632	6.7	0.2	2.0	581	3.7	0.1	0.4	504	0.7	0.0	400.0	25	689.8	1.0
2/12/10 1:00	3.6	700	6.7	0.3	3.6	634	6.7	0.2	4.7	583	8.8	0.3	0.3	508	0.5	0.0	840.0	25	1516.9	2.2
2/12/10 1:30	3.8	700	7.1	0.3	5.9	642	11.1	0.4	11.3	594	21.5	0.7	0.2	521	0.4	0.0	560.0	26	986.1	1.4
2/12/10 2:00	3.6	700	6.7	0.3	4.6	645	8.6	0.3	15.7	599	30.0	1.0	0.3	530	0.5	0.0	610.0	26	1079.9	1.6
2/12/10 2:30	3.4	700	6.3	0.2	6.6	651	12.4	0.5	10.5	609	19.9	0.7	0.4	547	0.7	0.0	1000.0	27	1825.5	2.8
2/12/10 3:00	3.5	707	6.5	0.3	12.8	655	24.4	0.9	8.3	617	15.7	0.5	0.2	561	0.4	0.0	600.0	28	1061.1	1.7
2/12/10 3:30	3.7	707	6.9	0.3	14.8	664	28.3	1.1	15.3	628	29.2	1.0	0.3	575	0.5	0.0	140.0	28	226.2	0.4
2/12/10 4:00	3.9	714	7.3	0.3	10.8	682	20.5	0.8	19.8	639	38.0	1.4	0.2	593	0.4	0.0	79.0	29	123.2	0.2
2/12/10 4:30	4.8	720	9.0	0.4	15.5	690	29.6	1.1	18.9	656	36.3	1.3	0.3	617	0.5	0.0	280.0	30	472.3	0.8
2/12/10 5:00	3.3	741	6.1	0.3	19.6	709	37.7	1.5	22.0	665	42.4	1.6	0.3	626	0.5	0.0	450.0	31	781.7	1.4
2/12/10 5:30	4.1	755	7.6	0.3	19.8	723	38.0	1.5	23.4	682	45.1	1.7	0.4	641	0.7	0.0	180.0	31	295.4	0.5
2/12/10 6:00	3.7	755	6.9	0.3	21.8	728	42.0	1.7	12.3	696	23.4	0.9	0.3	656	0.5	0.0	240.0	32	401.0	0.7
2/12/10 6:30	4.2	770	7.8	0.3	19.9	744	38.2	1.6	7.4	723	13.9	0.6	0.6	691	1.1	0.0	180.0	33	295.4	0.5
2/12/10 7:00	6.4	791	12.0	0.5	14.3	757	27.3	1.2	10.1	729	19.1	0.8	0.4	686	0.7	0.0	160.0	34	260.7	0.5
																	110.0	33	175.1	0.3

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/12/10 7:30	10.0	799	19.0	0.9	9.4	767	17.8	0.8	8.2	741	15.5	0.6	0.4	702	0.7	0.0	150.0	34	243.4	0.5
2/12/10 8:00	12.0	828	22.8	1.1	12.1	789	23.0	1.0	7.3	756	13.7	0.6	1.1	707	2.0	0.1	82.0	34	128.2	0.2
2/12/10 8:30	12.0	836	22.8	1.1	11.9	794	22.6	1.0	5.8	759	10.9	0.5	0.5	707	0.9	0.0	75.0	34	116.6	0.2
2/12/10 9:00	12.0	851	22.8	1.1	10.2	808	19.3	0.9	4.7	772	8.8	0.4	0.4	717	0.7	0.0	53.0	35	80.6	0.2
2/12/10 9:30	15.0	851	28.7	1.4	8.8	805	16.6	0.8	4.3	765	8.0	0.3	0.4	707	0.7	0.0	43.0	34	64.6	0.1
2/12/10 10:00	17.0	890	32.6	1.6	10.2	837	19.3	0.9	4.2	794	7.8	0.3	0.5	728	0.9	0.0	81.0	35	126.5	0.3
2/12/10 10:30	18.0	890	34.5	1.7	8.7	832	16.4	0.8	3.3	784	6.1	0.3	0.4	712	0.7	0.0	48.0	35	72.6	0.1
2/12/10 11:00	17.0	897	32.6	1.6	7.3	841	13.7	0.6	2.7	794	5.0	0.2	0.8	722	1.4	0.1	39.0	35	58.2	0.1
2/12/10 11:30	12.0	913	22.8	1.2	6.6	852	12.4	0.6	2.3	800	4.2	0.2	0.3	722	0.5	0.0	36.0	35	53.5	0.1
2/12/10 12:00	9.6	913	18.2	0.9	5.7	850	10.7	0.5	4.6	797	8.6	0.4	0.3	717	0.5	0.0	41.0	35	61.4	0.1
2/12/10 12:30	9.1	913	17.2	0.9	5.7	853	10.7	0.5	3.1	803	5.7	0.3	0.6	728	1.1	0.0	80.0	35	124.8	0.2
2/12/10 13:00	9.5	913	18.0	0.9	4.5	852	8.4	0.4	2.0	800	3.7	0.2	0.4	722	0.7	0.0	620.0	35	1098.7	2.2
2/12/10 13:30	9.1	913	17.2	0.9	5.4	855	10.1	0.5	1.8	806	3.3	0.1	0.4	733	0.7	0.0	1000.0	36	1825.5	3.7
2/12/10 14:00	9.2	921	17.4	0.9	4.9	857	9.2	0.4	2.4	803	4.4	0.2	0.4	722	0.7	0.0	230.0	35	383.2	0.8
2/12/10 14:30	6.9	929	13.0	0.7	4.8	864	9.0	0.4	2.2	810	4.0	0.2	0.5	728	0.9	0.0	100.0	35	158.2	0.3
2/12/10 15:00	7.1	929	13.4	0.7	5.4	861	10.1	0.5	4.9	803	9.2	0.4	0.3	717	0.5	0.0	63.0	35	96.9	0.2
2/12/10 15:30	6.2	945	11.6	0.6	5.1	872	9.5	0.5	12.8	810	24.4	1.1	0.3	717	0.5	0.0	89.0	35	139.8	0.3
2/12/10 16:00	6.6	937	12.4	0.7	6.0	866	11.3	0.5	11.3	807	21.5	1.0	0.3	717	0.5	0.0	54.0	35	82.2	0.2
2/12/10 16:30	6.4	937	12.0	0.6	10.6	865	20.1	1.0	6.7	804	12.6	0.6	0.3	712	0.5	0.0	55.0	35	83.9	0.2
2/12/10 17:00	4.7	945	8.8	0.5	14.3	870	27.3	1.3	3.3	807	6.1	0.3	0.5	712	0.9	0.0	90.0	35	141.5	0.3
2/12/10 17:30	4.5	937	8.4	0.4	12.0	865	22.8	1.1	3.4	804	6.3	0.3	0.3	712	0.5	0.0	120.0	35	192.0	0.4
2/12/10 18:00	4.9	937	9.2	0.5	8.2	865	15.5	0.8	3.7	804	6.9	0.3	0.4	712	0.7	0.0	55.0	35	83.9	0.2
2/12/10 18:30	5.6	937	10.5	0.6	6.5	866	12.2	0.6	2.1	807	3.9	0.2	0.3	717	0.5	0.0	100.0	35	158.2	0.3
2/12/10 19:00	4.4	937	8.2	0.4	5.7	863	10.7	0.5	1.9	800	3.5	0.2	0.7	707	1.3	0.0	71.0	34	110.0	0.2
2/12/10 19:30	3.8	921	7.1	0.4	5.2	852	9.7	0.5	2.9	794	5.4	0.2	0.3	707	0.5	0.0	98.0	34	154.9	0.3
2/12/10 20:00	4.3	921	8.0	0.4	6.5	849	12.2	0.6	3.4	788	6.3	0.3	0.4	696	0.7	0.0	56.0	34	85.5	0.2
2/12/10 20:30	6.0	937	11.3	0.6	5.3	860	9.9	0.5	2.6	794	4.8	0.2	0.3	696	0.5	0.0	43.0	34	64.6	0.1
2/12/10 21:00	9.2	937	17.4	0.9	6.0	860	11.3	0.5	2.5	794	4.6	0.2	0.4	696	0.7	0.0	37.0	34	55.0	0.1
2/12/10 21:30	10.0	913	19.0	1.0	5.4	843	10.1	0.5	2.4	785	4.4	0.2	0.4	696	0.7	0.0	44.0	34	66.2	0.1
2/12/10 22:00	9.0	929	17.0	0.9	5.4	854	10.1	0.5	2.6	791	4.8	0.2	0.3	696	0.5	0.0	180.0	34	295.4	0.6
2/12/10 22:30	7.0	913	13.2	0.7	5.5	840	10.3	0.5	2.0	778	3.7	0.2	0.3	686	0.5	0.0	160.0	33	260.7	0.5
2/12/10 23:00	5.6	913	10.5	0.5	5.5	843	10.3	0.5	1.8	785	3.3	0.1	0.3	696	0.5	0.0	64.0	34	98.5	0.2
2/12/10 23:30	4.7	913	8.8	0.5	5.0	838	9.3	0.4	1.6	775	2.9	0.1	0.3	681	0.5	0.0	59.0	33	90.3	0.2
2/13/10 0:00	4.2	913	7.8	0.4	5.5	840	10.3	0.5	1.9	778	3.5	0.2	0.4	686	0.7	0.0	120.0	33	192.0	0.4
2/13/10 0:30	3.8	913	7.1	0.4	4.6	837	8.6	0.4	4.6	772	8.6	0.4	0.3	676	0.5	0.0	61.0	33	93.6	0.2
2/13/10 1:00	4.4	905	8.2	0.4	4.8	831	9.0	0.4	4.0	769	7.4	0.3	0.3	676	0.5	0.0	50.0	33	75.8	0.1
2/13/10 1:30	4.5	905	8.4	0.4	5.5	830	10.3	0.5	2.5	766	4.6	0.2	0.3	671	0.5	0.0	34.0	33	50.3	0.1
2/13/10 2:00	4.5	905	8.4	0.4	7.7	830	14.5	0.7	2.7	766	5.0	0.2	0.3	671	0.5	0.0	43.0	33	64.6	0.1
2/13/10 2:30	4.3	905	8.0	0.4	6.6	827	12.4	0.6	2.5	760	4.6	0.2	0.4	661	0.7	0.0	41.0	32	61.4	0.1
2/13/10 3:00	4.5	897	8.4	0.4	5.7	821	10.7	0.5	2.2	757	4.0	0.2	0.4	661	0.7	0.0	33.0	32	48.7	0.1
2/13/10 3:30	4.6	890	8.6	0.4	5.7	814	10.7	0.5	1.9	751	3.5	0.1	0.3	656	0.5	0.0	29.0	32	42.5	0.1
2/13/10 4:00	4.0	882	7.4	0.4	5.5	807	10.3	0.5	1.5	745	2.7	0.1	0.5	651	0.9	0.0	25.0	32	36.3	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/13/10 4:30	4.2	882	7.8	0.4	9.3	806	17.6	0.8	1.7	742	3.1	0.1	0.3	646	0.5	0.0	24.0	32	34.8	0.1
2/13/10 5:00	3.6	882	6.7	0.3	5.4	807	10.1	0.5	1.8	745	3.3	0.1	0.5	651	0.9	0.0	24.0	32	34.8	0.1
2/13/10 5:30	3.7	874	6.9	0.3	4.3	802	8.0	0.4	1.4	742	2.6	0.1	0.4	651	0.7	0.0	20.0	32	28.6	0.1
2/13/10 6:00	4.6	882	8.6	0.4	4.0	804	7.4	0.3	1.4	739	2.6	0.1	0.3	641	0.5	0.0	24.0	31	34.8	0.1
2/13/10 6:30	5.2	874	9.7	0.5	4.0	801	7.4	0.3	1.0	739	1.8	0.1	0.3	646	0.5	0.0	70.0	32	108.3	0.2
2/13/10 7:00	5.0	866	9.3	0.5	3.8	792	7.1	0.3	1.0	730	1.8	0.1	0.3	636	0.5	0.0	64.0	31	98.5	0.2
2/13/10 7:30	4.3	874	8.0	0.4	4.0	799	7.4	0.3	1.0	736	1.8	0.1	0.4	641	0.7	0.0	85.0	31	133.1	0.2
2/13/10 8:00	4.2	866	7.8	0.4	3.9	792	7.3	0.3	0.9	730	1.6	0.1	0.3	636	0.5	0.0	75.0	31	116.6	0.2
2/13/10 8:30	3.9	866	7.3	0.4	3.7	791	6.9	0.3	1.1	727	2.0	0.1	0.4	631	0.7	0.0	100.0	31	158.2	0.3
2/13/10 9:00	4.2	851	7.8	0.4	4.0	780	7.4	0.3	1.8	721	3.3	0.1	0.4	631	0.7	0.0	210.0	31	347.9	0.6
2/13/10 9:30	3.7	859	6.9	0.3	3.7	782	6.9	0.3	2.4	718	4.4	0.2	0.4	622	0.7	0.0	170.0	31	278.0	0.5
2/13/10 10:00	3.4	851	6.3	0.3	3.8	779	7.1	0.3	2.2	718	4.0	0.2	0.3	626	0.5	0.0	77.0	31	119.9	0.2
2/13/10 10:30	5.5	851	10.3	0.5	3.4	777	6.2	0.3	2.0	715	3.7	0.1	0.3	622	0.5	0.0	72.0	31	111.6	0.2
2/13/10 11:00	3.4	859	6.3	0.3	2.9	781	5.4	0.2	2.7	715	5.0	0.2	0.3	617	0.5	0.0	52.0	30	79.0	0.1
2/13/10 11:30	4.1	843	7.6	0.4	1.9	770	3.5	0.2	4.4	709	8.2	0.3	0.3	617	0.5	0.0	44.0	30	66.2	0.1
2/13/10 12:00	3.5	843	6.5	0.3	2.6	767	4.8	0.2	4.1	703	7.6	0.3	0.3	607	0.5	0.0	33.0	30	48.7	0.1
2/13/10 12:30	3.2	843	5.9	0.3	2.6	769	4.8	0.2	3.2	706	6.0	0.2	0.3	612	0.5	0.0	30.0	30	44.0	0.1
2/13/10 13:00	3.2	836	5.9	0.3	3.7	761	6.9	0.3	2.4	697	4.4	0.2	0.3	602	0.5	0.0	120.0	30	192.0	0.3
2/13/10 13:30	2.8	836	5.2	0.2	3.2	764	5.9	0.3	1.5	703	2.7	0.1	0.3	612	0.5	0.0	140.0	30	226.2	0.4
2/13/10 14:00	3.6	836	6.7	0.3	2.7	758	5.0	0.2	2.0	692	3.7	0.1	0.4	593	0.7	0.0	100.7	29	159.3	0.3
2/13/10 14:30	3.2	821	5.9	0.3	2.2	749	4.0	0.2	1.4	689	2.6	0.1	0.3	598	0.5	0.0	51.0	29	77.4	0.1
2/13/10 15:00	3.2	821	5.9	0.3	1.4	751	2.6	0.1	1.6	691	2.9	0.1	0.3	602	0.5	0.0	42.0	30	63.0	0.1
2/13/10 15:30	3.6	828	6.7	0.3	1.3	753	2.4	0.1	2.6	689	4.8	0.2	0.3	593	0.5	0.0	37.0	29	55.0	0.1
2/13/10 16:00	3.7	828	6.9	0.3	0.8	753	1.4	0.1	4.2	689	7.8	0.3	0.2	593	0.4	0.0	35.0	29	51.9	0.1
2/13/10 16:30	3.9	821	7.3	0.3	1.3	744	2.4	0.1	4.0	680	7.4	0.3	0.3	584	0.5	0.0	42.0	29	63.0	0.1
2/13/10 17:00	4.9	813	9.2	0.4	2.1	741	3.9	0.2	2.7	680	5.0	0.2	0.4	588	0.7	0.0	44.0	29	66.2	0.1
2/13/10 17:30	5.1	806	9.5	0.4	3.2	733	5.9	0.2	1.6	671	2.9	0.1	0.5	579	0.9	0.0	33.0	29	48.7	0.1
2/13/10 18:00	5.6	806	10.5	0.5	3.5	733	6.5	0.3	1.3	671	2.4	0.1	0.3	579	0.5	0.0	28.0	29	40.9	0.1
2/13/10 18:30	4.8	806	9.0	0.4	2.4	731	4.4	0.2	1.4	669	2.6	0.1	0.6	575	1.1	0.0	27.0	28	39.4	0.1
2/13/10 19:00	4.2	799	7.8	0.4	1.6	724	2.9	0.1	1.0	660	1.8	0.1	0.3	565	0.5	0.0	27.0	28	39.4	0.1
2/13/10 19:30	3.9	791	7.3	0.3	1.3	723	2.4	0.1	1.3	665	2.4	0.1	0.4	579	0.7	0.0	28.0	29	40.9	0.1
2/13/10 20:00	3.7	791	6.9	0.3	1.0	719	1.8	0.1	1.2	657	2.2	0.1	0.3	565	0.5	0.0	23.0	28	33.2	0.1
2/13/10 20:30	3.2	784	5.9	0.3	1.2	714	2.2	0.1	0.8	654	1.4	0.1	0.4	565	0.7	0.0	28.0	28	40.9	0.1
2/13/10 21:00	3.3	784	6.1	0.3	0.7	714	1.3	0.1	1.1	654	2.0	0.1	0.3	565	0.5	0.0	25.0	28	36.3	0.1
2/13/10 21:30	4.0	791	7.4	0.3	1.3	717	2.4	0.1	0.7	655	1.3	0.0	0.3	561	0.5	0.0	24.0	28	34.8	0.1
2/13/10 22:00	4.1	762	7.6	0.3	1.0	696	1.8	0.1	0.7	640	1.3	0.0	0.3	556	0.5	0.0	20.0	27	28.6	0.0
2/13/10 22:30	4.6	777	8.6	0.4	0.5	706	0.9	0.0	0.8	646	1.4	0.1	0.3	556	0.5	0.0	22.0	27	31.7	0.0
2/13/10 23:00	5.1	777	9.5	0.4	0.7	704	1.3	0.0	0.6	643	1.1	0.0	0.3	552	0.5	0.0	21.0	27	30.2	0.0
2/13/10 23:30	4.1	770	7.6	0.3	1.0	700	1.8	0.1	0.9	640	1.6	0.1	0.3	552	0.5	0.0	24.0	27	34.8	0.1
2/14/10 0:00	3.5	762	6.5	0.3	0.9	693	1.6	0.1	1.3	635	2.4	0.1	0.3	547	0.5	0.0	22.0	27	31.7	0.0
2/14/10 0:30	3.8	762	7.1	0.3	0.7	693	1.3	0.0	0.7	635	1.3	0.0	0.2	547	0.4	0.0	18.0	27	25.6	0.0
2/14/10 1:00	3.1	762	5.7	0.2	0.8	692	1.4	0.1	0.7	632	1.3	0.0	0.3	543	0.5	0.0	17.0	27	24.1	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/14/10 1:30	3.1	755	5.7	0.2	0.7	686	1.3	0.0	0.9	627	1.6	0.1	0.3	539	0.5	0.0	16.0	27	22.6	0.0
2/14/10 2:00	3.5	762	6.5	0.3	0.8	690	1.4	0.1	0.6	630	1.1	0.0	0.3	539	0.5	0.0	17.0	27	24.1	0.0
2/14/10 2:30	3.5	755	6.5	0.3	0.5	683	0.9	0.0	1.0	622	1.8	0.1	0.3	530	0.5	0.0	16.0	26	22.6	0.0
2/14/10 3:00	3.1	755	5.7	0.2	1.0	684	1.8	0.1	0.9	624	1.6	0.1	0.4	534	0.7	0.0	17.0	26	24.1	0.0
2/14/10 3:30	3.6	755	6.7	0.3	0.8	684	1.4	0.1	0.7	624	1.3	0.0	0.3	534	0.5	0.0	20.0	26	28.6	0.0
2/14/10 4:00	3.2	748	5.9	0.2	0.4	679	0.7	0.0	0.7	621	1.3	0.0	0.4	534	0.7	0.0	24.0	26	34.8	0.1
2/14/10 4:30	3.9	762	7.3	0.3	1.3	690	2.4	0.1	1.4	630	2.6	0.1	0.3	539	0.5	0.0	200.0	27	330.4	0.5
2/14/10 5:00	3.2	762	5.9	0.3	0.7	690	1.3	0.0	0.6	630	1.1	0.0	0.4	539	0.7	0.0	250.0	27	418.7	0.6
2/14/10 5:30	3.7	755	6.9	0.3	0.7	687	1.3	0.0	0.8	629	1.4	0.1	0.4	543	0.7	0.0	81.0	27	126.5	0.2
2/14/10 6:00	3.1	762	5.7	0.2	0.8	695	1.4	0.1	2.6	638	4.8	0.2	0.4	552	0.7	0.0	350.0	27	598.6	0.9
2/14/10 6:30	2.9	755	5.4	0.2	0.5	693	0.9	0.0	0.7	640	1.3	0.0	1.4	561	2.6	0.1	430.0	28	744.9	1.2
2/14/10 7:00	3.6	748	6.7	0.3	0.7	685	1.3	0.0	2.5	632	4.6	0.2	0.3	552	0.5	0.0	320.0	27	544.2	0.8
2/14/10 7:30	3.3	755	6.1	0.3	0.8	694	1.4	0.1	5.3	643	9.9	0.4	0.3	565	0.5	0.0	400.0	28	689.8	1.1
2/14/10 8:00	3.1	755	5.7	0.2	0.9	693	1.6	0.1	4.9	640	9.2	0.3	0.3	565	0.5	0.0	390.0	28	671.5	1.0
2/14/10 8:30	3.1	762	5.7	0.2	1.5	699	2.7	0.1	6.6	646	12.4	0.5	0.4	565	0.7	0.0	160.0	28	260.7	0.4
2/14/10 9:00	3.2	762	5.9	0.3	3.5	700	6.5	0.3	11.5	648	21.9	0.8	0.4	570	0.7	0.0	96.0	28	151.5	0.2
2/14/10 9:30	3.1	762	5.7	0.2	3.8	700	7.1	0.3	10.1	648	19.1	0.7	0.4	570	0.7	0.0	100.0	28	158.2	0.3
2/14/10 10:00	3.3	770	6.1	0.3	5.2	708	9.7	0.4	10.6	657	20.1	0.7	0.4	579	0.7	0.0	210.0	29	347.9	0.6
2/14/10 10:30	3.3	770	6.1	0.3	8.1	705	15.3	0.6	10.3	651	19.5	0.7	0.4	570	0.7	0.0	190.0	28	312.9	0.5
2/14/10 11:00	3.4	770	6.3	0.3	8.0	707	15.1	0.6	8.1	654	15.3	0.6	0.3	575	0.5	0.0	110.0	28	175.1	0.3
2/14/10 11:30	2.7	784	5.0	0.2	7.7	718	14.5	0.6	4.7	663	8.8	0.3	0.6	579	1.1	0.0	64.0	29	98.5	0.2
2/14/10 12:00	3.1	784	5.7	0.3	8.4	718	15.9	0.6	3.6	663	6.7	0.2	0.4	579	0.7	0.0	180.0	29	295.4	0.5
2/14/10 12:30	3.1	799	5.7	0.3	7.0	731	13.2	0.5	4.5	674	8.4	0.3	0.4	588	0.7	0.0	94.0	29	148.2	0.2
2/14/10 13:00	3.2	791	5.9	0.3	4.3	729	8.0	0.3	5.6	677	10.5	0.4	0.3	598	0.5	0.0	200.0	29	330.4	0.5
2/14/10 13:30	4.7	806	8.8	0.4	3.2	740	5.9	0.2	4.9	685	9.2	0.4	0.3	602	0.5	0.0	310.0	30	526.2	0.9
2/14/10 14:00	5.6	799	10.5	0.5	4.0	739	7.4	0.3	3.3	688	6.1	0.2	0.3	612	0.5	0.0	460.0	30	800.2	1.4
2/14/10 14:30	6.0	806	11.3	0.5	4.6	744	8.6	0.4	4.5	691	8.4	0.3	0.3	612	0.5	0.0	550.0	30	967.4	1.6
2/14/10 15:00	7.2	813	13.6	0.6	4.1	752	7.6	0.3	3.6	700	6.7	0.3	0.4	622	0.7	0.0	400.0	31	689.8	1.2
2/14/10 15:30	8.4	813	15.9	0.7	2.9	755	5.4	0.2	5.3	705	9.9	0.4	0.3	631	0.5	0.0	340.0	31	580.4	1.0
2/14/10 16:00	9.3	813	17.6	0.8	3.6	756	6.7	0.3	9.5	708	18.0	0.7	0.3	636	0.5	0.0	190.0	31	312.9	0.5
2/14/10 16:30	9.3	821	17.6	0.8	4.3	763	8.0	0.3	12.9	714	24.6	1.0	0.3	641	0.5	0.0	120.0	31	192.0	0.3
2/14/10 17:00	8.3	821	15.7	0.7	5.3	765	9.9	0.4	14.7	717	28.1	1.1	0.4	646	0.7	0.0	100.0	32	158.2	0.3
2/14/10 17:30	7.8	828	14.7	0.7	7.6	771	14.3	0.6	12.8	723	24.4	1.0	0.3	651	0.5	0.0	98.0	32	154.9	0.3
2/14/10 18:00	6.0	843	11.3	0.5	10.5	785	19.9	0.9	10.3	735	19.5	0.8	0.3	661	0.5	0.0	62.0	32	95.2	0.2
2/14/10 18:30	5.9	843	11.1	0.5	10.6	786	20.1	0.9	7.5	738	14.1	0.6	0.3	666	0.5	0.0	65.0	33	100.1	0.2
2/14/10 19:00	6.1	851	11.4	0.5	10.6	793	20.1	0.9	5.1	744	9.5	0.4	0.4	671	0.7	0.0	57.0	33	87.1	0.2
2/14/10 19:30	6.0	866	11.3	0.5	8.0	805	15.1	0.7	3.3	753	6.1	0.3	0.3	676	0.5	0.0	52.0	33	79.0	0.1
2/14/10 20:00	5.4	874	10.1	0.5	5.8	812	10.9	0.5	3.8	759	7.1	0.3	0.7	681	1.3	0.0	42.0	33	63.0	0.1
2/14/10 20:30	5.7	874	10.3	0.5	4.1	815	7.6	0.3	2.6	766	4.8	0.2	0.3	691	0.5	0.0	38.0	34	56.6	0.1
2/14/10 21:00	5.7	874	10.7	0.5	3.6	812	6.7	0.3	2.3	759	4.2	0.2	0.3	681	0.5	0.0	55.0	33	83.9	0.2
2/14/10 21:30	6.1	882	11.4	0.6	3.0	815	5.6	0.3	2.2	760	4.0	0.2	0.5	676	0.9	0.0	38.0	33	56.6	0.1
2/14/10 22:00	7.9	882	14.9	0.7	2.4	815	4.4	0.2	2.0	760	3.7	0.2	0.4	676	0.7	0.0	34.0	33	50.3	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/14/10 22:30	9.9	890	18.8	0.9	2.6	822	4.8	0.2	1.9	766	3.5	0.1	0.5	681	0.9	0.0	38.0	33	56.6	0.1
2/14/10 23:00	11.0	897	20.9	1.1	2.1	828	3.9	0.2	1.7	769	3.1	0.1	0.3	681	0.5	0.0	35.0	33	51.9	0.1
2/14/10 23:30	10.0	897	19.0	1.0	1.7	826	3.1	0.1	2.2	766	4.0	0.2	0.3	676	0.5	0.0	36.0	33	53.5	0.1
2/15/10 0:00	9.3	890	17.6	0.9	1.7	821	3.1	0.1	1.5	763	2.7	0.1	0.5	676	0.9	0.0	34.0	33	50.3	0.1
2/15/10 0:30	8.9	897	16.8	0.8	1.6	824	2.9	0.1	1.7	763	3.1	0.1	0.3	671	0.5	0.0	36.0	33	53.5	0.1
2/15/10 1:00	6.9	897	13.0	0.7	1.6	823	2.9	0.1	2.5	760	4.6	0.2	0.3	666	0.5	0.0	33.0	33	48.7	0.1
2/15/10 1:30	5.6	897	10.5	0.5	1.6	823	2.9	0.1	2.6	760	4.7	0.2	0.3	666	0.5	0.0	29.0	33	42.5	0.1
2/15/10 2:00	5.4	897	10.1	0.5	1.4	823	2.6	0.1	2.6	760	4.9	0.2	0.3	666	0.5	0.0	30.0	33	44.0	0.1
2/15/10 2:30	4.5	890	8.4	0.4	1.7	816	3.1	0.1	2.7	754	5.0	0.2	0.4	661	0.7	0.0	27.0	32	39.4	0.1
2/15/10 3:00	4.3	897	8.0	0.4	3.4	818	6.3	0.3	2.8	751	5.1	0.2	0.3	651	0.5	0.0	29.0	32	42.5	0.1
2/15/10 3:30	4.2	897	7.8	0.4	1.5	818	2.7	0.1	2.8	751	5.2	0.2	0.5	651	0.9	0.0	25.0	32	36.3	0.1
2/15/10 4:00	4.8	890	9.0	0.4	1.5	814	2.7	0.1	2.9	751	5.4	0.2	0.3	656	0.5	0.0	25.0	32	36.3	0.1
2/15/10 4:30	3.8	890	7.1	0.4	3.2	811	5.9	0.3	3.0	745	5.5	0.2	0.3	646	0.5	0.0	26.0	32	37.8	0.1
2/15/10 5:00	3.6	890	6.7	0.3	1.2	811	2.2	0.1	3.0	745	5.6	0.2	0.4	646	0.7	0.0	29.0	32	42.5	0.1
2/15/10 5:30	4.0	882	7.4	0.4	1.5	804	2.7	0.1	3.1	739	5.7	0.2	0.3	641	0.5	0.0	23.0	31	33.2	0.1
2/15/10 6:00	3.8	874	7.1	0.3	1.0	799	1.8	0.1	3.2	736	5.9	0.2	0.3	641	0.5	0.0	28.0	31	40.9	0.1
2/15/10 6:30	3.5	882	6.5	0.3	1.0	801	1.8	0.1	3.2	733	6.0	0.2	0.3	631	0.5	0.0	86.0	31	134.8	0.2
2/15/10 7:00	3.6	882	6.7	0.3	1.0	801	1.8	0.1	3.3	733	6.1	0.3	0.3	631	0.5	0.0	38.0	31	56.6	0.1
2/15/10 7:30	3.6	874	6.7	0.3	1.0	796	1.8	0.1	3.4	730	6.2	0.3	0.3	631	0.5	0.0	35.0	31	51.9	0.1
2/15/10 8:00	3.3	866	6.1	0.3	1.1	791	2.0	0.1	3.4	727	6.4	0.3	1.7	631	3.1	0.1	35.0	31	51.9	0.1
2/15/10 8:30	3.4	874	6.3	0.3	0.8	793	1.4	0.1	3.5	724	6.5	0.3	0.3	622	0.5	0.0	31.0	31	45.6	0.1
2/15/10 9:00	3.5	859	5.7	0.3	1.2	782	2.2	0.1	3.6	718	6.6	0.3	0.3	622	0.5	0.0	26.0	31	37.8	0.1
2/15/10 9:30	3.1	859	5.7	0.3	1.3	781	2.4	0.1	3.6	715	6.7	0.3	0.2	617	0.4	0.0	210.0	30	347.9	0.6
2/15/10 10:00	3.7	851	6.9	0.3	1.2	774	2.2	0.1	3.7	709	6.9	0.3	0.3	612	0.5	0.0	150.0	30	243.4	0.4
2/15/10 10:30	3.4	851	6.3	0.3	1.6	774	2.9	0.1	3.8	709	7.0	0.3	0.3	612	0.5	0.0	48.0	30	72.6	0.1
2/15/10 11:00	3.2	851	5.9	0.3	1.9	772	3.5	0.2	3.8	706	7.1	0.3	0.3	607	0.5	0.0	34.0	30	50.3	0.1
2/15/10 11:30	3.4	851	6.3	0.3	1.4	771	2.6	0.1	3.9	704	7.2	0.3	0.3	602	0.5	0.0	29.0	30	42.5	0.1
2/15/10 12:00	3.5	851	6.5	0.3	1.3	771	2.4	0.1	4.0	704	7.4	0.3	0.4	602	0.7	0.0	25.0	30	36.3	0.1
2/15/10 12:30	3.2	843	5.9	0.3	1.4	766	2.6	0.1	4.0	700	7.5	0.3	0.3	602	0.5	0.0	29.0	30	42.5	0.1
2/15/10 13:00	3.5	836	6.5	0.3	1.3	758	2.4	0.1	4.1	692	7.6	0.3	0.3	593	0.5	0.0	22.0	29	31.7	0.1
2/15/10 13:30	3.1	843	5.7	0.3	2.8	763	5.2	0.2	4.2	695	7.7	0.3	0.3	593	0.5	0.0	22.0	29	31.7	0.1
2/15/10 14:00	3.3	828	6.1	0.3	4.0	751	7.4	0.3	4.2	686	7.9	0.3	0.5	588	0.9	0.0	21.0	29	30.2	0.0
2/15/10 14:30	3.3	828	6.1	0.3	2.2	750	4.0	0.2	4.3	683	8.0	0.3	0.5	584	0.9	0.0	20.0	29	28.6	0.0
2/15/10 15:00	3.3	821	6.1	0.3	1.6	744	2.9	0.1	4.4	680	8.1	0.3	0.4	584	0.7	0.0	62.0	29	95.2	0.2
2/15/10 15:30	3.7	813	6.9	0.3	1.5	738	2.7	0.1	4.4	674	8.2	0.3	0.4	579	0.7	0.0	38.0	29	56.6	0.1
2/15/10 16:00	3.5	813	6.5	0.3	1.3	736	2.4	0.1	4.5	672	8.4	0.3	0.3	575	0.5	0.0	25.0	28	36.3	0.1
2/15/10 16:30	3.7	813	6.9	0.3	1.6	735	2.9	0.1	4.6	669	8.5	0.3	0.3	570	0.5	0.0	25.0	28	36.3	0.1
2/15/10 17:00	3.5	813	6.5	0.3	1.7	734	3.1	0.1	4.6	666	8.6	0.3	0.5	565	0.9	0.0	21.0	28	30.2	0.0
2/15/10 17:30	3.2	813	5.9	0.3	1.9	735	3.5	0.1	4.7	669	8.7	0.3	0.3	570	0.5	0.0	22.0	28	31.7	0.1
2/15/10 18:00	4.2	799	7.8	0.4	1.1	724	2.0	0.1	4.7	660	8.9	0.3	0.3	565	0.5	0.0	20.0	28	28.6	0.0
2/15/10 18:30	4.7	791	8.8	0.4	1.3	720	2.4	0.1	4.8	660	9.0	0.3	0.4	570	0.7	0.0	18.0	28	25.6	0.0
2/15/10 19:00	4.9	799	9.2	0.4	1.5	721	2.7	0.1	4.9	655	9.1	0.3	0.3	556	0.5	0.0	19.0	27	27.1	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/15/10 19:30	3.9	791	7.3	0.3	1.6	717	2.9	0.1	4.9	655	9.2	0.3	0.4	561	0.7	0.0	18.0	28	25.6	0.0
2/15/10 20:00	4.0	799	7.4	0.3	1.9	719	3.5	0.1	5.0	652	9.4	0.3	0.3	552	0.5	0.0	19.0	27	27.1	0.0
2/15/10 20:30	3.7	791	6.9	0.3	1.4	714	2.6	0.1	5.1	649	9.5	0.3	0.3	552	0.5	0.0	19.0	27	27.1	0.0
2/15/10 21:00	3.7	791	6.9	0.3	1.5	716	2.7	0.1	5.1	652	9.6	0.4	0.3	556	0.5	0.0	21.0	27	30.2	0.0
2/15/10 21:30	3.5	799	6.5	0.3	1.5	719	2.7	0.1	5.2	652	9.8	0.4	0.3	552	0.5	0.0	24.0	27	34.8	0.1
2/15/10 22:00	3.5	791	6.5	0.3	1.4	714	2.6	0.1	5.3	649	9.9	0.4	0.3	552	0.5	0.0	120.0	27	192.0	0.3
2/15/10 22:30	3.5	799	6.5	0.3	1.9	719	3.5	0.1	5.3	652	10.0	0.4	0.4	552	0.7	0.0	110.0	27	175.1	0.3
2/15/10 23:00	3.5	799	6.5	0.3	1.6	721	2.9	0.1	5.4	655	10.1	0.4	0.5	556	0.9	0.0	120.0	27	192.0	0.3
2/15/10 23:30	3.5	806	6.5	0.3	1.4	727	2.6	0.1	5.5	661	10.3	0.4	0.4	561	0.7	0.0	560.0	28	986.1	1.5
2/16/10 0:00	3.6	799	6.7	0.3	2.0	722	3.7	0.1	5.5	658	10.4	0.4	0.4	561	0.7	0.0	700.0	28	1249.8	1.9
2/16/10 0:30	3.9	799	7.3	0.3	1.6	722	2.9	0.1	5.6	658	10.5	0.4	0.4	561	0.7	0.0	380.0	28	653.2	1.0
2/16/10 1:00	4.0	813	7.4	0.3	1.9	732	3.5	0.1	5.7	664	10.6	0.4	0.5	561	0.9	0.0	410.0	28	708.1	1.1
2/16/10 1:30	3.6	813	6.7	0.3	1.8	734	3.3	0.1	5.7	666	10.8	0.4	0.3	565	0.5	0.0	290.0	28	490.2	0.8
2/16/10 2:00	3.6	813	6.7	0.3	2.5	734	4.6	0.2	5.8	666	10.9	0.4	0.3	565	0.5	0.0	120.0	28	192.0	0.3
2/16/10 2:30	3.8	806	7.1	0.3	3.3	729	6.1	0.3	5.9	663	11.0	0.4	0.3	565	0.5	0.0	93.0	28	146.5	0.2
2/16/10 3:00	4.0	813	7.4	0.3	5.0	732	9.3	0.4	5.9	664	11.1	0.4	0.3	561	0.5	0.0	60.0	28	92.0	0.1
2/16/10 3:30	3.6	806	6.7	0.3	8.3	730	15.7	0.6	6.0	666	11.3	0.4	0.3	570	0.5	0.0	380.0	28	653.2	1.0
2/16/10 4:00	4.0	813	7.4	0.3	12.9	732	24.6	1.0	6.1	664	11.4	0.4	0.4	561	0.7	0.0	330.0	28	562.3	0.9
2/16/10 4:30	3.9	813	7.3	0.3	13.1	732	25.0	1.0	6.1	664	11.5	0.4	0.4	561	0.7	0.0	150.0	28	243.4	0.4
2/16/10 5:00	3.6	813	6.7	0.3	10.4	732	19.7	0.8	6.2	664	11.7	0.4	0.3	561	0.5	0.0	95.0	28	149.8	0.2
2/16/10 5:30	3.5	813	6.5	0.3	9.1	731	17.2	0.7	6.3	661	11.8	0.4	0.3	556	0.5	0.0	52.0	27	79.0	0.1
2/16/10 6:00	4.6	821	8.6	0.4	4.1	739	7.6	0.3	6.5	669	12.2	0.5	0.3	556	0.5	0.0	100.0	27	158.2	0.2
2/16/10 6:30	4.1	821	7.6	0.4	4.2	737	7.8	0.3	6.4	667	12.0	0.5	0.3	561	0.5	0.0	94.0	28	148.2	0.2
2/16/10 7:00	5.4	813	10.1	0.5	7.7	734	14.5	0.6	6.5	666	12.3	0.5	0.4	565	0.7	0.0	490.0	28	855.7	1.3
2/16/10 7:30	6.8	813	12.8	0.6	10.5	734	19.9	0.8	6.6	666	12.4	0.5	0.3	565	0.5	0.0	83.0	28	129.8	0.2
2/16/10 8:00	10.0	813	19.0	0.9	8.0	732	15.1	0.6	6.7	664	12.5	0.5	0.4	561	0.7	0.0	240.0	28	401.0	0.6
2/16/10 8:30	12.0	806	22.8	1.0	5.5	730	10.3	0.4	6.7	666	12.7	0.5	0.6	570	1.1	0.0	270.0	28	454.4	0.7
2/16/10 9:00	11.0	821	20.9	1.0	3.7	740	6.9	0.3	6.8	672	12.8	0.5	0.3	570	0.5	0.0	680.0	28	1211.9	1.9
2/16/10 9:30	11.0	806	20.9	0.9	3.5	731	6.5	0.3	6.9	669	12.9	0.5	0.3	575	0.5	0.0	620.0	28	1098.7	1.7
2/16/10 10:00	8.9	813	16.8	0.8	4.0	738	7.4	0.3	6.9	674	13.0	0.5	0.3	579	0.5	0.0	190.0	28	312.9	0.5
2/16/10 10:30	6.9	821	13.0	0.6	6.5	743	12.2	0.5	7.0	677	13.2	0.5	0.3	579	0.5	0.0	150.0	29	243.4	0.4
2/16/10 11:00	6.2	813	11.6	0.5	6.3	739	11.8	0.5	13.3	677	13.2	0.5	0.3	584	0.7	0.0	83.0	29	129.8	0.2
2/16/10 11:30	6.2	813	12.6	0.6	5.4	736	10.1	0.4	17.7	672	33.9	1.3	0.7	575	1.3	0.0	66.0	29	101.8	0.2
2/16/10 12:00	8.8	828	16.6	0.8	6.6	750	12.4	0.5	11.6	683	22.1	0.8	0.3	584	0.5	0.0	52.0	28	79.0	0.1
2/16/10 12:30	10.0	813	19.0	0.9	10.6	738	20.1	0.8	6.3	674	11.8	0.4	0.3	579	0.5	0.0	59.0	29	90.3	0.1
2/16/10 13:00	7.8	821	14.7	0.7	13.1	742	25.0	1.0	4.2	675	7.8	0.3	0.3	579	0.5	0.0	80.0	29	124.8	0.2
2/16/10 13:30	6.2	836	11.6	0.5	10.2	753	19.3	0.8	7.8	675	7.8	0.3	0.3	575	0.5	0.0	40.0	28	59.8	0.1
2/16/10 14:00	5.3	821	9.9	0.5	7.1	743	13.4	0.6	2.9	684	5.4	0.2	0.3	579	0.5	0.0	39.0	29	58.2	0.1
2/16/10 14:30	6.2	828	11.6	0.5	5.0	747	9.3	0.4	2.2	677	4.0	0.2	0.3	579	0.5	0.0	36.0	29	53.5	0.1
2/16/10 15:00	5.8	821	10.9	0.5	3.7	743	6.9	0.3	2.5	678	4.6	0.2	0.3	575	0.5	0.0	66.0	28	101.8	0.2
2/16/10 15:30	7.0	828	13.2	0.6	3.5	750	6.5	0.3	2.5	677	4.6	0.2	0.3	579	0.5	0.0	67.0	29	103.4	0.2
2/16/10 16:00									1.9	683	3.5	0.1	0.4	584	0.7	0.0	39.0	29	58.2	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/16/10 16:30	6.5	828	12.2	0.6	3.4	748	6.3	0.3	1.5	680	2.7	0.1	0.3	579	0.5	0.0	46.0	29	69.4	0.1
2/16/10 17:00	6.8	828	12.8	0.6	3.2	748	5.9	0.2	1.3	680	2.4	0.1	0.3	579	0.5	0.0	49.0	29	74.2	0.1
2/16/10 17:30	8.4	821	15.9	0.7	2.9	743	5.4	0.2	2.1	677	3.9	0.1	0.3	579	0.5	0.0	40.0	29	59.8	0.1
2/16/10 18:00	11.0	821	20.9	1.0	2.6	740	4.8	0.2	2.2	672	4.0	0.2	0.4	570	0.7	0.0	32.0	28	47.2	0.1
2/16/10 18:30	12.0	821	22.8	1.1	2.3	740	4.2	0.2	2.2	672	4.0	0.2	0.5	570	0.9	0.0	34.0	28	50.3	0.1
2/16/10 19:00	8.3	821	15.7	0.7	3.0	742	5.6	0.2	2.8	675	5.2	0.2	0.3	575	0.5	0.0	50.0	28	75.8	0.1
2/16/10 19:30	6.7	813	12.6	0.6	3.2	735	5.9	0.2	1.7	669	3.1	0.1	0.3	570	0.5	0.0	46.0	28	69.4	0.1
2/16/10 20:00	6.5	821	12.2	0.6	3.4	739	6.3	0.3	1.4	669	2.6	0.1	0.3	565	0.5	0.0	58.0	28	88.7	0.1
2/16/10 20:30	4.8	821	9.0	0.4	2.9	740	5.4	0.2	2.0	672	3.7	0.1	0.3	570	0.5	0.0	28.0	28	40.9	0.1
2/16/10 21:00	4.6	821	8.6	0.4	2.8	740	5.2	0.2	1.2	672	2.2	0.1	0.5	570	0.9	0.0	26.0	28	37.8	0.1
2/16/10 21:30	4.4	813	8.2	0.4	2.7	734	5.0	0.2	1.4	666	2.6	0.1	0.3	565	0.5	0.0	38.0	28	56.6	0.1
2/16/10 22:00	4.7	821	8.8	0.4	2.9	739	5.4	0.2	1.7	669	3.1	0.1	0.3	565	0.5	0.0	46.0	28	69.4	0.1
2/16/10 22:30	4.3	806	8.0	0.4	2.4	729	4.4	0.2	2.1	663	3.9	0.1	0.3	565	0.5	0.0	56.0	28	85.5	0.1
2/16/10 23:00	3.7	806	6.9	0.3	2.6	727	4.8	0.2	1.2	661	2.2	0.1	0.3	561	0.5	0.0	38.0	28	56.6	0.1
2/16/10 23:30	3.6	813	6.7	0.3	2.6	732	4.8	0.2	1.0	664	1.8	0.1	0.3	561	0.5	0.0	27.0	28	39.4	0.1
2/17/10 0:00	3.6	806	6.7	0.3	2.9	727	5.4	0.2	1.1	661	2.0	0.1	0.5	561	0.9	0.0	38.0	28	56.6	0.1
2/17/10 0:30	3.8	813	7.1	0.3	2.4	731	4.4	0.2	1.5	661	2.7	0.1	0.3	556	0.5	0.0	85.0	27	133.1	0.2
2/17/10 1:00	3.9	806	7.3	0.3	2.1	726	3.9	0.2	1.7	658	3.1	0.1	0.4	556	0.7	0.0	37.0	27	55.0	0.1
2/17/10 1:30	3.9	806	7.3	0.3	2.4	724	4.4	0.2	1.7	655	3.1	0.1	0.3	552	0.5	0.0	32.0	27	47.2	0.1
2/17/10 2:00	3.9	799	7.3	0.3	2.6	719	4.8	0.2	1.2	652	2.2	0.1	0.3	552	0.5	0.0	44.0	27	66.2	0.1
2/17/10 2:30	3.6	799	6.7	0.3	2.7	718	5.0	0.2	1.2	650	2.2	0.1	0.4	547	0.7	0.0	50.0	27	75.8	0.1
2/17/10 3:00	4.0	799	7.4	0.3	2.4	716	4.4	0.2	1.7	647	3.1	0.1	0.3	543	0.5	0.0	36.0	27	53.5	0.1
2/17/10 3:30	3.7	791	6.9	0.3	2.5	711	4.6	0.2	1.7	644	3.1	0.1	0.3	543	0.5	0.0	31.0	27	45.6	0.1
2/17/10 4:00	3.7	799	6.9	0.3	2.3	716	4.2	0.2	1.5	647	2.7	0.1	0.3	543	0.5	0.0	36.0	27	53.5	0.1
2/17/10 4:30	3.9	791	7.3	0.3	2.6	710	4.8	0.2	1.3	641	2.4	0.1	0.4	539	0.7	0.0	35.0	27	51.9	0.1
2/17/10 5:00	3.5	791	6.5	0.3	2.7	710	5.0	0.2	2.5	641	4.6	0.2	0.3	539	0.5	0.0	27.0	27	39.4	0.1
2/17/10 5:30	3.4	777	6.3	0.3	3.0	700	5.6	0.2	3.5	635	6.5	0.2	0.3	539	0.5	0.0	23.0	27	33.2	0.0
2/17/10 6:00	3.4	784	6.3	0.3	2.4	702	4.4	0.2	2.5	633	4.6	0.2	0.6	530	1.1	0.0	35.0	26	51.9	0.1
2/17/10 6:30	3.6	777	6.7	0.3	2.6	699	4.8	0.2	1.2	633	2.2	0.1	0.3	534	0.5	0.0	49.0	26	74.2	0.1
2/17/10 7:00	3.4	777	6.3	0.3	2.5	697	4.6	0.2	1.1	630	2.0	0.1	0.3	530	0.5	0.0	33.0	26	48.7	0.1
2/17/10 7:30	3.9	777	7.3	0.3	3.7	697	6.9	0.3	1.3	630	2.4	0.1	0.3	530	0.5	0.0	25.0	26	36.3	0.1
2/17/10 8:00	3.7	777	6.9	0.3	2.3	697	4.2	0.2	0.9	630	1.6	0.1	0.4	530	0.7	0.0	26.0	26	37.8	0.1
2/17/10 8:30	3.9	770	7.3	0.3	2.3	691	4.2	0.2	1.1	625	2.0	0.1	0.2	525	0.4	0.0	27.0	26	39.4	0.1
2/17/10 9:00	5.3	770	9.9	0.4	2.5	690	4.6	0.2	1.5	622	2.7	0.1	0.3	521	0.5	0.0	28.0	26	40.9	0.1
2/17/10 9:30	3.7	770	6.9	0.3	2.3	690	4.2	0.2	1.5	622	2.7	0.1	0.6	521	1.1	0.0	39.0	26	58.2	0.1
2/17/10 10:00	3.8	770	7.1	0.3	2.0	690	3.7	0.1	1.4	622	2.6	0.1	0.3	521	0.5	0.0	27.0	26	39.4	0.1
2/17/10 10:30	3.5	770	6.5	0.3	2.4	688	4.4	0.2	1.7	620	3.1	0.1	0.3	517	0.5	0.0	28.0	26	40.9	0.1
2/17/10 11:00	3.5	755	6.5	0.3	2.6	679	4.8	0.2	1.1	614	2.0	0.1	0.4	517	0.7	0.0	51.0	26	77.4	0.1
2/17/10 11:30	3.5	755	6.5	0.3	2.4	677	4.4	0.2	1.0	611	1.8	0.1	0.3	512	0.5	0.0	34.0	25	50.3	0.1
2/17/10 12:00	3.8	762	7.1	0.3	2.0	682	3.7	0.1	1.2	614	2.2	0.1	0.3	512	0.5	0.0	28.0	25	40.9	0.1
2/17/10 12:30	3.4	755	6.3	0.3	2.2	674	4.0	0.2	1.4	606	2.6	0.1	0.8	504	1.4	0.0	26.0	25	37.8	0.1
2/17/10 13:00	3.3	755	6.1	0.3	2.3	676	4.2	0.2	1.2	609	2.2	0.1	0.4	508	0.7	0.0	25.0	25	36.3	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/17/10 13:30	5.3	755	9.9	0.4	2.6	676	4.8	0.2	1.6	609	2.9	0.1	0.4	508	0.7	0.0	19.0	25	27.1	0.0
2/17/10 14:00	3.6	748	6.7	0.3	2.5	670	4.6	0.2	1.4	603	2.6	0.1	0.3	504	0.5	0.0	19.0	25	27.1	0.0
2/17/10 14:30	3.4	748	6.3	0.3	2.5	668	4.6	0.2	1.2	601	2.2	0.1	0.3	500	0.5	0.0	25.0	25	36.3	0.1
2/17/10 15:00	3.4	741	6.3	0.3	2.8	663	5.2	0.2	1.1	598	2.0	0.1	0.3	500	0.5	0.0	16.0	25	22.6	0.0
2/17/10 15:30	3.4	734	6.3	0.3	3.2	659	5.9	0.2	0.9	595	1.6	0.1	0.2	500	0.4	0.0	15.0	25	21.1	0.0
2/17/10 16:00	3.1	748	5.7	0.2	2.8	667	5.2	0.2	0.9	598	1.6	0.1	0.3	495	0.5	0.0	16.0	25	22.6	0.0
2/17/10 16:30	3.2	734	5.9	0.2	2.4	656	4.4	0.2	0.9	590	1.6	0.1	0.3	491	0.5	0.0	16.0	24	22.6	0.0
2/17/10 17:00	3.0	741	5.6	0.2	2.2	661	4.0	0.2	0.9	593	1.6	0.1	0.4	491	0.7	0.0	14.0	24	19.6	0.0
2/17/10 17:30	3.3	741	6.1	0.3	2.2	661	4.0	0.2	1.3	593	2.4	0.1	0.5	491	0.9	0.0	19.0	24	27.1	0.0
2/17/10 18:00	3.4	734	6.3	0.3	3.5	656	6.5	0.2	0.7	590	1.3	0.0	0.3	491	0.5	0.0	14.0	24	19.6	0.0
2/17/10 18:30	3.0	734	5.6	0.2	2.2	655	4.0	0.1	0.6	588	1.1	0.0	0.3	487	0.5	0.0	16.0	24	22.6	0.0
2/17/10 19:00	3.7	734	6.9	0.3	2.3	652	4.2	0.2	0.7	583	1.3	0.0	0.3	479	0.5	0.0	15.0	24	21.1	0.0
2/17/10 19:30	3.9	727	7.3	0.3	2.2	647	4.0	0.1	0.6	580	1.1	0.0	0.3	479	0.5	0.0	16.0	24	22.6	0.0
2/17/10 20:00	3.3	727	6.1	0.3	2.3	647	4.2	0.2	0.5	580	0.9	0.0	0.3	479	0.5	0.0	14.0	24	19.6	0.0
2/17/10 20:30	3.5	727	6.5	0.3	2.6	647	4.8	0.2	0.8	580	1.4	0.0	0.3	479	0.5	0.0	15.0	24	21.1	0.0
2/17/10 21:00	3.4	714	6.3	0.3	2.9	637	5.4	0.2	0.9	572	1.6	0.1	0.3	475	0.5	0.0	13.0	24	18.1	0.0
2/17/10 21:30	3.3	720	6.1	0.2	2.3	641	4.2	0.2	0.6	575	1.1	0.0	0.3	475	0.5	0.0	17.0	24	24.1	0.0
2/17/10 22:00	3.2	707	5.9	0.2	2.0	631	3.7	0.1	1.0	567	1.8	0.1	0.3	471	0.5	0.0	14.0	23	19.6	0.0
2/17/10 22:30	3.5	707	6.5	0.3	2.1	631	3.9	0.1	0.7	567	1.3	0.0	0.7	471	1.3	0.0	12.0	23	16.6	0.0
2/17/10 23:00	3.4	700	6.3	0.2	2.3	623	4.2	0.1	0.9	559	1.6	0.1	0.3	462	0.5	0.0	13.0	23	18.1	0.0
2/17/10 23:30	3.4	700	6.3	0.2	2.0	623	3.7	0.1	1.0	559	1.8	0.1	0.3	462	0.5	0.0	14.0	23	19.6	0.0
2/18/10 0:00	3.4	700	6.3	0.2	2.2	622	4.0	0.1	0.6	557	1.1	0.0	0.3	458	0.5	0.0	13.0	23	18.1	0.0
2/18/10 0:30	3.0	700	5.6	0.2	2.4	623	4.4	0.2	0.7	559	1.3	0.0	0.3	462	0.5	0.0	14.0	23	19.6	0.0
2/18/10 1:00	3.1	693	5.7	0.2	2.0	618	3.7	0.1	1.2	554	2.2	0.1	0.3	458	0.5	0.0	12.0	23	16.6	0.0
2/18/10 1:30	3.3	693	6.1	0.2	2.2	618	4.0	0.1	0.6	554	1.1	0.0	0.3	458	0.5	0.0	14.0	23	19.6	0.0
2/18/10 2:00	3.2	686	5.9	0.2	1.9	612	3.5	0.1	0.5	549	0.9	0.0	0.4	454	0.7	0.0	12.0	23	16.6	0.0
2/18/10 2:30	3.6	686	6.7	0.3	1.8	610	3.3	0.1	0.5	546	0.9	0.0	0.3	450	0.5	0.0	11.0	23	15.2	0.0
2/18/10 3:00	2.9	700	5.4	0.2	2.2	618	4.0	0.1	0.5	550	0.9	0.0	0.3	447	0.5	0.0	10.0	22	13.7	0.0
2/18/10 3:30	3.2	680	5.9	0.2	1.9	603	3.5	0.1	0.6	539	1.1	0.0	0.4	443	0.7	0.0	12.0	22	16.6	0.0
2/18/10 4:00	2.9	686	5.4	0.2	1.8	608	3.3	0.1	0.6	542	1.1	0.0	0.3	443	0.5	0.0	12.0	22	16.6	0.0
2/18/10 4:30	3.3	673	6.1	0.2	2.6	600	4.8	0.2	0.5	539	0.9	0.0	0.3	447	0.5	0.0	15.0	22	21.1	0.0
2/18/10 5:00	3.1	673	5.7	0.2	1.8	599	3.3	0.1	0.5	536	0.9	0.0	0.3	443	0.5	0.0	12.0	22	16.6	0.0
2/18/10 5:30	3.2	680	5.9	0.2	1.9	602	3.5	0.1	1.0	537	1.8	0.1	0.9	439	1.6	0.0	11.0	22	15.2	0.0
2/18/10 6:00	3.2	673	5.9	0.2	1.8	598	3.3	0.1	0.6	534	1.1	0.0	0.3	439	0.5	0.0	10.0	22	13.7	0.0
2/18/10 6:30	3.2	673	5.9	0.2	1.8	596	3.3	0.1	0.4	532	0.7	0.0	0.3	435	0.5	0.0	11.0	22	15.2	0.0
2/18/10 7:00	4.7	673	8.8	0.3	2.0	596	3.7	0.1	0.6	532	1.1	0.0	0.3	435	0.5	0.0	11.0	22	15.2	0.0
2/18/10 7:30	3.3	667	6.1	0.2	1.7	591	3.1	0.1	0.6	527	1.1	0.0	0.3	431	0.5	0.0	11.0	22	15.2	0.0
2/18/10 8:00	3.3	667	6.1	0.2	1.8	589	3.3	0.1	0.6	524	1.1	0.0	0.3	427	0.5	0.0	15.0	21	21.1	0.0
2/18/10 8:30	3.4	660	6.3	0.2	1.9	585	3.5	0.1	0.5	522	0.9	0.0	0.3	427	0.5	0.0	15.0	21	21.1	0.0
2/18/10 9:00	3.1	660	5.7	0.2	1.9	586	3.5	0.1	0.6	524	1.1	0.0	0.3	431	0.5	0.0	13.0	22	18.1	0.0
2/18/10 9:30	3.2	653	5.9	0.2	2.0	581	3.7	0.1	0.5	519	0.9	0.0	0.3	427	0.5	0.0	11.0	21	15.2	0.0
2/18/10 10:00	3.5	660	6.5	0.2	2.6	584	4.8	0.2	1.2	520	2.2	0.1	0.3	423	0.5	0.0	11.0	21	15.2	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/18/10 10:30	3.0	647	5.6	0.2	1.7	575	3.1	0.1	0.4	514	0.7	0.0	0.3	423	0.5	0.0	11.0	21	15.2	0.0
2/18/10 11:00	3.1	647	5.7	0.2	1.7	574	3.1	0.1	0.7	512	1.3	0.0	0.3	419	0.5	0.0	13.0	21	18.1	0.0
2/18/10 11:30	3.3	647	6.1	0.2	2.2	572	4.0	0.1	0.6	510	1.1	0.0	0.3	416	0.5	0.0	14.0	21	19.6	0.0
2/18/10 12:00	3.3	641	6.1	0.2	1.8	570	3.3	0.1	0.6	510	1.1	0.0	0.3	419	0.5	0.0	13.0	21	18.1	0.0
2/18/10 12:30	3.0	647	5.6	0.2	1.8	571	3.3	0.1	0.6	507	1.1	0.0	0.3	412	0.5	0.0	16.0	21	22.6	0.0
2/18/10 13:00	2.9	641	5.4	0.2	2.0	567	3.7	0.1	0.4	505	0.7	0.0	0.3	412	0.5	0.0	16.0	21	22.6	0.0
2/18/10 13:30	2.9	635	5.4	0.2	2.6	563	4.8	0.2	0.5	503	0.9	0.0	0.3	412	0.5	0.0	13.0	21	18.1	0.0
2/18/10 14:00	2.9	641	5.4	0.2	2.2	567	4.0	0.1	0.6	505	1.1	0.0	0.2	412	0.4	0.0	15.0	21	21.1	0.0
2/18/10 14:30	3.3	635	6.1	0.2	1.9	562	3.5	0.1	0.5	500	0.9	0.0	0.2	408	0.4	0.0	12.0	21	16.6	0.0
2/18/10 15:00	3.0	629	5.6	0.2	2.0	558	3.7	0.1	0.6	498	1.1	0.0	0.3	408	0.5	0.0	13.0	21	18.1	0.0
2/18/10 15:30	2.9	641	5.4	0.2	2.0	566	3.7	0.1	0.4	503	0.7	0.0	0.3	408	0.5	0.0	10.0	21	13.7	0.0
2/18/10 16:00	2.9	629	5.4	0.2	2.2	557	4.0	0.1	0.5	496	0.9	0.0	0.2	404	0.4	0.0	9.9	20	13.6	0.0
2/18/10 16:30	3.2	629	5.9	0.2	2.2	557	4.0	0.1	0.6	496	1.1	0.0	0.3	404	0.5	0.0	12.0	20	16.6	0.0
2/18/10 17:00	2.9	623	5.4	0.2	2.0	551	3.7	0.1	1.4	491	2.6	0.1	0.2	401	0.4	0.0	9.0	20	12.3	0.0
2/18/10 17:30	3.1	623	5.7	0.2	2.4	551	4.4	0.1	0.5	491	0.9	0.0	0.2	401	0.4	0.0	12.0	20	16.6	0.0
2/18/10 18:00	3.1	623	5.7	0.2	2.1	550	3.9	0.1	0.5	489	0.9	0.0	0.4	397	0.7	0.0	11.0	20	15.2	0.0
2/18/10 18:30	2.9	617	5.4	0.2	2.2	545	4.0	0.1	0.6	484	1.1	0.0	0.3	393	0.5	0.0	10.0	20	13.7	0.0
2/18/10 19:00	3.1	617	5.7	0.2	2.2	546	4.0	0.1	0.4	486	0.7	0.0	0.2	397	0.4	0.0	9.6	20	13.1	0.0
2/18/10 19:30	3.4	617	6.3	0.2	2.5	544	4.6	0.1	1.1	482	2.0	0.1	0.3	390	0.5	0.0	9.8	20	13.4	0.0
2/18/10 20:00	3.3	611	6.1	0.2	2.2	540	4.0	0.1	0.4	480	0.7	0.0	0.2	390	0.4	0.0	9.4	20	12.8	0.0
2/18/10 20:30	3.1	611	5.7	0.2	2.1	540	3.9	0.1	0.5	480	0.9	0.0	0.3	390	0.5	0.0	9.6	20	13.1	0.0
2/18/10 21:00	2.9	605	5.4	0.2	2.2	536	4.0	0.1	0.5	477	0.9	0.0	0.2	390	0.4	0.0	10.0	20	13.7	0.0
2/18/10 21:30	3.3	611	6.1	0.2	2.1	537	3.9	0.1	0.4	475	0.7	0.0	0.3	382	0.5	0.0	11.0	19	15.2	0.0
2/18/10 22:00	2.9	605	5.4	0.2	2.2	535	4.0	0.1	0.4	473	0.7	0.0	0.3	386	0.5	0.0	8.0	19	10.8	0.0
2/18/10 22:30	2.9	605	5.4	0.2	2.2	533	4.0	0.1	0.6	473	1.1	0.0	0.3	382	0.5	0.0	9.1	19	12.4	0.0
2/18/10 23:00	3.2	605	5.9	0.2	2.2	533	4.0	0.1	0.4	473	0.7	0.0	0.3	382	0.5	0.0	8.4	19	11.4	0.0
2/18/10 23:30	2.9	599	5.4	0.2	2.2	528	4.0	0.1	0.4	468	0.7	0.0	0.2	379	0.4	0.0	10.0	19	13.7	0.0
2/19/10 0:00	3.2	599	5.9	0.2	2.0	528	3.7	0.1	0.4	468	0.7	0.0	0.3	379	0.5	0.0	9.0	19	12.3	0.0
2/19/10 0:30	2.9	593	5.4	0.2	2.0	523	3.7	0.1	0.4	464	0.7	0.0	0.3	375	0.5	0.0	8.5	19	11.5	0.0
2/19/10 1:00	2.9	588	5.4	0.2	2.5	519	4.6	0.1	0.3	462	0.5	0.0	0.2	375	0.4	0.0	9.5	19	13.0	0.0
2/19/10 1:30	2.9	593	5.4	0.2	2.0	523	3.7	0.1	0.4	464	0.7	0.0	0.3	375	0.5	0.0	10.0	19	13.7	0.0
2/19/10 2:00	2.9	599	5.4	0.2	2.1	527	3.9	0.1	0.4	466	0.7	0.0	0.2	375	0.4	0.0	9.2	19	12.6	0.0
2/19/10 2:30	3.3	593	6.1	0.2	1.9	522	3.5	0.1	0.3	462	0.5	0.0	0.3	372	0.5	0.0	8.5	19	11.5	0.0
2/19/10 3:00	3.1	588	5.7	0.2	1.9	518	3.5	0.1	0.4	460	0.7	0.0	0.3	372	0.5	0.0	8.0	19	10.8	0.0
2/19/10 3:30	3.1	582	5.7	0.2	2.0	513	3.7	0.1	0.4	455	0.7	0.0	0.3	368	0.5	0.0	9.0	19	12.3	0.0
2/19/10 4:00	3.0	582	5.6	0.2	1.8	512	3.3	0.1	0.4	453	0.7	0.0	0.2	365	0.4	0.0	8.2	18	11.1	0.0
2/19/10 4:30	3.1	588	5.7	0.2	2.2	516	4.0	0.1	0.5	455	0.9	0.0	0.2	365	0.4	0.0	7.4	18	10.0	0.0
2/19/10 5:00	2.9	582	5.4	0.2	2.1	512	3.9	0.1	0.7	453	1.3	0.0	0.2	365	0.4	0.0	9.3	18	12.7	0.0
2/19/10 5:30	2.9	582	5.4	0.2	1.8	511	3.3	0.1	0.4	451	0.7	0.0	0.2	361	0.4	0.0	8.8	18	12.0	0.0
2/19/10 6:00	3.4	576	6.3	0.2	1.8	507	3.3	0.1	0.6	449	1.1	0.0	0.2	361	0.4	0.0	7.4	18	10.0	0.0
2/19/10 6:30	3.1	570	5.7	0.2	2.3	503	4.2	0.1	0.4	446	0.7	0.0	0.3	361	0.5	0.0	8.8	18	12.0	0.0
2/19/10 7:00	3.0	570	5.6	0.2	1.8	503	3.3	0.1	0.4	446	0.7	0.0	0.3	361	0.5	0.0	7.1	18	9.5	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/19/10 7:30	3.2	576	5.9	0.2	1.8	506	3.3	0.1	0.4	447	0.7	0.0	0.3	358	0.5	0.0	8.3	18	11.3	0.0
2/19/10 8:00	3.0	570	5.6	0.2	2.2	502	4.0	0.1	0.4	444	0.7	0.0	0.3	358	0.5	0.0	8.5	18	11.5	0.0
2/19/10 8:30	3.1	565	5.7	0.2	2.6	498	4.8	0.1	0.4	442	0.7	0.0	0.3	358	0.5	0.0	6.8	18	9.1	0.0
2/19/10 9:00	3.1	570	5.7	0.2	2.1	501	3.9	0.1	0.4	442	0.7	0.0	0.3	354	0.5	0.0	8.4	18	11.4	0.0
2/19/10 9:30	2.8	570	5.2	0.2	1.8	501	3.3	0.1	0.4	442	0.7	0.0	0.2	354	0.4	0.0	7.4	18	10.0	0.0
2/19/10 10:00	2.9	565	5.4	0.2	1.8	496	3.3	0.1	1.3	438	2.4	0.1	0.2	351	0.4	0.0	7.5	18	10.1	0.0
2/19/10 10:30	3.0	559	5.6	0.2	1.8	492	3.3	0.1	0.4	436	0.7	0.0	0.2	351	0.4	0.0	7.7	18	10.4	0.0
2/19/10 11:00	3.0	559	5.6	0.2	1.7	492	3.1	0.1	1.4	436	2.6	0.1	0.3	351	0.5	0.0	7.0	18	9.4	0.0
2/19/10 11:30	3.3	559	6.1	0.2	2.5	491	4.6	0.1	0.4	434	0.7	0.0	0.2	347	0.4	0.0	8.0	18	10.8	0.0
2/19/10 12:00	3.1	559	5.7	0.2	2.0	491	3.7	0.1	0.3	434	0.5	0.0	0.2	347	0.4	0.0	10.0	18	13.7	0.0
2/19/10 12:30	3.0	559	5.6	0.2	1.8	491	3.3	0.1	0.3	434	0.5	0.0	0.6	347	1.1	0.0	16.0	18	22.6	0.0
2/19/10 13:00	2.9	559	5.4	0.2	2.2	490	4.0	0.1	0.4	432	0.7	0.0	0.3	344	0.5	0.0	10.0	17	13.7	0.0
2/19/10 13:30	3.0	548	5.6	0.2	1.9	482	3.5	0.1	0.4	427	0.7	0.0	0.2	344	0.4	0.0	12.0	17	16.6	0.0
2/19/10 14:00	3.0	548	5.6	0.2	1.7	481	3.1	0.1	0.4	425	0.7	0.0	0.2	341	0.4	0.0	9.0	17	12.3	0.0
2/19/10 14:30	3.1	542	5.7	0.2	1.9	478	3.5	0.1	0.2	425	0.4	0.0	0.3	344	0.5	0.0	9.1	17	12.4	0.0
2/19/10 15:00	3.0	548	5.6	0.2	2.1	481	3.9	0.1	0.4	425	0.7	0.0	0.3	341	0.5	0.0	8.3	17	11.3	0.0
2/19/10 15:30	3.0	548	5.6	0.2	2.2	480	4.0	0.1	0.3	423	0.5	0.0	0.2	337	0.4	0.0	7.1	17	9.5	0.0
2/19/10 16:00	3.0	542	5.6	0.2	2.0	476	3.7	0.1	0.7	421	1.3	0.0	0.3	337	0.5	0.0	8.7	17	11.8	0.0
2/19/10 16:30	3.3	542	6.1	0.2	2.1	476	3.9	0.1	0.4	421	0.7	0.0	0.2	337	0.4	0.0	8.4	17	11.4	0.0
2/19/10 17:00	3.1	542	5.7	0.2	2.1	475	3.9	0.1	0.3	419	0.5	0.0	0.2	334	0.4	0.0	7.9	17	10.7	0.0
2/19/10 17:30	3.3	537	6.1	0.2	2.3	472	4.2	0.1	0.4	417	0.7	0.0	0.3	334	0.5	0.0	8.5	17	11.5	0.0
2/19/10 18:00	3.1	531	5.7	0.2	2.5	467	4.6	0.1	0.3	412	0.5	0.0	0.2	331	0.4	0.0	9.1	17	12.4	0.0
2/19/10 18:30	2.9	537	5.4	0.2	2.3	470	4.2	0.1	0.4	415	0.7	0.0	0.2	331	0.4	0.0	6.6	17	8.8	0.0
2/19/10 19:00	3.1	537	5.7	0.2	2.0	470	3.7	0.1	0.2	415	0.4	0.0	0.2	331	0.4	0.0	7.7	17	10.4	0.0
2/19/10 19:30	3.0	531	5.6	0.2	2.3	467	4.2	0.1	0.3	412	0.5	0.0	0.5	331	0.9	0.0	8.2	17	11.1	0.0
2/19/10 20:00	2.9	526	5.4	0.2	2.2	462	4.0	0.1	0.6	408	1.1	0.0	0.3	327	0.5	0.0	6.5	17	8.7	0.0
2/19/10 20:30	5.3	526	9.9	0.3	2.3	461	4.2	0.1	0.3	406	0.5	0.0	0.4	324	0.7	0.0	7.9	17	10.7	0.0
2/19/10 21:00	2.9	526	5.4	0.2	2.1	461	3.9	0.1	0.3	406	0.5	0.0	0.2	324	0.4	0.0	7.4	17	10.0	0.0
2/19/10 21:30	3.0	526	5.6	0.2	2.1	461	3.9	0.1	0.3	406	0.5	0.0	0.2	324	0.4	0.0	6.9	17	9.2	0.0
2/19/10 22:00	3.4	521	6.3	0.2	2.1	456	3.9	0.1	0.2	402	0.4	0.0	0.2	321	0.4	0.0	8.4	16	11.4	0.0
2/19/10 22:30	2.9	521	5.4	0.2	2.3	456	4.2	0.1	0.2	402	0.4	0.0	0.2	321	0.4	0.0	6.3	16	8.4	0.0
2/19/10 23:00	3.0	521	5.6	0.2	2.0	456	3.7	0.1	0.4	402	0.7	0.0	0.3	321	0.5	0.0	7.0	16	9.4	0.0
2/19/10 23:30	2.9	515	5.4	0.2	2.2	453	4.0	0.1	0.4	400	0.7	0.0	0.2	321	0.4	0.0	8.6	16	11.7	0.0
2/20/10 0:00	2.9	515	5.4	0.2	2.0	452	3.7	0.1	0.3	398	0.5	0.0	0.3	318	0.5	0.0	9.2	16	12.6	0.0
2/20/10 0:30	3.2	515	5.9	0.2	2.4	451	4.4	0.1	0.3	396	0.5	0.0	0.2	314	0.4	0.0	6.9	16	9.2	0.0
2/20/10 1:00	3.3	515	6.1	0.2	2.1	452	3.9	0.1	0.3	398	0.5	0.0	0.2	318	0.4	0.0	6.6	16	8.8	0.0
2/20/10 1:30	3.4	515	6.3	0.2	2.0	451	3.7	0.1	0.3	396	0.5	0.0	0.3	314	0.5	0.0	7.6	16	10.2	0.0
2/20/10 2:00	3.1	510	5.7	0.2	2.0	447	3.7	0.1	0.3	394	0.5	0.0	0.2	314	0.4	0.0	7.1	16	9.5	0.0
2/20/10 2:30	2.9	510	5.4	0.2	2.0	447	3.7	0.1	0.2	394	0.4	0.0	0.2	314	0.4	0.0	8.5	16	11.5	0.0
2/20/10 3:00	3.0	510	5.6	0.2	2.0	446	3.7	0.1	0.3	392	0.5	0.0	0.2	311	0.4	0.0	7.8	16	10.5	0.0
2/20/10 3:30	3.1	510	5.7	0.2	1.9	446	3.5	0.1	0.4	392	0.7	0.0	0.2	311	0.4	0.0	7.5	16	10.1	0.0
2/20/10 4:00	3.3	504	6.1	0.2	2.0	441	3.7	0.1	0.3	388	0.5	0.0	0.2	308	0.4	0.0	8.1	16	11.0	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity	Streamflow	SSC	SSL	Turbidity	Streamflow	SSC	SSL	Turbidity	Streamflow	SSC	SSL	Turbidity	Streamflow	SSC	SSL	Turbidity	Streamflow	SSC	SSL
	(FNU)	(ft ³ /s)	(mg/L)	(T)	(FNU)	(ft ³ /s)	(mg/L)	(T)	(FNU)	(ft ³ /s)	(mg/L)	(T)	(FNU)	(ft ³ /s)	(mg/L)	(T)	(FNU)	(ft ³ /s)	(mg/L)	(T)
2/20/10 4:30	2.9	504	5.4	0.2	1.9	441	3.5	0.1	0.3	388	0.5	0.0	0.2	308	0.4	0.0	7.5	16	10.1	0.0
2/20/10 5:00	3.0	499	5.6	0.2	2.5	438	4.6	0.1	0.3	386	0.5	0.0	0.3	308	0.5	0.0	8.4	16	11.4	0.0
2/20/10 5:30	3.0	499	5.6	0.2	2.2	437	4.0	0.1	0.3	384	0.5	0.0	0.2	305	0.4	0.0	7.6	16	10.2	0.0
2/20/10 6:00	3.2	499	5.9	0.2	2.0	437	3.7	0.1	0.8	384	1.4	0.0	0.3	305	0.5	0.0	6.8	16	9.1	0.0
2/20/10 6:30	3.1	499	5.7	0.2	2.0	437	3.7	0.1	0.4	384	0.7	0.0	0.3	305	0.5	0.0	6.9	16	9.2	0.0
2/20/10 7:00	3.0	499	5.6	0.2	1.9	437	3.5	0.1	0.2	384	0.4	0.0	0.2	305	0.4	0.0	6.7	16	9.0	0.0
2/20/10 7:30	3.1	499	5.7	0.2	2.0	436	3.7	0.1	0.2	382	0.4	0.0	0.2	302	0.4	0.0	6.3	15	8.4	0.0
2/20/10 8:00	3.0	499	5.6	0.2	1.9	436	3.5	0.1	0.3	382	0.5	0.0	0.3	302	0.5	0.0	6.9	15	9.2	0.0
2/20/10 8:30	3.1	494	5.7	0.2	2.2	432	4.0	0.1	0.3	380	0.5	0.0	0.3	302	0.5	0.0	5.5	15	7.3	0.0
2/20/10 9:00	2.8	489	5.2	0.1	3.1	428	5.6	0.1	0.3	376	0.5	0.0	0.2	299	0.4	0.0	6.3	15	8.4	0.0
2/20/10 9:30	2.8	489	5.2	0.1	3.9	428	7.3	0.2	0.3	376	0.5	0.0	0.2	299	0.4	0.0	6.3	15	8.4	0.0
2/20/10 10:00	3.7	494	6.9	0.2	2.0	431	3.7	0.1	0.3	378	0.5	0.0	0.2	299	0.4	0.0	6.9	15	9.2	0.0
2/20/10 10:30	2.9	489	5.4	0.1	2.0	427	3.7	0.1	0.3	374	0.5	0.0	0.2	296	0.4	0.0	6.0	15	8.0	0.0
2/20/10 11:00	3.0	484	5.6	0.2	2.0	423	3.7	0.1	0.3	372	0.5	0.0	0.2	296	0.4	0.0	7.0	15	9.4	0.0
2/20/10 11:30	2.7	489	5.0	0.1	2.2	426	4.0	0.1	0.4	372	0.7	0.0	0.3	293	0.5	0.0	13.0	15	18.1	0.0
2/20/10 12:00	2.8	484	5.2	0.1	2.2	422	4.0	0.1	0.6	370	1.1	0.0	0.4	293	0.7	0.0	9.9	15	13.6	0.0
2/20/10 12:30	2.9	478	5.4	0.1	2.1	419	3.9	0.1	0.2	368	0.4	0.0	0.2	293	0.4	0.0	7.8	15	10.5	0.0
2/20/10 13:00	2.9	484	5.4	0.1	2.0	422	3.7	0.1	0.2	370	0.4	0.0	0.2	293	0.4	0.0	8.5	15	11.5	0.0
2/20/10 13:30	2.8	478	5.2	0.1	2.0	419	3.7	0.1	0.3	368	0.5	0.0	0.3	293	0.5	0.0	6.7	15	9.0	0.0
2/20/10 14:00	3.0	478	5.6	0.1	2.0	418	3.7	0.1	0.3	366	0.5	0.0	0.2	290	0.4	0.0	7.1	15	9.5	0.0
2/20/10 14:30	3.1	473	5.7	0.2	2.1	414	3.9	0.1	0.5	364	0.9	0.0	0.2	290	0.4	0.0	6.6	15	8.8	0.0
2/20/10 15:00	2.8	473	5.2	0.1	1.9	414	3.5	0.1	0.3	364	0.5	0.0	0.2	290	0.4	0.0	6.6	15	8.8	0.0
2/20/10 15:30	3.2	473	5.9	0.2	1.9	413	3.5	0.1	0.3	362	0.5	0.0	0.3	286	0.5	0.0	7.5	15	10.1	0.0
2/20/10 16:00	2.8	468	5.2	0.1	2.1	410	3.9	0.1	0.4	360	0.7	0.0	0.3	286	0.5	0.0	6.4	15	8.5	0.0
2/20/10 16:30	3.7	468	6.9	0.2	2.1	410	3.9	0.1	0.6	360	1.1	0.0	0.2	286	0.4	0.0	6.8	15	9.1	0.0
2/20/10 17:00	2.5	468	4.6	0.1	2.1	410	3.9	0.1	0.3	360	0.5	0.0	0.2	286	0.4	0.0	6.0	15	8.0	0.0
2/20/10 17:30	2.8	468	5.2	0.1	2.1	409	3.9	0.1	1.4	359	2.6	0.1	0.2	283	0.4	0.0	5.7	15	7.5	0.0
2/20/10 18:00	2.9	468	5.4	0.1	2.2	409	4.0	0.1	0.3	359	0.5	0.0	0.2	283	0.4	0.0	6.9	15	9.2	0.0
2/20/10 18:30	2.9	468	5.4	0.1	2.2	409	4.0	0.1	0.3	359	0.5	0.0	0.2	283	0.4	0.0	6.9	15	9.2	0.0
2/20/10 19:00	2.8	463	5.2	0.1	2.1	404	4.2	0.1	0.2	355	0.4	0.0	0.2	280	0.4	0.0	6.5	14	8.7	0.0
2/20/10 19:30	3.0	463	5.6	0.1	3.1	404	5.7	0.1	0.2	355	0.4	0.0	0.3	280	0.5	0.0	6.4	14	8.5	0.0
2/20/10 20:00	2.8	463	5.2	0.1	2.3	404	4.2	0.1	0.3	355	0.5	0.0	0.2	280	0.4	0.0	6.6	14	8.8	0.0
2/20/10 20:30	2.8	463	5.2	0.1	2.1	403	3.9	0.1	0.9	353	1.6	0.0	0.3	277	0.5	0.0	5.8	14	7.7	0.0
2/20/10 21:00	2.9	458	5.4	0.1	2.3	400	4.2	0.1	0.5	351	0.9	0.0	0.2	277	0.4	0.0	6.0	14	8.0	0.0
2/20/10 21:30	2.9	458	5.4	0.1	2.1	400	3.9	0.1	0.3	351	0.5	0.0	0.2	277	0.4	0.0	5.7	14	7.5	0.0
2/20/10 22:00	2.8	458	5.2	0.1	2.2	399	4.0	0.1	0.2	349	0.4	0.0	0.2	275	0.4	0.0	5.6	14	7.4	0.0
2/20/10 22:30	2.7	463	5.0	0.1	8.4	402	15.9	0.4	0.3	351	0.5	0.0	0.2	275	0.4	0.0	6.3	14	8.4	0.0
2/20/10 23:00	2.8	453	5.2	0.1	1.9	396	3.5	0.1	0.4	347	0.7	0.0	0.2	275	0.4	0.0	6.2	14	8.3	0.0
2/20/10 23:30	3.0	453	5.6	0.1	2.0	395	3.7	0.1	0.3	345	0.5	0.0	0.6	272	1.1	0.0	9.1	14	12.4	0.0
2/21/10 0:00	2.9	453	5.4	0.1	2.0	395	3.7	0.1	0.5	345	0.9	0.0	0.3	272	0.5	0.0	5.7	14	7.5	0.0
2/21/10 0:30	2.9	448	5.4	0.1	2.0	390	3.7	0.1	0.3	342	0.5	0.0	0.2	269	0.4	0.0	5.7	14	7.5	0.0
2/21/10 1:00	2.9	448	5.4	0.1	2.0	391	3.7	0.1	0.4	343	0.7	0.0	0.2	272	0.4	0.0	6.2	14	8.3	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/21/10 1:30	2.9	448	5.4	0.1	2.6	390	4.8	0.1	0.7	342	1.3	0.0	0.2	269	0.4	0.0	5.7	14	7.5	0.0
2/21/10 2:00	3.0	448	5.6	0.1	1.8	390	3.3	0.1	0.1	342	0.2	0.0	0.2	269	0.4	0.0	6.3	14	8.4	0.0
2/21/10 2:30	3.7	443	6.9	0.2	2.0	387	3.7	0.1	0.3	340	0.5	0.0	0.3	269	0.5	0.0	6.0	14	8.0	0.0
2/21/10 3:00	2.8	448	5.2	0.1	2.4	390	4.4	0.1	0.4	342	0.7	0.0	0.3	269	0.5	0.0	5.2	14	6.8	0.0
2/21/10 3:30	2.9	443	5.4	0.1	1.9	387	3.5	0.1	0.3	340	0.5	0.0	0.2	269	0.4	0.0	4.9	14	6.4	0.0
2/21/10 4:00	3.6	443	6.7	0.2	2.0	386	3.7	0.1	0.2	338	0.4	0.0	0.3	266	0.5	0.0	8.7	14	11.8	0.0
2/21/10 4:30	2.8	438	5.2	0.1	2.0	383	3.7	0.1	0.3	336	0.5	0.0	0.2	266	0.4	0.0	6.8	14	9.1	0.0
2/21/10 5:00	3.0	438	5.6	0.1	1.9	382	3.5	0.1	0.4	334	0.7	0.0	0.3	263	0.5	0.0	6.0	14	8.0	0.0
2/21/10 5:30	2.8	438	5.2	0.1	2.0	382	3.7	0.1	0.1	334	0.2	0.0	0.3	263	0.5	0.0	5.9	14	7.8	0.0
2/21/10 6:00	2.8	438	5.2	0.1	2.0	382	3.7	0.1	0.2	334	0.4	0.0	0.2	263	0.4	0.0	5.4	14	7.1	0.0
2/21/10 6:30	3.0	433	5.6	0.1	1.8	379	3.3	0.1	0.3	332	0.5	0.0	0.2	263	0.4	0.0	4.9	14	6.4	0.0
2/21/10 7:00	3.1	433	5.7	0.1	2.0	378	3.7	0.1	0.4	331	0.7	0.0	0.2	260	0.4	0.0	5.7	13	7.5	0.0
2/21/10 7:30	2.8	438	5.2	0.1	1.9	381	3.5	0.1	0.3	333	0.5	0.0	0.3	260	0.5	0.0	4.7	13	6.2	0.0
2/21/10 8:00	2.8	433	5.2	0.1	2.1	377	3.9	0.1	0.2	329	0.4	0.0	0.3	257	0.5	0.0	5.8	13	7.7	0.0
2/21/10 8:30	2.8	433	5.2	0.1	2.7	377	5.0	0.1	0.6	329	1.1	0.0	0.7	257	1.3	0.0	8.6	13	11.7	0.0
2/21/10 9:00	3.2	429	5.9	0.1	2.1	373	3.9	0.1	0.3	327	0.5	0.0	0.2	257	0.4	0.0	6.4	13	8.5	0.0
2/21/10 9:30	2.8	429	5.2	0.1	2.3	373	4.2	0.1	0.3	327	0.5	0.0	0.2	257	0.4	0.0	6.1	13	8.1	0.0
2/21/10 10:00	2.8	429	5.2	0.1	1.9	373	3.5	0.1	0.2	327	0.4	0.0	0.2	257	0.4	0.0	6.2	13	8.3	0.0
2/21/10 10:30	2.9	429	5.4	0.1	1.8	373	3.3	0.1	0.3	325	0.5	0.0	0.2	254	0.4	0.0	5.1	13	6.7	0.0
2/21/10 11:00	2.7	424	5.0	0.1	1.9	369	3.5	0.1	0.7	323	1.3	0.0	0.3	254	0.5	0.0	5.5	13	7.3	0.0
2/21/10 11:30	2.8	424	5.2	0.1	1.8	369	3.3	0.1	0.3	323	0.5	0.0	0.2	254	0.4	0.0	6.8	13	9.1	0.0
2/21/10 12:00	2.6	424	4.8	0.1	2.0	368	3.7	0.1	0.4	322	0.7	0.0	0.2	252	0.4	0.0	5.4	13	7.1	0.0
2/21/10 12:30	3.0	424	5.6	0.1	2.2	368	4.0	0.1	0.3	322	0.5	0.0	0.2	252	0.4	0.0	6.4	13	8.5	0.0
2/21/10 13:00	3.1	419	5.7	0.1	1.9	365	3.5	0.1	0.3	320	0.5	0.0	0.2	252	0.4	0.0	6.7	13	9.0	0.0
2/21/10 13:30	2.8	419	5.2	0.1	2.0	365	3.7	0.1	0.4	320	0.7	0.0	0.2	252	0.4	0.0	6.2	13	8.3	0.0
2/21/10 14:00	2.6	419	4.8	0.1	2.2	365	4.0	0.1	0.3	320	0.5	0.0	0.2	252	0.4	0.0	5.1	13	6.7	0.0
2/21/10 14:30	2.8	419	5.2	0.1	1.9	364	3.5	0.1	0.2	318	0.4	0.0	0.2	249	0.4	0.0	6.0	13	8.0	0.0
2/21/10 15:00	2.8	414	5.2	0.1	2.0	361	3.7	0.1	0.1	316	0.2	0.0	0.2	249	0.4	0.0	5.0	13	6.6	0.0
2/21/10 15:30	2.8	419	5.2	0.1	1.9	364	3.5	0.1	0.2	318	0.4	0.0	0.4	249	0.7	0.0	6.5	13	8.7	0.0
2/21/10 16:00	2.8	414	5.2	0.1	2.1	360	3.9	0.1	0.1	314	0.2	0.0	0.3	246	0.5	0.0	5.2	13	6.8	0.0
2/21/10 16:30	2.6	410	4.8	0.1	2.0	357	3.7	0.1	0.2	313	0.4	0.0	0.5	246	0.9	0.0	5.5	13	7.3	0.0
2/21/10 17:00	2.5	414	4.6	0.1	2.1	360	3.9	0.1	0.1	314	0.2	0.0	0.4	246	0.7	0.0	5.1	13	6.7	0.0
2/21/10 17:30	2.6	419	4.8	0.1	2.0	363	3.7	0.1	0.3	316	0.5	0.0	0.2	246	0.4	0.0	6.6	13	8.8	0.0
2/21/10 18:00	2.7	410	5.0	0.1	2.1	357	3.9	0.1	0.3	313	0.5	0.0	0.2	246	0.4	0.0	6.8	13	9.1	0.0
2/21/10 18:30	2.6	410	4.8	0.1	2.0	356	3.7	0.1	0.3	311	0.5	0.0	0.3	243	0.5	0.0	4.9	13	6.4	0.0
2/21/10 19:00	2.7	405	5.0	0.1	2.3	353	4.2	0.1	0.5	309	0.9	0.0	0.3	243	0.5	0.0	5.5	13	7.3	0.0
2/21/10 19:30	2.7	405	5.0	0.1	2.1	353	3.9	0.1	0.5	309	0.5	0.0	0.3	243	0.5	0.0	5.4	13	7.1	0.0
2/21/10 20:00	2.8	405	5.2	0.1	2.0	353	3.7	0.1	0.2	309	0.4	0.0	0.4	243	0.7	0.0	7.4	13	10.0	0.0
2/21/10 20:30	2.7	405	5.0	0.1	2.1	352	3.9	0.1	0.3	307	0.5	0.0	0.3	241	0.5	0.0	5.6	12	7.4	0.0
2/21/10 21:00	3.1	405	5.7	0.1	2.0	352	3.7	0.1	0.4	307	0.7	0.0	0.2	241	0.4	0.0	6.0	12	8.0	0.0
2/21/10 21:30	2.7	405	5.0	0.1	2.2	352	4.0	0.1	0.3	307	0.5	0.0	0.3	241	0.5	0.0	5.8	12	7.7	0.0
2/21/10 22:00	2.8	400	5.2	0.1	2.0	348	3.7	0.1	0.2	304	0.4	0.0	0.2	238	0.4	0.0	6.5	12	8.7	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/21/10 22:30	2.7	400	5.0	0.1	2.5	348	4.6	0.1	0.5	304	0.9	0.0	0.4	238	0.7	0.0	5.2	12	6.8	0.0
2/21/10 23:00	2.7	400	5.0	0.1	2.0	348	3.7	0.1	0.4	304	0.7	0.0	0.2	238	0.4	0.0	5.5	12	7.3	0.0
2/21/10 23:30	2.7	396	5.0	0.1	2.3	345	4.2	0.1	0.1	302	0.2	0.0	0.2	238	0.4	0.0	4.9	12	6.4	0.0
2/22/10 0:00	2.7	391	5.0	0.1	2.6	342	4.8	0.1	0.4	300	0.7	0.0	0.2	238	0.4	0.0	6.2	12	8.3	0.0
2/22/10 0:30	3.2	391	5.9	0.1	2.0	341	3.7	0.1	0.3	299	0.5	0.0	0.2	235	0.4	0.0	5.7	12	7.5	0.0
2/22/10 1:00	2.5	400	4.6	0.1	2.4	347	4.4	0.1	0.3	302	0.5	0.0	0.2	235	0.4	0.0	5.3	12	7.0	0.0
2/22/10 1:30	2.5	396	4.6	0.1	2.0	344	3.7	0.1	0.3	300	0.5	0.0	0.2	235	0.4	0.0	3.7	12	4.8	0.0
2/22/10 2:00	2.8	396	5.2	0.1	2.2	343	4.0	0.1	0.6	299	1.1	0.0	0.2	232	0.4	0.0	5.3	12	7.0	0.0
2/22/10 2:30	2.7	391	5.0	0.1	2.0	340	3.7	0.1	0.3	297	0.5	0.0	0.3	232	0.5	0.0	3.7	12	4.8	0.0
2/22/10 3:00	2.8	391	5.2	0.1	2.0	340	3.7	0.1	0.1	297	0.2	0.0	0.2	232	0.4	0.0	5.4	12	7.1	0.0
2/22/10 3:30	2.6	391	4.8	0.1	2.0	339	3.7	0.1	0.2	295	0.4	0.0	0.2	230	0.4	0.0	3.8	12	4.9	0.0
2/22/10 4:00	2.6	387	4.8	0.1	2.1	336	3.9	0.1	0.2	294	0.4	0.0	0.2	230	0.4	0.0	4.2	12	5.5	0.0
2/22/10 4:30	2.4	391	4.4	0.1	2.0	339	3.7	0.1	0.3	295	0.5	0.0	1.1	230	2.0	0.0	5.0	12	6.6	0.0
2/22/10 5:00	2.7	387	5.0	0.1	2.2	336	4.0	0.1	0.3	294	0.5	0.0	0.2	230	0.4	0.0	4.8	12	6.3	0.0
2/22/10 5:30	2.7	382	5.0	0.1	1.9	333	3.5	0.1	0.2	292	0.4	0.0	0.2	230	0.4	0.0	4.6	12	6.0	0.0
2/22/10 6:00	2.6	382	4.8	0.1	2.6	332	4.8	0.1	0.6	290	1.1	0.0	0.3	227	0.5	0.0	5.1	12	6.7	0.0
2/22/10 6:30	2.8	387	5.2	0.1	2.0	335	3.7	0.1	0.4	292	0.7	0.0	0.2	227	0.4	0.0	4.1	12	5.3	0.0
2/22/10 7:00	2.7	382	5.0	0.1	1.8	332	3.3	0.1	0.4	290	0.7	0.0	0.2	227	0.4	0.0	4.4	12	5.7	0.0
2/22/10 7:30	3.0	382	5.6	0.1	2.0	332	3.7	0.1	0.2	290	0.4	0.0	0.2	227	0.4	0.0	6.1	12	8.1	0.0
2/22/10 8:00	2.7	382	5.0	0.1	2.1	331	3.9	0.1	0.1	289	0.2	0.0	0.2	225	0.4	0.0	4.2	12	5.5	0.0
2/22/10 8:30	2.6	378	4.8	0.1	2.0	329	3.7	0.1	0.2	287	0.4	0.0	0.2	225	0.4	0.0	5.1	12	6.7	0.0
2/22/10 9:00	2.6	378	4.8	0.1	1.9	329	3.5	0.1	0.1	287	0.2	0.0	0.2	225	0.4	0.0	4.3	12	5.6	0.0
2/22/10 9:30	2.8	378	5.2	0.1	2.0	329	3.7	0.1	0.2	287	0.4	0.0	0.4	225	0.7	0.0	4.8	12	6.3	0.0
2/22/10 10:00	2.5	378	4.6	0.1	1.9	329	3.5	0.1	0.2	287	0.4	0.0	0.2	225	0.4	0.0	3.5	12	4.5	0.0
2/22/10 10:30	2.9	378	5.4	0.1	1.9	329	3.5	0.1	0.2	287	0.4	0.0	0.2	225	0.4	0.0	4.1	12	5.3	0.0
2/22/10 11:00	2.4	378	4.4	0.1	2.2	328	4.0	0.1	0.2	285	0.4	0.0	0.2	222	0.4	0.0	3.7	12	4.8	0.0
2/22/10 11:30	2.4	374	4.4	0.1	1.8	325	3.3	0.1	0.2	284	0.4	0.0	0.2	222	0.4	0.0	3.7	12	4.8	0.0
2/22/10 12:00	2.5	374	4.6	0.1	2.0	325	3.7	0.1	0.2	284	0.4	0.0	0.2	222	0.4	0.0	3.6	12	4.6	0.0
2/22/10 12:30	2.5	374	4.6	0.1	1.9	325	3.5	0.1	0.1	284	0.2	0.0	0.3	222	0.5	0.0	4.2	12	5.5	0.0
2/22/10 13:00	2.5	374	4.6	0.1	2.0	324	3.7	0.1	0.2	282	0.4	0.0	0.3	219	0.5	0.0	4.0	11	5.2	0.0
2/22/10 13:30	2.6	370	4.8	0.1	2.1	322	3.9	0.1	0.1	282	0.2	0.0	0.2	222	0.4	0.0	4.6	12	6.0	0.0
2/22/10 14:00	2.6	370	4.8	0.1	2.0	321	3.7	0.1	0.4	281	0.4	0.0	0.2	219	0.4	0.0	4.4	11	5.7	0.0
2/22/10 14:30	2.9	370	5.4	0.1	1.9	321	3.5	0.1	0.1	281	0.2	0.0	0.2	219	0.4	0.0	4.6	11	6.0	0.0
2/22/10 15:00	2.8	370	5.2	0.1	1.9	321	3.5	0.1	0.3	281	0.5	0.0	0.4	219	0.7	0.0	5.8	11	7.7	0.0
2/22/10 15:30	2.7	370	5.0	0.1	2.0	321	3.7	0.1	0.1	281	0.2	0.0	0.2	219	0.4	0.0	8.5	11	11.5	0.0
2/22/10 16:00	2.9	366	5.4	0.1	2.0	318	3.7	0.1	0.4	277	0.7	0.0	0.3	217	0.5	0.0	7.2	11	9.7	0.0
2/22/10 16:30	3.3	366	6.1	0.1	1.9	318	3.5	0.1	0.1	277	0.2	0.0	0.2	217	0.4	0.0	4.5	11	5.9	0.0
2/22/10 17:00	2.8	370	5.2	0.1	2.2	321	4.0	0.1	0.2	279	0.4	0.0	0.2	217	0.4	0.0	4.9	11	6.4	0.0
2/22/10 17:30	2.6	366	4.8	0.1	2.0	318	3.7	0.1	0.1	277	0.2	0.0	0.2	217	0.4	0.0	4.5	11	5.9	0.0
2/22/10 18:00	2.7	366	5.0	0.1	2.1	318	3.9	0.1	0.2	277	0.4	0.0	0.2	217	0.4	0.0	5.1	11	6.7	0.0
2/22/10 18:30	2.5	366	4.6	0.1	2.6	318	4.8	0.1	0.1	277	0.2	0.0	0.3	217	0.5	0.0	4.0	11	5.2	0.0
2/22/10 19:00	2.5	362	4.6	0.1	2.6	315	4.8	0.1	0.1	274	0.2	0.0	0.2	214	0.4	0.0	3.5	11	4.5	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/22/10 19:30	2.5	362	4.6	0.1	2.2	315	4.0	0.1	0.2	274	0.4	0.0	0.3	214	0.5	0.0	3.8	11	4.9	0.0
2/22/10 20:00	2.6	362	4.8	0.1	2.2	315	4.0	0.1	0.2	274	0.4	0.0	0.2	214	0.4	0.0	5.3	11	7.0	0.0
2/22/10 20:30	2.5	362	4.6	0.1	2.5	315	4.6	0.1	0.2	274	0.4	0.0	0.2	214	0.4	0.0	4.3	11	5.6	0.0
2/22/10 21:00	2.5	362	4.6	0.1	2.2	314	4.0	0.1	0.2	273	0.4	0.0	0.2	212	0.4	0.0	4.4	11	5.7	0.0
2/22/10 21:30	2.4	358	4.4	0.1	2.1	311	3.9	0.1	0.3	271	0.5	0.0	0.2	212	0.4	0.0	5.6	11	7.4	0.0
2/22/10 22:00	2.4	358	4.4	0.1	1.7	311	3.1	0.1	0.2	271	0.4	0.0	0.2	212	0.4	0.0	5.7	11	7.5	0.0
2/22/10 22:30	2.6	358	4.8	0.1	1.7	311	3.1	0.1	0.3	271	0.5	0.0	0.2	212	0.4	0.0	4.0	11	5.2	0.0
2/22/10 23:00	2.6	358	4.8	0.1	1.7	311	3.1	0.1	0.1	271	0.2	0.0	0.2	212	0.4	0.0	5.1	11	6.7	0.0
2/22/10 23:30	2.5	358	4.6	0.1	1.6	311	2.9	0.1	0.1	271	0.2	0.0	0.3	212	0.5	0.0	4.1	11	5.3	0.0
2/23/10 0:00	2.5	358	4.6	0.1	1.6	310	2.9	0.1	0.1	270	0.2	0.0	0.2	209	0.4	0.0	4.9	11	6.4	0.0
2/23/10 0:30	2.6	358	4.8	0.1	2.2	310	4.0	0.1	0.2	270	0.4	0.0	0.2	209	0.4	0.0	3.3	11	4.2	0.0
2/23/10 1:00	2.6	354	4.8	0.1	1.6	308	2.9	0.1	0.2	268	0.4	0.0	0.2	209	0.4	0.0	4.1	11	5.3	0.0
2/23/10 1:30	2.5	354	4.6	0.1	1.7	308	3.1	0.1	0.3	268	0.5	0.0	0.2	209	0.4	0.0	4.1	11	5.3	0.0
2/23/10 2:00	2.9	354	5.0	0.1	1.7	307	3.1	0.1	0.1	267	0.2	0.0	0.2	207	0.4	0.0	3.7	11	4.8	0.0
2/23/10 2:30	2.7	354	5.0	0.1	1.6	307	2.9	0.1	0.3	267	0.5	0.0	0.2	207	0.4	0.0	3.8	11	4.9	0.0
2/23/10 3:00	2.8	351	5.2	0.1	1.8	304	3.3	0.1	0.2	265	0.4	0.0	0.2	207	0.4	0.0	4.4	11	5.7	0.0
2/23/10 3:30	3.0	354	5.6	0.1	1.7	307	3.1	0.1	0.1	267	0.2	0.0	0.2	207	0.4	0.0	4.2	11	5.5	0.0
2/23/10 4:00	2.6	351	4.8	0.1	1.8	304	3.3	0.1	0.3	265	0.5	0.0	0.2	207	0.4	0.0	3.7	11	4.8	0.0
2/23/10 4:30	2.9	354	5.4	0.1	1.9	307	3.5	0.1	0.1	267	0.2	0.0	0.3	207	0.5	0.0	3.6	11	4.6	0.0
2/23/10 5:00	2.7	347	5.0	0.1	1.7	301	3.1	0.1	0.4	262	0.7	0.0	0.2	204	0.4	0.0	4.1	11	5.3	0.0
2/23/10 5:30	2.7	351	5.0	0.1	1.6	303	2.9	0.0	0.3	264	0.5	0.0	0.2	204	0.4	0.0	5.0	11	6.6	0.0
2/23/10 6:00	2.8	351	5.2	0.1	1.6	303	2.9	0.0	0.3	264	0.5	0.0	0.2	204	0.4	0.0	4.2	11	5.5	0.0
2/23/10 6:30	2.7	347	5.0	0.1	1.5	301	2.7	0.0	0.2	262	0.4	0.0	0.2	204	0.4	0.0	3.8	11	4.9	0.0
2/23/10 7:00	2.3	351	4.2	0.1	1.6	303	2.9	0.0	0.2	264	0.4	0.0	0.2	204	0.4	0.0	7.7	11	10.4	0.0
2/23/10 7:30	2.7	347	5.0	0.1	1.7	301	3.1	0.1	0.1	262	0.2	0.0	0.2	204	0.4	0.0	4.4	11	5.7	0.0
2/23/10 8:00	2.7	347	5.0	0.1	1.6	300	2.9	0.0	0.3	261	0.5	0.0	0.2	202	0.4	0.0	3.5	11	4.5	0.0
2/23/10 8:30	2.7	347	5.0	0.1	1.5	300	2.7	0.0	0.2	261	0.4	0.0	0.3	202	0.5	0.0	4.6	11	6.0	0.0
2/23/10 9:00	2.6	347	4.8	0.1	1.5	300	2.7	0.0	0.3	261	0.5	0.0	0.2	202	0.4	0.0	3.9	11	5.0	0.0
2/23/10 9:30	2.6	347	4.8	0.1	1.7	300	3.1	0.1	0.1	261	0.2	0.0	0.2	202	0.4	0.0	4.9	11	6.4	0.0
2/23/10 10:00	2.6	343	4.8	0.1	1.6	297	2.9	0.0	0.3	259	0.5	0.0	0.2	202	0.4	0.0	15.0	11	21.1	0.0
2/23/10 10:30	2.7	343	5.0	0.1	1.5	297	2.7	0.0	0.1	259	0.2	0.0	0.2	202	0.4	0.0	740.0	11	1325.8	0.8
2/23/10 11:00	2.5	339	4.6	0.1	1.5	294	2.7	0.0	0.1	256	0.2	0.0	0.2	199	0.4	0.0	460.0	10	800.2	0.5
2/23/10 11:30	2.5	343	4.6	0.1	1.7	297	3.1	0.1	0.2	258	0.2	0.0	0.2	199	0.4	0.0	140.0	10	226.2	0.1
2/23/10 12:00	2.5	343	4.6	0.1	1.7	297	3.1	0.1	0.2	258	0.4	0.0	0.2	199	0.4	0.0	81.0	10	126.5	0.1
2/23/10 12:30	2.7	343	5.0	0.1	1.6	297	2.9	0.0	0.2	258	0.4	0.0	0.2	199	0.4	0.0	45.0	10	67.8	0.0
2/23/10 13:00	2.7	343	5.0	0.1	1.8	297	3.3	0.1	0.3	258	0.5	0.0	0.2	199	0.4	0.0	40.0	10	59.8	0.0
2/23/10 13:30	2.5	343	4.6	0.1	1.7	297	3.1	0.1	0.2	258	0.4	0.0	0.2	199	0.4	0.0	33.0	10	48.7	0.0
2/23/10 14:00	2.4	343	4.4	0.1	1.6	297	2.9	0.0	0.1	258	0.2	0.0	0.2	199	0.4	0.0	30.0	10	44.0	0.0
2/23/10 14:30	2.5	343	4.6	0.1	1.7	297	3.1	0.1	0.4	258	0.7	0.0	0.4	199	0.7	0.0	31.0	10	45.6	0.0
2/23/10 15:00	2.7	343	5.0	0.1	1.6	297	2.9	0.0	0.2	258	3.9	0.1	0.2	199	0.4	0.0	24.0	10	34.8	0.0
2/23/10 15:30	2.4	343	4.4	0.1	1.6	297	2.9	0.0	5.3	258	9.9	0.1	0.2	199	0.4	0.0	26.0	10	37.8	0.0
2/23/10 16:00	2.7	343	5.0	0.1	1.8	297	3.3	0.1	7.6	258	14.3	0.2	0.2	199	0.4	0.0	27.0	10	39.4	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/23/10 16:30	2.7	343	5.0	0.1	1.8	296	3.3	0.1	7.6	256	14.3	0.2	0.3	197	0.5	0.0	48.0	10	72.6	0.0
2/23/10 17:00	2.5	343	4.6	0.1	2.0	296	3.7	0.1	6.4	256	12.0	0.2	0.2	197	0.4	0.0	75.0	10	116.6	0.1
2/23/10 17:30	2.8	347	5.2	0.1	2.9	299	5.4	0.1	4.7	259	8.8	0.1	0.2	199	0.4	0.0	140.0	10	226.2	0.1
2/23/10 18:00	2.8	347	5.2	0.1	5.1	299	9.5	0.2	3.2	259	5.9	0.1	0.3	199	0.5	0.0	120.0	10	192.0	0.1
2/23/10 18:30	2.8	351	5.2	0.1	6.1	303	11.4	0.2	2.4	262	4.4	0.1	0.2	202	0.4	0.0	110.0	11	175.1	0.1
2/23/10 19:00	3.1	351	5.7	0.1	6.5	303	12.2	0.2	2.1	264	3.9	0.1	0.3	204	0.5	0.0	110.0	11	175.1	0.1
2/23/10 19:30	2.8	354	5.2	0.1	5.6	307	10.5	0.2	1.7	267	3.1	0.0	0.3	207	0.5	0.0	97.0	11	153.2	0.1
2/23/10 20:00	2.7	358	5.0	0.1	4.8	310	9.0	0.2	1.3	270	2.4	0.0	0.2	209	0.4	0.0	70.0	11	108.3	0.1
2/23/10 20:30	2.8	362	5.2	0.1	4.0	314	7.4	0.1	1.2	273	2.2	0.0	0.2	212	0.4	0.0	780.0	11	1402.1	0.9
2/23/10 21:00	2.6	366	4.8	0.1	3.2	317	5.9	0.1	1.5	276	2.7	0.0	0.2	214	0.4	0.0	610.0	11	1079.9	0.7
2/23/10 21:30	2.9	370	5.4	0.1	3.0	321	5.6	0.1	1.7	279	3.1	0.0	0.3	217	0.5	0.0	250.0	11	418.7	0.3
2/23/10 22:00	2.8	374	5.2	0.1	2.8	324	5.2	0.1	2.1	282	3.9	0.1	0.2	219	0.4	0.0	390.0	11	671.5	0.4
2/23/10 22:30	3.1	374	5.7	0.1	3.1	325	5.7	0.1	3.2	284	5.9	0.1	0.2	222	0.4	0.0	270.0	12	454.4	0.3
2/23/10 23:00	3.2	378	5.9	0.1	2.7	329	5.0	0.1	3.2	288	5.9	0.1	0.3	232	0.5	0.0	150.0	12	243.4	0.2
2/23/10 23:30	3.1	378	5.7	0.1	2.8	331	5.2	0.1	3.7	292	6.9	0.1	0.3	235	0.4	0.0	360.0	12	616.8	0.4
2/24/10 0:00	2.9	382	5.4	0.1	2.9	335	5.4	0.1	3.6	295	6.7	0.1	0.2	235	0.4	0.0	520.0	12	911.5	0.6
2/24/10 0:30	3.5	382	6.5	0.1	3.7	336	6.9	0.1	4.3	298	8.0	0.1	0.3	241	0.5	0.0	160.0	12	260.7	0.2
2/24/10 1:00	4.0	387	7.4	0.2	4.0	340	7.4	0.1	9.1	302	17.2	0.3	0.2	243	0.4	0.0	120.0	13	192.0	0.1
2/24/10 1:30	4.8	387	9.0	0.2	4.0	340	7.4	0.1	15.9	302	30.4	0.5	0.2	243	0.4	0.0	88.0	13	138.1	0.1
2/24/10 2:00	5.5	391	10.3	0.2	4.2	344	7.8	0.2	15.1	305	28.9	0.5	0.3	246	0.5	0.0	110.0	13	175.1	0.1
2/24/10 2:30	5.8	391	10.9	0.2	4.7	345	8.8	0.2	13.6	307	25.9	0.4	0.3	249	0.5	0.0	120.0	13	192.0	0.1
2/24/10 3:00	5.4	396	10.1	0.2	6.1	348	11.4	0.2	11.8	309	22.4	0.4	0.3	257	0.4	0.0	200.0	13	330.4	0.2
2/24/10 3:30	4.8	396	9.0	0.2	9.2	350	17.4	0.3	10.4	312	19.7	0.3	0.2	254	0.4	0.0	180.0	13	295.4	0.2
2/24/10 4:00	4.7	405	8.8	0.2	11.3	357	21.5	0.4	10.9	317	20.7	0.4	0.2	257	0.4	0.0	170.0	13	278.0	0.2
2/24/10 4:30	4.0	405	7.4	0.2	11.3	358	21.5	0.4	11.3	319	21.5	0.4	0.3	260	0.5	0.0	320.0	13	544.2	0.4
2/24/10 5:00	3.9	410	7.3	0.2	10.6	363	20.1	0.4	9.2	324	17.4	0.3	0.2	266	0.4	0.0	210.0	14	347.9	0.3
2/24/10 5:30	3.9	419	6.9	0.2	8.7	373	16.4	0.3	6.6	333	12.4	0.2	0.2	275	0.4	0.0	86.0	14	134.8	0.1
2/24/10 6:00	3.5	419	6.5	0.2	8.9	374	16.8	0.4	5.0	337	9.3	0.2	0.3	280	0.5	0.0	70.0	14	108.3	0.1
2/24/10 6:30	3.9	424	7.3	0.2	9.1	381	17.2	0.4	5.3	344	9.9	0.2	0.3	290	0.5	0.0	220.0	15	365.6	0.3
2/24/10 7:00	4.1	429	7.6	0.2	8.4	389	15.9	0.3	5.5	355	10.3	0.2	0.3	305	0.5	0.0	380.0	16	653.2	0.6
2/24/10 7:30	3.9	429	7.3	0.2	7.6	396	14.3	0.3	6.1	369	11.4	0.2	0.4	327	0.7	0.0	360.0	17	616.8	0.6
2/24/10 8:00	4.7	438	8.8	0.2	5.8	411	10.9	0.3	6.6	388	12.4	0.3	0.4	354	0.7	0.0	1150.0	18	2117.6	2.1
2/24/10 8:30	4.3	448	8.0	0.2	5.8	427	10.9	0.3	8.4	409	15.9	0.4	0.3	382	0.5	0.0	600.0	19	1061.1	1.2
2/24/10 9:00	4.9	458	9.2	0.2	5.4	440	10.1	0.2	8.1	424	15.3	0.4	0.3	401	0.5	0.0	560.0	20	837.2	0.9
2/24/10 9:30	5.8	463	10.9	0.3	6.4	452	12.0	0.3	5.4	442	10.1	0.3	0.3	427	0.5	0.0	560.0	21	986.1	1.2
2/24/10 10:00	6.8	478	12.8	0.3	7.2	471	13.6	0.4	8.6	464	16.3	0.4	0.7	454	1.3	0.0	1060.0	23	1942.0	2.5
2/24/10 10:30	8.6	484	16.3	0.4	9.1	481	17.2	0.5	14.7	478	28.1	0.8	0.4	475	0.7	0.0	180.0	24	295.4	0.4
2/24/10 11:00	9.6	499	18.2	0.5	7.3	499	13.7	0.4	26.4	499	51.0	1.4	0.3	500	0.5	0.0	95.0	25	149.8	0.2
2/24/10 11:30	9.2	515	17.4	0.5	6.6	516	12.4	0.4	30.8	516	59.7	1.7	0.3	517	0.5	0.0	87.0	26	136.5	0.2
2/24/10 12:00	8.7	542	16.4	0.5	10.0	541	19.0	0.6	25.2	540	48.7	1.5	1.0	539	1.8	0.1	140.0	27	226.2	0.3
2/24/10 12:30	11.0	576	20.9	0.7	17.8	565	34.1	1.1	26.1	556	50.4	1.6	0.4	543	0.7	0.0	84.0	27	131.5	0.2
2/24/10 13:00	8.2	611	15.5	0.5	24.5	592	47.3	1.6	20.2	576	38.8	1.3	0.5	552	0.9	0.0	54.0	27	82.2	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/24/10 13:30	9.3	653	17.6	0.6	21.2	622	40.8	1.4	10.0	596	19.0	0.6	0.6	556	1.1	0.0	44.0	27	66.2	0.1
2/24/10 14:00	6.9	680	13.0	0.5	21.5	641	41.4	1.5	6.6	609	12.4	0.4	0.4	561	0.7	0.0	68.0	28	105.0	0.2
2/24/10 14:30	7.1	714	13.4	0.5	17.8	661	34.1	1.3	5.7	618	10.7	0.4	0.5	552	0.9	0.0	61.0	27	93.6	0.1
2/24/10 15:00	8.0	727	15.1	0.6	10.7	672	20.3	0.8	5.0	626	9.3	0.3	0.3	556	0.5	0.0	39.0	27	58.2	0.1
2/24/10 15:30	7.3	755	13.8	0.6	7.0	690	13.2	0.5	3.9	635	7.3	0.3	0.4	552	0.7	0.0	35.0	27	51.9	0.1
2/24/10 16:00	7.2	770	13.5	0.6	5.8	700	10.9	0.4	2.6	640	4.8	0.2	0.4	552	0.7	0.0	36.0	27	53.5	0.1
2/24/10 16:30	7.0	784	13.1	0.6	5.5	709	10.3	0.4	2.7	646	5.0	0.2	0.6	552	1.1	0.0	150.0	27	243.4	0.4
2/24/10 17:00	7.9	791	14.9	0.7	4.8	714	9.0	0.4	2.8	649	5.2	0.2	0.5	552	0.9	0.0	75.0	27	116.6	0.2
2/24/10 17:30	13.0	791	24.8	1.1	5.0	714	9.3	0.4	2.0	649	3.7	0.1	0.5	552	0.9	0.0	59.0	27	90.3	0.1
2/24/10 18:00	16.0	791	30.6	1.4	3.7	711	6.9	0.3	1.7	644	3.1	0.1	0.3	543	0.5	0.0	37.0	27	55.0	0.1
2/24/10 18:30	16.0	799	30.6	1.4	3.9	718	7.3	0.3	1.7	650	3.1	0.1	0.6	547	1.1	0.0	41.0	27	61.4	0.1
2/24/10 19:00	14.0	799	26.7	1.2	3.6	721	6.7	0.3	2.4	655	4.4	0.2	0.5	556	0.9	0.0	350.0	27	598.6	0.9
2/24/10 19:30	12.0	799	22.8	1.0	3.6	721	6.7	0.3	3.4	655	6.3	0.2	0.7	556	1.3	0.0	130.0	27	209.1	0.3
2/24/10 20:00	8.2	806	15.5	0.7	3.3	731	6.1	0.3	2.6	669	4.8	0.2	0.5	575	0.9	0.0	350.0	28	598.6	1.0
2/24/10 20:30	5.3	828	9.9	0.5	4.4	751	8.2	0.3	2.2	686	4.0	0.2	0.3	588	0.5	0.0	570.0	29	1004.8	1.6
2/24/10 21:00	5.1	843	9.5	0.5	4.8	769	9.0	0.4	2.7	706	5.0	0.2	0.4	612	0.7	0.0	1020.0	30	1864.3	3.2
2/24/10 21:30	4.1	843	7.6	0.4	4.2	778	7.8	0.3	6.1	723	11.4	0.5	0.4	641	0.7	0.0	550.0	31	967.4	1.7
2/24/10 22:00	4.4	859	8.2	0.4	4.8	793	9.0	0.4	5.9	738	11.1	0.5	0.7	656	1.3	0.0	320.0	32	544.2	1.0
2/24/10 22:30	3.6	866	6.7	0.3	5.3	807	9.9	0.4	10.6	756	20.1	0.9	0.4	681	0.7	0.0	920.0	33	1670.7	3.1
2/24/10 23:00	4.6	874	8.6	0.4	7.2	818	13.6	0.6	25.3	772	48.8	2.1	0.6	702	1.1	0.0	420.0	34	726.5	1.4
2/24/10 23:30	5.0	890	9.3	0.5	8.1	834	15.3	0.7	28.8	787	55.8	2.5	0.5	717	0.9	0.0	450.0	35	781.7	1.5
2/25/10 0:00	5.1	921	9.5	0.5	12.4	857	23.6	1.1	21.7	803	41.8	1.9	0.5	722	0.9	0.0	150.0	35	243.4	0.5
2/25/10 0:30	4.8	929	9.0	0.5	21.5	868	41.4	2.0	22.1	816	42.6	2.0	0.4	738	0.7	0.0	91.0	36	143.1	0.3
2/25/10 1:00	5.5	978	10.3	0.6	23.9	904	46.1	2.3	22.5	842	43.3	2.1	0.5	749	0.9	0.0	82.0	36	128.2	0.3
2/25/10 1:30	6.5	1012	12.2	0.7	20.9	927	40.2	2.1	16.4	856	31.4	1.5	0.4	749	0.7	0.0	100.0	36	158.2	0.3
2/25/10 2:00	4.9	1020	9.2	0.5	21.1	933	40.6	2.1	9.8	859	18.6	0.9	0.8	749	1.4	0.1	65.0	36	100.1	0.2
2/25/10 2:30	5.1	1029	9.5	0.6	17.9	941	34.3	1.8	8.1	866	15.3	0.7	0.4	754	0.7	0.0	64.0	37	98.5	0.2
2/25/10 3:00	8.9	1058	16.8	1.0	14.0	960	26.7	1.4	6.9	878	13.0	0.6	0.5	754	0.9	0.0	62.0	37	95.2	0.2
2/25/10 3:30	7.1	1058	13.4	0.8	9.4	962	17.8	1.0	5.1	881	9.5	0.5	0.7	760	1.3	0.1	45.0	37	67.8	0.1
2/25/10 4:00	12.0	1058	22.8	1.4	6.5	960	12.2	0.7	3.7	878	6.9	0.3	0.3	754	0.5	0.0	43.0	37	64.6	0.1
2/25/10 4:30	17.0	1067	32.6	2.0	6.1	963	11.4	0.6	3.4	875	6.3	0.3	0.6	744	1.1	0.0	43.0	36	64.6	0.1
2/25/10 5:00	18.0	1077	34.5	2.1	5.0	971	9.3	0.5	3.6	882	6.7	0.3	0.3	749	0.5	0.0	55.0	36	83.9	0.2
2/25/10 5:30	17.0	1086	32.6	2.0	4.8	971	9.0	0.5	4.0	874	7.4	0.4	0.4	728	0.7	0.0	50.0	35	75.8	0.2
2/25/10 6:00	17.0	1077	32.6	2.0	5.0	968	9.3	0.5	2.7	876	5.0	0.2	0.4	738	0.7	0.0	56.0	36	85.5	0.2
2/25/10 6:30	16.0	1077	30.6	1.9	5.9	964	11.1	0.6	2.5	870	4.6	0.2	0.3	728	0.5	0.0	51.0	35	77.4	0.2
2/25/10 7:00	12.0	1067	22.8	1.4	5.1	959	9.5	0.5	2.1	869	3.9	0.2	0.4	733	0.7	0.0	89.0	36	139.8	0.3
2/25/10 7:30	8.9	1077	16.8	1.0	4.0	964	7.4	0.4	2.4	870	4.4	0.2	0.5	728	0.9	0.0	300.0	35	508.2	1.0
2/25/10 8:00	7.4	1067	13.9	0.8	4.2	954	7.8	0.4	2.6	859	4.8	0.2	0.3	717	0.5	0.0	200.0	35	330.4	0.6
2/25/10 8:30	5.2	1058	9.7	0.6	4.3	950	8.0	0.4	2.5	859	4.6	0.2	0.4	722	0.7	0.0	87.0	35	136.5	0.3
2/25/10 9:00	4.8	1086	9.0	0.5	3.8	964	7.1	0.4	3.6	861	6.7	0.3	0.4	707	0.7	0.0	120.0	34	192.0	0.4
2/25/10 9:30	5.4	1058	10.1	0.6	3.1	943	5.7	0.3	4.8	846	9.0	0.4	0.4	702	0.7	0.0	54.0	34	82.2	0.2
2/25/10 10:00	5.9	1039	11.1	0.6	4.0	930	7.4	0.4	8.7	839	16.4	0.8	0.3	702	0.5	0.0	86.0	34	134.8	0.3

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/25/10 10:30	3.8	1029	7.1	0.4	4.1	920	7.6	0.4	5.9	829	11.1	0.5	0.3	691	0.5	0.0	270.0	34	454.4	0.9
2/25/10 11:00	3.0	1048	5.6	0.3	6.6	935	12.4	0.7	3.7	839	6.9	0.3	0.8	696	1.4	0.1	93.0	34	146.5	0.3
2/25/10 11:30	3.4	1039	6.3	0.4	8.0	925	15.1	0.8	3.3	829	6.1	0.3	0.2	686	0.4	0.0	57.0	33	87.1	0.2
2/25/10 12:00	3.3	1020	6.1	0.4	5.8	908	10.9	0.6	2.7	813	5.0	0.2	0.3	671	0.5	0.0	85.0	33	133.1	0.2
2/25/10 12:30	4.2	1012	7.8	0.4	4.5	903	8.4	0.4	4.7	812	8.8	0.4	0.3	676	0.5	0.0	48.0	33	72.6	0.1
2/25/10 13:00	2.8	995	5.2	0.3	4.3	887	8.0	0.4	5.6	797	10.5	0.5	0.4	661	0.7	0.0	47.0	32	71.0	0.1
2/25/10 13:30	3.5	995	6.5	0.4	4.3	889	8.0	0.4	3.6	800	6.7	0.3	0.3	666	0.5	0.0	55.0	33	83.9	0.2
2/25/10 14:00	3.0	1003	5.6	0.3	5.9	893	11.1	0.6	2.8	800	5.2	0.2	0.4	661	0.7	0.0	43.0	32	64.6	0.1
2/25/10 14:30	2.9	978	5.4	0.3	5.6	876	10.5	0.5	2.6	790	4.8	0.2	0.3	661	0.5	0.0	42.0	32	63.0	0.1
2/25/10 15:00	4.7	970	8.8	0.5	4.7	869	8.8	0.4	1.9	784	3.5	0.2	0.3	656	0.5	0.0	32.0	32	47.2	0.1
2/25/10 15:30	5.0	970	9.3	0.5	4.3	867	8.0	0.4	1.8	781	3.3	0.1	0.2	651	0.4	0.0	32.0	32	47.2	0.1
2/25/10 16:00	5.3	962	9.9	0.5	3.7	860	6.9	0.3	2.0	774	3.7	0.2	0.2	646	0.4	0.0	30.0	32	44.0	0.1
2/25/10 16:30	3.9	962	7.3	0.4	3.4	860	6.3	0.3	1.8	774	3.3	0.1	0.3	646	0.5	0.0	28.0	32	40.9	0.1
2/25/10 17:00	3.6	945	6.7	0.4	6.6	847	12.4	0.6	1.5	765	2.7	0.1	0.4	641	0.7	0.0	28.0	31	40.9	0.1
2/25/10 17:30	3.0	945	5.6	0.3	3.5	844	6.5	0.3	1.9	759	3.5	0.1	0.3	631	0.5	0.0	26.0	31	37.8	0.1
2/25/10 18:00	3.7	945	6.9	0.4	3.1	843	5.7	0.3	1.2	756	2.2	0.1	0.2	626	0.4	0.0	28.0	31	40.9	0.1
2/25/10 18:30	3.9	929	7.3	0.4	3.2	829	5.9	0.3	1.5	744	2.7	0.1	0.4	617	0.7	0.0	28.0	30	40.9	0.1
2/25/10 19:00	3.5	929	6.5	0.3	3.7	832	6.9	0.3	1.2	750	2.2	0.1	0.2	626	0.4	0.0	25.0	31	36.3	0.1
2/25/10 19:30	3.3	921	6.1	0.3	2.8	823	5.2	0.2	1.2	741	2.2	0.1	0.3	617	0.5	0.0	25.0	30	36.3	0.1
2/25/10 20:00	2.7	913	5.0	0.3	2.6	818	4.8	0.2	1.2	737	2.2	0.1	0.3	617	0.5	0.0	26.0	30	37.8	0.1
2/25/10 20:30	2.5	905	4.6	0.2	2.9	811	5.4	0.2	1.0	731	1.8	0.1	0.4	612	0.7	0.0	24.0	30	34.8	0.1
2/25/10 21:00	2.3	905	4.2	0.2	4.5	808	5.2	0.2	1.1	726	2.0	0.1	0.3	602	0.5	0.0	24.0	30	34.8	0.1
2/25/10 21:30	2.3	897	4.2	0.2	2.6	805	8.4	0.4	2.7	728	5.0	0.2	0.3	612	0.5	0.0	26.0	30	37.8	0.1
2/25/10 22:00	2.2	897	4.0	0.2	2.6	799	4.8	0.2	1.4	720	2.6	0.1	0.6	598	1.1	0.0	28.0	29	56.6	0.1
2/25/10 22:30	2.1	897	3.9	0.2	2.6	801	4.8	0.2	1.4	720	2.7	0.1	0.3	598	0.5	0.0	28.0	29	40.9	0.1
2/25/10 23:00	2.0	897	3.7	0.2	2.7	801	5.0	0.2	1.5	720	2.7	0.1	0.3	598	0.5	0.0	25.0	29	36.3	0.1
2/25/10 23:30	2.5	882	4.6	0.2	3.7	790	6.9	0.3	1.3	713	2.4	0.1	0.3	598	0.5	0.0	28.0	29	42.5	0.1
2/26/10 0:00	1.9	897	3.5	0.2	2.9	799	5.4	0.2	1.2	717	2.2	0.1	0.2	593	0.4	0.0	29.0	29	40.9	0.1
2/26/10 0:30	1.7	874	3.1	0.2	2.9	784	5.4	0.2	1.4	707	2.6	0.1	0.2	593	0.4	0.0	28.0	29	51.9	0.1
2/26/10 1:00	1.5	882	2.7	0.1	2.5	789	4.6	0.2	0.9	711	1.6	0.1	0.3	593	0.5	0.0	35.0	29	40.9	0.1
2/26/10 1:30	1.8	859	3.3	0.2	2.8	772	5.2	0.2	1.0	698	1.8	0.1	0.3	588	0.5	0.0	91.0	29	143.1	0.2
2/26/10 2:00	1.7	874	3.1	0.2	3.1	782	5.7	0.3	1.0	705	1.8	0.1	0.2	588	0.4	0.0	56.0	29	85.5	0.1
2/26/10 2:30	2.0	859	3.7	0.2	3.3	772	6.1	0.3	1.5	698	2.7	0.1	0.3	588	0.5	0.0	28.0	29	40.9	0.1
2/26/10 3:00	3.0	874	5.6	0.3	2.8	781	5.2	0.2	5.3	702	9.9	0.4	0.3	584	0.5	0.0	25.0	29	36.3	0.1
2/26/10 3:30	1.6	866	2.9	0.1	2.6	775	4.8	0.2	1.5	699	2.7	0.1	0.3	584	0.5	0.0	32.0	29	47.2	0.1
2/26/10 4:00	2.3	859	4.2	0.2	3.0	770	5.6	0.2	2.2	696	4.0	0.2	0.3	584	0.5	0.0	49.0	29	74.2	0.1
2/26/10 4:30	1.6	866	2.9	0.1	2.7	772	5.0	0.2	3.0	693	5.6	0.2	0.3	575	0.5	0.0	38.0	28	56.6	0.1
2/26/10 5:00	1.6	859	2.9	0.1	3.3	767	6.1	0.3	1.7	690	3.1	0.1	0.2	575	0.4	0.0	28.0	28	40.9	0.1
2/26/10 5:30	1.6	859	2.9	0.1	3.4	767	6.3	0.3	1.4	690	2.6	0.1	0.4	575	0.7	0.0	33.0	28	48.7	0.1
2/26/10 6:00	2.6	851	4.8	0.2	3.7	759	6.9	0.3	1.4	682	2.6	0.1	0.4	565	0.7	0.0	41.0	28	61.4	0.1
2/26/10 6:30	1.9	859	3.5	0.2	2.9	764	5.4	0.2	1.8	685	3.3	0.1	0.2	565	0.4	0.0	65.0	28	100.1	0.2
2/26/10 7:00	1.8	836	3.3	0.2	3.1	750	5.7	0.2	2.8	678	5.2	0.2	0.4	570	0.7	0.0	44.0	28	66.2	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/26/10 7:30	1.5	851	2.7	0.1	2.8	759	5.2	0.2	1.2	682	2.2	0.1	0.3	565	0.5	0.0	30.0	28	44.0	0.1
2/26/10 8:00	1.8	836	3.3	0.2	3.5	750	6.5	0.3	1.4	678	2.6	0.1	0.3	570	0.5	0.0	30.0	28	44.0	0.1
2/26/10 8:30	1.6	843	2.9	0.1	3.1	754	5.7	0.2	1.4	678	2.6	0.1	0.3	565	0.5	0.0	37.0	28	55.0	0.1
2/26/10 9:00	1.6	836	2.9	0.1	3.0	749	5.6	0.2	1.7	675	3.1	0.1	0.4	565	0.7	0.0	24.0	28	34.8	0.1
2/26/10 9:30	1.9	836	3.5	0.2	3.2	747	5.9	0.2	2.0	673	3.7	0.1	0.3	561	0.5	0.0	31.0	28	45.6	0.1
2/26/10 10:00	2.0	836	3.7	0.2	3.1	747	5.7	0.2	1.7	673	3.1	0.1	0.6	561	1.1	0.0	34.0	28	50.3	0.1
2/26/10 10:30	2.2	821	4.0	0.2	3.4	739	6.3	0.3	1.2	669	2.2	0.1	0.2	565	0.4	0.0	25.0	28	36.3	0.1
2/26/10 11:00	2.1	828	3.9	0.2	3.1	742	5.7	0.2	1.2	670	2.2	0.1	0.3	561	0.5	0.0	25.0	28	36.3	0.1
2/26/10 11:30	1.8	828	3.3	0.2	3.2	744	5.9	0.2	1.3	672	2.4	0.1	0.3	565	0.5	0.0	27.0	28	39.4	0.1
2/26/10 12:00	2.5	828	4.6	0.2	2.9	742	5.4	0.2	1.0	670	1.8	0.1	0.2	561	0.4	0.0	30.0	28	44.0	0.1
2/26/10 12:30	1.5	828	2.7	0.1	2.8	739	5.2	0.2	1.2	664	2.2	0.1	0.4	552	0.7	0.0	50.0	27	75.8	0.1
2/26/10 13:00	2.4	821	4.4	0.2	2.9	736	5.4	0.2	1.2	664	2.2	0.1	0.3	556	0.5	0.0	31.0	27	45.6	0.1
2/26/10 13:30	1.8	821	3.3	0.2	2.9	736	5.4	0.2	1.0	664	1.8	0.1	0.2	556	0.4	0.0	25.0	27	36.3	0.1
2/26/10 14:00	1.7	821	3.1	0.1	3.0	734	5.6	0.2	0.9	661	1.6	0.1	0.4	552	0.7	0.0	26.0	27	37.8	0.1
2/26/10 14:30	2.0	821	3.7	0.2	3.5	733	6.5	0.3	1.0	659	1.8	0.1	0.4	547	0.7	0.0	35.0	27	51.9	0.1
2/26/10 15:00	1.7	799	3.1	0.1	2.6	719	4.8	0.2	1.2	652	2.2	0.1	0.3	552	0.5	0.0	95.0	27	149.8	0.2
2/26/10 15:30	1.9	806	3.5	0.2	3.0	723	5.6	0.2	1.3	653	2.4	0.1	0.2	552	0.4	0.0	31.0	27	45.6	0.1
2/26/10 16:00	1.9	813	3.5	0.2	2.8	729	5.2	0.2	1.0	658	1.8	0.1	0.4	552	0.7	0.0	40.0	27	59.8	0.1
2/26/10 16:30	1.8	806	3.3	0.1	2.8	723	5.2	0.2	0.9	653	1.6	0.1	0.3	547	0.5	0.0	26.0	27	37.8	0.1
2/26/10 17:00	1.7	806	3.1	0.1	2.9	724	5.4	0.2	0.9	655	1.6	0.1	0.4	552	0.7	0.0	18.0	27	25.6	0.0
2/26/10 17:30	1.7	813	3.1	0.1	2.7	731	5.0	0.2	1.9	661	3.5	0.1	0.3	556	0.5	0.0	21.0	27	30.2	0.0
2/26/10 18:00	2.0	806	3.7	0.2	2.7	724	5.0	0.2	1.8	655	3.3	0.1	0.3	552	0.5	0.0	38.0	27	56.6	0.1
2/26/10 18:30	1.6	791	2.9	0.1	2.9	716	5.4	0.2	1.5	652	2.7	0.1	0.3	556	0.5	0.0	61.0	27	93.6	0.1
2/26/10 19:00	1.5	791	2.7	0.1	2.9	716	5.4	0.2	2.2	652	4.0	0.1	0.3	556	0.5	0.0	96.0	27	151.5	0.2
2/26/10 19:30	1.9	799	3.5	0.2	3.6	722	6.7	0.3	1.4	658	2.6	0.1	0.3	561	0.5	0.0	33.0	28	48.7	0.1
2/26/10 20:00	1.9	799	3.5	0.2	3.1	722	5.7	0.2	1.7	658	3.1	0.1	0.2	561	0.4	0.0	23.0	28	33.2	0.1
2/26/10 20:30	1.4	806	2.6	0.1	3.3	731	6.1	0.3	1.7	669	3.1	0.1	0.2	575	0.4	0.0	21.0	28	30.2	0.0
2/26/10 21:00	1.4	799	2.6	0.1	2.9	729	5.4	0.2	1.5	671	2.7	0.1	0.3	584	0.5	0.0	18.0	29	25.6	0.0
2/26/10 21:30	2.0	791	3.7	0.2	2.6	724	4.8	0.2	2.6	668	4.8	0.2	0.4	584	0.7	0.0	18.0	29	25.6	0.0
2/26/10 22:00	1.5	799	2.7	0.1	3.0	732	5.6	0.2	2.2	677	4.0	0.2	0.4	593	0.7	0.0	18.0	29	25.6	0.0
2/26/10 22:30	1.6	806	2.9	0.1	3.2	737	5.9	0.2	1.2	680	2.2	0.1	0.3	593	0.5	0.0	31.0	29	45.6	0.1
2/26/10 23:00	1.5	806	2.7	0.1	3.7	739	6.9	0.3	0.9	682	1.6	0.1	0.3	598	0.5	0.0	71.0	29	110.0	0.2
2/26/10 23:30	1.6	813	2.9	0.1	3.6	745	6.7	0.3	1.0	688	1.8	0.1	0.2	602	0.4	0.0	92.0	30	144.8	0.2
2/27/10 0:00	2.4	813	4.4	0.2	3.1	745	5.7	0.2	0.7	688	1.3	0.0	0.3	602	0.5	0.0	37.0	30	55.0	0.1
2/27/10 0:30	2.1	813	3.9	0.2	3.1	745	5.7	0.2	1.8	688	3.3	0.1	0.3	602	0.5	0.0	21.0	30	30.2	0.1
2/27/10 1:00	2.0	828	3.7	0.2	2.8	756	5.2	0.2	1.0	694	1.8	0.1	0.3	602	0.5	0.0	20.0	30	28.6	0.0
2/27/10 1:30	1.4	828	2.6	0.1	3.4	757	6.3	0.3	1.8	697	3.3	0.1	0.3	607	0.5	0.0	20.0	30	28.6	0.0
2/27/10 2:00	2.0	821	3.7	0.2	2.9	751	5.4	0.2	2.8	691	5.2	0.2	0.3	602	0.5	0.0	17.0	30	24.1	0.0
2/27/10 2:30	1.3	828	2.4	0.1	3.0	754	5.6	0.2	1.9	692	3.5	0.1	0.6	598	1.1	0.0	14.0	29	19.6	0.0
2/27/10 3:00	1.5	828	2.7	0.1	3.2	754	5.9	0.3	1.4	692	2.6	0.1	0.4	598	0.7	0.0	15.0	29	21.1	0.0
2/27/10 3:30	2.5	828	4.6	0.2	4.0	756	7.4	0.3	1.1	694	2.0	0.1	0.2	602	0.4	0.0	51.0	30	77.4	0.1
2/27/10 4:00	1.9	821	3.5	0.2	3.6	751	6.7	0.3	1.2	691	2.2	0.1	0.3	602	0.5	0.0	28.0	30	40.9	0.1

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/27/10 4:30	3.4	821	6.3	0.3	3.0	749	5.6	0.2	0.7	689	1.3	0.0	0.3	598	0.5	0.0	21.0	29	30.2	0.0
2/27/10 5:00	2.0	821	3.7	0.2	2.8	751	5.2	0.2	0.7	691	1.3	0.0	0.3	602	0.5	0.0	19.0	30	27.1	0.0
2/27/10 5:30	1.9	821	3.5	0.2	2.7	751	5.0	0.2	0.6	691	1.1	0.0	0.4	602	0.7	0.0	21.0	30	30.2	0.1
2/27/10 6:00	1.4	821	2.6	0.1	2.7	747	5.0	0.2	1.0	686	1.8	0.1	0.3	593	0.5	0.0	16.0	29	22.6	0.0
2/27/10 6:30	1.4	821	2.6	0.1	2.7	747	5.0	0.2	1.0	686	1.8	0.1	0.3	593	0.5	0.0	18.0	29	25.6	0.0
2/27/10 7:00	2.4	821	4.4	0.2	2.8	747	5.2	0.2	0.9	686	1.6	0.1	0.4	593	0.7	0.0	17.0	29	24.1	0.0
2/27/10 7:30	1.9	813	3.5	0.2	3.0	741	5.6	0.2	1.4	680	2.6	0.1	0.3	588	0.5	0.0	17.0	29	24.1	0.0
2/27/10 8:00	2.0	813	3.7	0.2	2.6	741	4.8	0.2	0.8	680	1.4	0.1	0.5	588	0.9	0.0	19.0	29	27.1	0.0
2/27/10 8:30	2.4	813	4.4	0.2	2.7	739	5.0	0.2	1.7	677	3.1	0.1	0.3	584	0.5	0.0	17.0	29	24.1	0.0
2/27/10 9:00	1.8	813	3.3	0.2	3.2	738	5.9	0.2	0.7	674	1.3	0.0	0.3	579	0.5	0.0	15.0	29	21.1	0.0
2/27/10 9:30	1.5	813	2.7	0.1	2.3	738	4.2	0.2	1.2	674	2.2	0.1	0.8	579	1.4	0.0	13.0	29	18.1	0.0
2/27/10 10:00	1.5	813	2.7	0.1	2.5	736	4.6	0.2	0.6	672	1.1	0.0	0.4	575	0.7	0.0	13.0	28	18.1	0.0
2/27/10 10:30	1.2	799	2.2	0.1	2.5	728	4.6	0.2	0.8	668	1.4	0.1	0.2	579	0.4	0.0	11.0	29	15.2	0.0
2/27/10 11:00	1.3	799	2.4	0.1	2.4	725	4.4	0.2	1.0	663	1.8	0.1	0.3	570	0.5	0.0	14.0	28	19.6	0.0
2/27/10 11:30	1.2	799	2.2	0.1	2.3	726	4.2	0.2	0.6	666	1.1	0.0	0.3	575	0.5	0.0	13.0	28	18.1	0.0
2/27/10 12:00	1.2	791	2.2	0.1	2.2	720	4.0	0.2	0.6	660	1.1	0.0	0.3	570	0.5	0.0	10.0	28	13.7	0.0
2/27/10 12:30	1.3	799	2.4	0.1	2.6	724	4.8	0.2	0.9	660	1.6	0.1	0.3	565	0.5	0.0	12.0	28	16.6	0.0
2/27/10 13:00	2.0	799	3.7	0.2	2.2	722	4.0	0.2	0.7	658	1.3	0.0	0.3	561	0.5	0.0	13.0	28	18.1	0.0
2/27/10 13:30	1.4	799	2.6	0.1	2.5	722	4.6	0.2	1.5	658	2.7	0.1	0.5	568	0.9	0.0	16.0	28	22.6	0.0
2/27/10 14:00	1.1	784	2.0	0.1	2.4	711	4.4	0.2	0.4	649	0.7	0.0	0.3	556	0.5	0.0	12.0	27	16.6	0.0
2/27/10 14:30	1.1	784	2.0	0.1	2.3	709	4.2	0.2	0.4	646	0.7	0.0	0.3	552	0.5	0.0	12.0	27	16.6	0.0
2/27/10 15:00	1.1	784	2.0	0.1	2.5	711	4.6	0.2	0.5	649	0.9	0.0	0.3	556	0.5	0.0	11.0	27	15.2	0.0
2/27/10 15:30	1.2	770	2.2	0.1	2.2	700	4.0	0.2	0.4	640	0.7	0.0	0.2	552	0.4	0.0	12.0	27	16.6	0.0
2/27/10 16:00	1.2	777	2.2	0.1	2.3	703	4.2	0.2	0.5	641	0.9	0.0	0.4	547	0.7	0.0	12.0	27	16.6	0.0
2/27/10 16:30	1.1	777	2.0	0.1	2.7	702	5.0	0.2	0.6	638	1.1	0.0	0.3	543	0.5	0.0	12.0	27	16.6	0.0
2/27/10 17:00	1.4	777	2.6	0.1	3.1	700	5.7	0.2	0.7	635	1.3	0.0	0.3	539	0.5	0.0	10.0	27	13.7	0.0
2/27/10 17:30	1.1	762	2.0	0.1	2.4	692	4.4	0.2	0.6	632	1.1	0.0	0.3	543	0.5	0.0	10.0	27	13.7	0.0
2/27/10 18:00	1.3	762	2.4	0.1	2.3	692	4.2	0.2	0.6	632	1.1	0.0	0.3	543	0.5	0.0	12.0	27	16.6	0.0
2/27/10 18:30	1.0	762	1.8	0.1	2.3	689	4.2	0.2	0.5	627	0.9	0.0	0.5	534	0.9	0.0	9.8	26	13.4	0.0
2/27/10 19:00	1.3	762	2.4	0.1	2.4	688	4.4	0.2	0.7	624	1.3	0.0	0.3	530	0.5	0.0	9.8	26	13.4	0.0
2/27/10 19:30	1.2	762	2.2	0.1	2.5	688	4.6	0.2	0.7	624	1.3	0.0	0.2	530	0.4	0.0	11.0	26	15.2	0.0
2/27/10 20:00	1.1	748	2.0	0.1	2.5	675	4.6	0.2	1.4	613	2.6	0.1	0.2	521	0.4	0.0	11.0	26	15.2	0.0
2/27/10 20:30	1.4	748	2.6	0.1	2.4	677	4.4	0.2	0.7	616	1.3	0.0	0.3	525	0.5	0.0	12.0	26	16.6	0.0
2/27/10 21:00	1.1	748	2.0	0.1	2.5	672	4.6	0.2	0.7	608	1.3	0.0	0.3	512	0.5	0.0	12.0	25	16.6	0.0
2/27/10 21:30	0.9	748	1.6	0.1	2.4	674	4.4	0.2	0.3	611	0.5	0.0	0.2	517	0.4	0.0	9.8	26	13.4	0.0
2/27/10 22:00	1.4	741	2.6	0.1	3.3	668	6.1	0.2	0.7	606	1.3	0.0	0.3	512	0.5	0.0	11.0	25	15.2	0.0
2/27/10 22:30	1.0	741	1.8	0.1	2.3	668	4.2	0.2	1.3	606	2.4	0.1	0.2	512	0.4	0.0	12.0	25	16.6	0.0
2/27/10 23:00	1.3	734	2.4	0.1	2.5	663	4.6	0.2	0.6	603	1.1	0.0	0.2	512	0.4	0.0	11.0	25	15.2	0.0
2/27/10 23:30	1.5	727	2.7	0.1	2.3	657	4.2	0.2	0.6	597	1.1	0.0	0.3	508	0.5	0.0	10.0	25	13.7	0.0
2/28/10 0:00	0.9	727	1.6	0.1	2.3	654	4.2	0.2	0.5	592	0.9	0.0	0.3	500	0.5	0.0	12.0	25	16.6	0.0
2/28/10 0:30	1.3	727	2.4	0.1	2.3	654	4.2	0.2	0.5	592	0.9	0.0	0.2	500	0.4	0.0	12.0	25	16.6	0.0
2/28/10 1:00	1.1	720	2.0	0.1	2.5	649	4.6	0.2	0.6	589	1.1	0.0	0.2	500	0.4	0.0	12.0	25	16.6	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)	Turbidity (FNU)	Streamflow (ft ³ /s)	SSC (mg/L)	SSL (T)
2/28/10 1:30	0.9	720	1.6	0.1	2.4	647	4.4	0.2	0.5	584	0.9	0.0	0.3	491	0.5	0.0	11.0	24	15.2	0.0
2/28/10 2:00	0.9	720	1.6	0.1	2.3	647	4.2	0.2	0.4	584	0.7	0.0	0.3	491	0.5	0.0	9.6	24	13.1	0.0
2/28/10 2:30	1.6	720	2.9	0.1	2.2	647	4.0	0.1	0.7	584	1.3	0.0	0.3	491	0.5	0.0	9.4	24	12.8	0.0
2/28/10 3:00	1.9	707	3.5	0.1	2.5	637	4.6	0.2	0.4	579	0.7	0.0	2.8	491	5.2	0.1	11.0	24	15.2	0.0
2/28/10 3:30	1.4	707	2.6	0.1	2.9	636	5.4	0.2	0.6	576	1.1	0.0	0.3	487	0.5	0.0	9.9	24	13.6	0.0
2/28/10 4:00	1.2	700	2.2	0.1	2.2	630	4.0	0.1	0.3	571	0.5	0.0	0.3	483	0.5	0.0	9.6	24	13.1	0.0
2/28/10 4:30	1.0	707	1.8	0.1	2.3	635	4.2	0.2	0.5	574	0.9	0.0	0.5	483	0.9	0.0	9.5	24	13.0	0.0
2/28/10 5:00	1.1	693	2.0	0.1	2.2	624	4.0	0.1	0.5	566	0.9	0.0	0.7	479	1.3	0.0	9.1	24	12.4	0.0
2/28/10 5:30	1.0	700	1.8	0.1	3.5	629	6.5	0.2	0.4	569	0.7	0.0	0.3	479	0.5	0.0	9.9	24	13.6	0.0
2/28/10 6:00	1.2	700	2.2	0.1	2.3	629	4.2	0.1	0.4	569	0.7	0.0	0.3	479	0.5	0.0	9.9	24	13.6	0.0
2/28/10 6:30	2.1	686	3.9	0.1	1.5	618	2.7	0.1	0.4	561	0.7	0.0	0.2	475	0.4	0.0	8.5	24	11.5	0.0
2/28/10 7:00	0.9	686	1.6	0.1	2.0	617	3.7	0.1	0.4	558	0.7	0.0	0.2	471	0.4	0.0	9.7	23	13.3	0.0
2/28/10 7:30	1.0	686	1.8	0.1	1.8	617	3.3	0.1	0.9	558	1.6	0.1	0.2	471	0.4	0.0	8.2	23	11.1	0.0
2/28/10 8:00	2.7	680	5.0	0.2	1.8	611	3.3	0.1	0.7	553	1.3	0.0	0.3	467	0.5	0.0	10.0	23	13.7	0.0
2/28/10 8:30	2.0	680	3.7	0.1	1.8	610	3.3	0.1	0.4	551	0.7	0.0	0.3	462	0.5	0.0	10.0	23	13.7	0.0
2/28/10 9:00	1.6	673	2.9	0.1	1.5	605	2.7	0.1	0.4	548	0.7	0.0	0.2	462	0.4	0.0	8.1	23	11.0	0.0
2/28/10 9:30	1.2	673	2.2	0.1	1.5	604	2.7	0.1	0.4	546	0.7	0.0	0.2	458	0.4	0.0	7.6	23	10.2	0.0
2/28/10 10:00	0.9	667	1.6	0.1	1.6	600	2.9	0.1	0.4	543	0.7	0.0	0.3	458	0.5	0.0	8.3	23	11.3	0.0
2/28/10 10:30	0.9	667	1.6	0.1	1.7	598	3.1	0.1	0.5	541	0.9	0.0	0.4	454	0.7	0.0	7.3	23	9.8	0.0
2/28/10 11:00	0.9	667	1.6	0.1	1.5	598	2.7	0.1	0.4	541	0.7	0.0	0.3	454	0.5	0.0	7.6	23	10.2	0.0
2/28/10 11:30	1.0	667	1.8	0.1	1.7	598	3.1	0.1	0.5	541	0.9	0.0	0.3	454	0.5	0.0	7.1	23	9.5	0.0
2/28/10 12:00	1.1	667	2.0	0.1	1.8	597	3.3	0.1	0.4	538	0.7	0.0	0.8	450	1.4	0.0	8.6	23	11.7	0.0
2/28/10 12:30	0.8	653	1.4	0.1	1.5	587	2.7	0.1	0.4	531	0.7	0.0	0.3	447	0.5	0.0	8.2	22	11.1	0.0
2/28/10 13:00	1.1	660	2.0	0.1	1.7	590	3.1	0.1	0.3	531	0.5	0.0	0.3	443	0.5	0.0	9.1	22	12.4	0.0
2/28/10 13:30	1.0	653	1.8	0.1	1.7	586	3.1	0.1	0.5	528	0.9	0.0	0.2	443	0.4	0.0	7.6	22	10.2	0.0
2/28/10 14:00	0.9	653	1.6	0.1	1.7	584	3.1	0.1	0.5	526	0.9	0.0	0.3	439	0.5	0.0	8.0	22	10.8	0.0
2/28/10 14:30	0.7	647	1.3	0.0	1.4	580	2.6	0.1	0.6	523	1.1	0.0	0.3	439	0.5	0.0	7.9	22	10.7	0.0
2/28/10 15:00	0.8	647	1.4	0.1	1.9	580	3.5	0.1	0.3	523	0.5	0.0	0.2	439	0.4	0.0	7.7	22	10.4	0.0
2/28/10 15:30	1.1	641	2.0	0.1	1.7	576	3.1	0.1	1.9	521	3.5	0.1	0.2	439	0.4	0.0	8.2	22	11.1	0.0
2/28/10 16:00	1.4	647	2.6	0.1	1.7	579	3.1	0.1	0.4	521	0.7	0.0	0.3	435	0.5	0.0	7.9	22	10.7	0.0
2/28/10 16:30	0.8	641	1.4	0.1	1.5	573	2.7	0.1	0.4	516	0.7	0.0	0.3	431	0.5	0.0	7.3	22	9.8	0.0
2/28/10 17:00	0.9	641	1.6	0.1	2.2	573	4.0	0.1	0.3	516	0.5	0.0	0.3	431	0.5	0.0	8.3	22	11.3	0.0
2/28/10 17:30	1.2	635	2.2	0.1	1.5	568	2.7	0.1	0.4	512	0.7	0.0	0.2	427	0.4	0.0	7.2	21	9.7	0.0
2/28/10 18:00	0.8	629	1.4	0.1	1.5	563	2.7	0.1	0.3	507	0.5	0.0	0.3	423	0.5	0.0	8.0	21	10.8	0.0
2/28/10 18:30	0.9	635	1.6	0.1	1.4	565	2.6	0.1	0.6	507	1.1	0.0	0.4	419	0.7	0.0	7.2	21	9.7	0.0
2/28/10 19:00	0.7	629	1.3	0.0	2.3	560	4.2	0.1	0.4	502	0.7	0.0	0.3	416	0.5	0.0	7.9	21	10.7	0.0
2/28/10 19:30	0.9	629	1.6	0.1	1.8	561	3.3	0.1	0.4	505	0.7	0.0	0.3	419	0.5	0.0	8.4	21	11.4	0.0
2/28/10 20:00	0.9	629	1.6	0.1	2.2	561	4.0	0.1	0.4	505	0.7	0.0	0.3	419	0.5	0.0	7.8	21	10.5	0.0
2/28/10 20:30	1.3	623	2.4	0.1	1.8	556	3.3	0.1	0.4	500	0.7	0.0	0.4	416	0.7	0.0	9.1	21	12.4	0.0
2/28/10 21:00	1.0	623	1.8	0.1	1.6	555	2.9	0.1	0.7	498	1.3	0.0	0.2	412	0.4	0.0	7.9	21	10.7	0.0
2/28/10 21:30	1.0	617	1.8	0.1	1.4	550	2.6	0.1	0.4	493	0.7	0.0	0.2	408	0.4	0.0	8.3	21	11.3	0.0
2/28/10 22:00	1.0	611	1.8	0.1	1.5	546	2.7	0.1	0.3	491	0.5	0.0	0.3	408	0.5	0.0	9.1	21	12.4	0.0

Date & Time	Station 1				Station 2				Station 3				Station 4				Station 5			
	Turbidity	Streamflow	SSC	SSL	Turbidity	Streamflow	SSC	SSL	Turbidity	Streamflow	SSC	SSL	Turbidity	Streamflow	SSC	SSL	Turbidity	Streamflow	SSC	SSL
	(FNU)	(ft ³ /s)	(mg/L)	(T)	(FNU)	(ft ³ /s)	(mg/L)	(T)	(FNU)	(ft ³ /s)	(mg/L)	(T)	(FNU)	(ft ³ /s)	(mg/L)	(T)	(FNU)	(ft ³ /s)	(mg/L)	(T)
2/28/10 22:30	0.9	617	1.6	0.1	1.7	550	3.1	0.1	0.3	493	0.5	0.0	0.3	408	0.5	0.0	7.4	21	10.0	0.0
2/28/10 23:00	1.2	611	2.2	0.1	1.8	546	3.3	0.1	1.1	491	2.0	0.1	0.3	408	0.5	0.0	12.0	21	16.6	0.0
2/28/10 23:30	0.8	605	1.4	0.0	1.5	540	2.7	0.1	0.6	486	1.1	0.0	0.2	404	0.4	0.0	7.7	20	10.4	0.0
3/1/10 0:00	1.1	599	2.0	0.1	1.5	535	2.7	0.1	0.6	481	1.1	0.0	0.2	401	0.4	0.0	6.9	20	9.2	0.0
Totals			3302				2509				1838					312				907

B: GIS Data Set Metadata

B.1: Landslide Inventory

GIS data set available online:

http://water.usgs.gov/GIS/dsdl/LNsantiam_LandslideInventory_gdb.zip

Identification_Information:

Citation:

Citation_Information:

Originator: Steven Sobieszczyk

Publication_Date: 2010

Title: Landslide Deposit Boundaries for the Little North Santiam River Basin, Oregon

Geospatial_Data_Presentation_Form: vector digital data

Online_Linkage:

http://water.usgs.gov/lookup/getspatial?lnsantiam_LandslideInventory

Description:

Abstract:

This layer is an inventory of existing landslides deposits in the Little North Santiam River Basin, Oregon (2009). Each landslide deposit shown on this map has been classified according to a number of specific characteristics identified at the time recorded in the GIS database. The classification scheme was developed by the Oregon Department of Geology and Mineral Industries (Burns and Madin, 2009). Several significant landslide characteristics recorded in the database are portrayed with symbology on this map. The specific characteristics shown for each landslide are the activity of landsliding, landslide features, deep or shallow failure, type of landslide movement, and confidence of landslide interpretation. These landslide characteristics are determined primarily on the basis of geomorphic features, or landforms, observed for each landslide.

Data layers in this geodatabase include: landslide deposit boundaries (Deposits); field-verified location imagery (Photos); head scarp or scarp flanks (Scarp_Flanks); and secondary scarp features (Scarps). The geodatabase template was developed by the Oregon Department of Geology and Mineral Industries (Burns and Madin, 2009).

Purpose:

This data set is one of 4 feature data sets included in a basin-wide landslide inventory. The landslide inventory is one of the essential data layers used to delineate regional landslide susceptibility. This landslide inventory is not regulatory, and revisions can happen when new information regarding landslides is found or future (new) landslides occur. Therefore, it is possible that landslides within the map area were not identified or occurred after the map was prepared.

This landslide inventory is intended to provide users with basic information regarding landslides within the Little North Santiam River Basin. The geologic, terrain, and climatic conditions that led to slope failures in the past may provide clues to the locations and conditions of future slope failures, and it is intended that this map will provide useful information to develop regional landslide susceptibility maps, guide site-specific

investigations for future developments, assist in regional planning, and mitigation of existing landslides.

Supplemental_Information:

This work was completed as part of the Master's thesis "Using Turbidity Monitoring and LiDAR-Derived Imagery to Investigate Sources of Suspended Sediment in the Little North Santiam River Basin, Oregon, Winter 2009–2010" by Steven Sobieszczyk, Portland State University and U.S. Geological Survey.

Citations:

Burns, W.J., and Madin, I.P., 2009, Protocol for inventory mapping of landslide deposits from light detection and ranging (LIDAR) imagery: Oregon Department of Geology and Mineral Industries Special Paper 42, 30 p.

Oregon Department of Geology and Mineral Industries and Watershed Sciences, Inc., 2009, LiDAR of Western Oregon and the Willamette Valley: digital data set courtesy of Ian Madin, available via external hard drive [digital data set]

Oregon Department of Geology and Mineral Industries, 2009, Oregon geologic data compilation: digital data set courtesy of Bill Burns, will be available online at <http://ogdc.geos.pdx.edu/> [digital data set]

Time_Period_of_Content:

Time_Period_Information:

Single_Date/Time:

Calendar_Date: 2009

Currentness_Reference: ground condition

Status:

Progress: Complete

Maintenance_and_Update_Frequency: None planned

Spatial_Domain:

Bounding_Coordinates:

West_Bounding_Coordinate: -122.583361

East_Bounding_Coordinate: -122.135924

North_Bounding_Coordinate: 44.899782

South_Bounding_Coordinate: 44.776577

Keywords:

Theme:

Theme_Keyword_Thesaurus: None

Theme_Keyword: deposits

Theme_Keyword: landslide

Theme_Keyword: inventory

Place:

Place_Keyword_Thesaurus: None

Place_Keyword: Little North Santiam River Basin

Place_Keyword: Elkhorn

Place_Keyword: Elkhorn Valley

Place_Keyword: Marion County

Place_Keyword: Oregon

Temporal:
 Temporal_Keyword_Thesaurus: None
 Temporal_Keyword: 2009
 Temporal_Keyword: 2010
 Access_Constraints: None
 Use_Constraints:
 None

The U.S. Geological Survey should be acknowledged as the data source in products derived from these data.

Point_of_Contact:
 Contact_Information:
 Contact_Person_Primary:
 Contact_Person: Steven Sobieszczyk
 Contact_Organization: U.S. Geological Survey
 Contact_Position: Hydrologist
 Contact_Address:
 Address_Type: mailing and physical address
 Address: 2130 SW 5th Ave.
 City: Portland
 State_or_Province: OR
 Postal_Code: 97201
 Country: USA
 Contact_Voice_Telephone: 503-251-3208
 Contact_Facsimile_Telephone: 503-251-3470
 Contact_Electronic_Mail_Address: ssobie@usgs.gov

Contact_Instructions: Warning: Although accurate at the time of production, this information may have become obsolete. See the Metadata_Reference_Information section for a current contact.

Browse_Graphic:
 Browse_Graphic_File_Name:
http://water.usgs.gov/GIS/browse/LNsantiam_LandslideInventory.jpeg
 Browse_Graphic_File_Description: Illustration of data set.
 Browse_Graphic_File_Type: JPEG
 Native_Data_Set_Environment: Microsoft Windows XP Version 5.1 (Build 2600)
 Service Pack 3; ESRI ArcCatalog 9.3.1.3000

Cross_Reference:
 Citation_Information:
 Originator: Steven Sobieszczyk
 Publication_Date: 2010
 Title: Head Scarp Boundary for the Landslides in the Little North Santiam River Basin, Oregon

Geospatial_Data_Presentation_Form: vector digital data
 Online_Linkage:
http://water.usgs.gov/lookup/getspatial?LNsantiam_LandslideInventory.gdb

Cross_Reference:
 Citation_Information:

Originator: Steven Sobieszczyk
 Publication_Date: 2010
 Title: Top of Head Scarp and Internal Scarps for Landslide Deposits in the Little North Santiam River Basin, Oregon
 Geospatial_Data_Presentation_Form: vector digital data
 Online_Linkage:
http://water.usgs.gov/lookup/getspatial?LNsantiam_LandslideInventory.gdb
 Cross_Reference:
 Citation_Information:
 Originator: Steven Sobieszczyk
 Publication_Date: 2010
 Title: Location of Photographs Showing Landslide Features in the Little North Santiam River Basin, Oregon
 Geospatial_Data_Presentation_Form: vector digital data
 Online_Linkage:
http://water.usgs.gov/lookup/getspatial?LNsantiam_LandslideInventory.gdb
 Data_Quality_Information:
 Attribute_Accuracy:
 Attribute_Accuracy_Report:
 Deposits represent feature conditions mapped from LiDAR data obtained during flights in summer 2009.

CONFIDENCE OF INTERPRETATION: Each landslide should be classified according to a "confidence" that the mapper assigns based on the likelihood that the landslide actually exists. Landslides are mapped on the basis of characteristic morphology, and the confidence of the interpretation is based on the visual strength of the morphologies. As a landslide ages, after its most recent movement, weathering (primarily through erosion) degrades the morphologies produced by landsliding. With time, landslide morphologies may become so subtle that they resemble morphologies produced by geologic processes and conditions unrelated to landsliding.

Some landslides have several different types of morphologies associated with them. A good way to define certainty is through a simple point system associated with these features. The point system used is based on a ranking of four primary landslide features with a ranking of 0 to 10 points per feature. For example, if during mapping, the head scarp and toe of a landslide were identifiable and had very strong visual strength, the mapper would apply 10 points for the head scarp and 10 points for the toe equaling 20 points, which would be associated with a moderate certainty of identification.

Logical Consistency_Report: Locations were quality-assured by both DOGAMI and USGS personnel for accuracy, completeness, and logical consistency. Snapping and polygon tracing was set during digitizing to avoid overlap.

Completeness_Report: Data are complete.

Positional_Accuracy:

Horizontal_Positional_Accuracy:

Horizontal_Positional_Accuracy_Report: 3 feet

Vertical_Positional_Accuracy:

Vertical_Positional_Accuracy_Report: 6 inches

Lineage:

Source_Information:
 Source_Citation:
 Citation_Information:
 Originator: Burns, W.J., and Madin, I.P.
 Publication_Date: 2009
 Title: Protocol for Inventory Mapping of Landslide Deposits from Light Detection and Ranging (Lidar) Imagery
 Geospatial_Data_Presentation_Form: document
 Series_Information:
 Series_Name: Special Paper
 Issue_Identification: 42
 Publication_Information:
 Publication_Place: Portland
 Publisher: Oregon Department of Geology and Mineral Industries
 Type_of_Source_Media: paper
 Source_Time_Period_of_Content:
 Time_Period_Information:
 Single_Date/Time:
 Calendar_Date: 2009
 Source_Currentness_Reference: publication date
 Source_Citation_Abbreviation: SP42
 Source_Contribution: Burns, W.J., and Madin, I.P., 2009, Protocol for inventory mapping of landslide deposits from light detection and ranging (LIDAR) imagery: Oregon Department of Geology and Mineral Industries Special Paper 42, 30 p.

Source_Information:
 Source_Citation:
 Citation_Information:
 Originator: Oregon Department of Geology and Mineral Industries
 Publication_Date: 2009
 Title: Oregon Geologic Data Compilation
 Edition: 5
 Geospatial_Data_Presentation_Form: vector digital data
 Online_Linkage: <http://ogdc.geos.pdx.edu/>
 Type_of_Source_Media: online
 Source_Time_Period_of_Content:
 Time_Period_Information:
 Single_Date/Time:
 Calendar_Date: 2009
 Source_Currentness_Reference: publication date
 Source_Citation_Abbreviation: DOGAMI GEO
 Source_Contribution: Oregon Department of Geology and Mineral Industries, 2009b, Oregon geologic data compilation: digital data set courtesy of Bill Burns, will be available online at <http://ogdc.geos.pdx.edu/> [digital data set]

Source_Information:
 Source_Citation:
 Citation_Information:

Originator: Oregon Department of Geology and Mineral Industries and Watershed Sciences, Inc.

Publication_Date: 2009

Title: LiDAR of Western Oregon and the Willamette Valley

Geospatial_Data_Presentation_Form: raster digital data

Online_Linkage: <http://www.oregongeology.org/sub/projects/olc/default.htm>

Type_of_Source_Media: hard drive

Source_Time_Period_of_Content:

Time_Period_Information:

Single_Date/Time:

Calendar_Date: 2009

Source_Currentness_Reference: ground condition

Source_Citation_Abbreviation: LiDAR

Source_Contribution: Oregon Department of Geology and Mineral Industries and Watershed Sciences, Inc., 2009, LiDAR of Western Oregon and the Willamette Valley: digital data set courtesy of Ian Madin, available via external hard drive [digital data set]

Process_Step:

Process_Description: Acquired 3ft-resolution Light Detection and Ranging (LiDAR) data

Source_Used_Citation_Abbreviation: LiDAR

Process_Date: 2010

Process_Contact:

Contact_Information:

Contact_Person_Primary:

Contact_Person: Steven Sobieszczyk

Contact_Organization: U.S. Geological Survey

Contact_Position: Hydrologist

Contact_Address:

Address_Type: mailing and physical address

Address: 2130 SW 5th Ave.

City: Portland

State_or_Province: OR

Postal_Code: 97201

Country: USA

Contact_Voice_Telephone: (503) 251-3208

Contact_Facsimile_Telephone: (503) 251-3470

Contact_Electronic_Mail_Address: ssobie@usgs.gov

Process_Step:

Process_Description:

Converted LiDAR digital elevation model (DEM) into a slope raster using Spatial Analyst extension in ArcGIS 9.3.

Source_Used_Citation_Abbreviation: LiDAR

Process_Date: 2010

Process_Contact:

Contact_Information:

Contact_Person_Primary:

Contact_Person: Steven Sobieszczyk

Contact_Organization: U.S. Geological Survey
 Contact_Position: Hydrologist
 Contact_Address:
 Address_Type: mailing and physical address
 Address: 2130 SW 5th Ave.
 City: Portland
 State_or_Province: OR
 Postal_Code: 97201
 Country: USA
 Contact_Voice_Telephone: (503) 251-3208
 Contact_Facsimile_Telephone: (503) 251-3470
 Contact_Electronic_Mail_Address: ssobie@usgs.gov

Process_Step:

Process_Description:

Used slopeshade (slope raster: stretched, standard deviation 5, "black and white" inverted color) map and 60% transparent DEM as backdrop for identifying landslide deposits. Generated contour lines, as well.

Process_Date: 2010

Process_Contact:

Contact_Information:

Contact_Person_Primary:

Contact_Person: Steven Sobieszczyk
 Contact_Organization: U.S. Geological Survey
 Contact_Position: Hydrologist
 Contact_Address:
 Address_Type: mailing and physical address
 Address: 2130 SW 5th Ave.
 City: Portland
 State_or_Province: OR
 Postal_Code: 97201
 Country: USA
 Contact_Voice_Telephone: (503) 251-3208
 Contact_Facsimile_Telephone: (503) 251-3470
 Contact_Electronic_Mail_Address: ssobie@usgs.gov

Process_Step:

Process_Description:

Manually digitized landslide features using methods defined in Special Paper 42 (Burns and Madin, 2009).

"The method employed to identify landslide areas in this study uses two kinds of data: 1) spatial data and 2) tabular data. Spatial data are data that can be mapped as points, lines, or polygons. Tabular data are descriptive data, usually in text or numeric form, stored in rows and columns in a database and linked to spatial data. To facilitate data collection, a geodatabase template was developed as part of this protocol. The template includes empty feature classes for deposits, scarp flanks, scarps, and photos. The geodatabase includes relationship classes between the feature classes. The template includes all fields for the tabular data, located in the Deposits feature class. Individual

mappers who use this template can then easily transfer their data into a master geodatabase."

Source_Used_Citation_Abbreviation: SP42

Source_Used_Citation_Abbreviation: DOGAMI GEO

Process_Date: 2010

Process_Contact:

Contact_Information:

Contact_Person_Primary:

Contact_Person: Steven Sobieszczyk

Contact_Organization: U.S. Geological Survey

Contact_Position: Hydrologist

Contact_Address:

Address_Type: mailing and physical address

Address: 2130 SW 5th Ave.

City: Portland

State_or_Province: OR

Postal_Code: 97201

Country: USA

Contact_Voice_Telephone: (503) 251-3208

Contact_Facsimile_Telephone: (503) 251-3470

Contact_Electronic_Mail_Address: ssobie@usgs.gov

Spatial_Data_Organization_Information:

Direct_Spatial_Reference_Method: Vector

Point_and_Vector_Object_Information:

SDTS_Terms_Description:

SDTS_Point_and_Vector_Object_Type: G-polygon

Point_and_Vector_Object_Count: 401

Spatial_Reference_Information:

Horizontal_Coordinate_System_Definition:

Planar:

Map_Projection:

Map_Projection_Name: Lambert Conformal Conic

Lambert_Conformal_Conic:

Standard_Parallel: 43.000000

Standard_Parallel: 45.500000

Longitude_of_Central_Meridian: -120.500000

Latitude_of_Projection-Origin: 41.750000

False_Easting: 1312335.958005

False_Northing: 0.000000

Planar_Coordinate_Information:

Planar_Coordinate_Encoding_Method: coordinate pair

Coordinate_Representation:

Abscissa_Resolution: 0.000328

Ordinate_Resolution: 0.000328

Planar_Distance_Units: international feet

Geodetic_Model:

Horizontal_Datum_Name: D_North_American_1983_HARN

Ellipsoid_Name: Geodetic Reference System 80
 Semi-major_Axis: 6378137.000000
 Denominator_of_Flattening_Ratio: 298.257222
 Vertical_Coordinate_System_Definition:
 Altitude_System_Definition:
 Altitude_Datum_Name: North American Vertical Datum of 1988
 Altitude_Resolution: 0.000100
 Altitude_Distance_Units: feet
 Altitude_Encoding_Method: Explicit elevation coordinate included with horizontal coordinates
 Entity_and_Attribute_Information:
 Detailed_Description:
 Entity_Type:
 Entity_Type_Label: Deposits
 Entity_Type_Definition: Polygonal scarp features identified with landslide deposits. Includes head scarp and flank scarps
 Entity_Type_Definition_Source: U.S. Geological Survey
 Attribute:
 Attribute_Label: OBJECTID
 Attribute_Definition: Internal feature number.
 Attribute_Definition_Source: ESRI
 Attribute_Domain_Values:
 Unrepresentable_Domain: Sequential unique whole numbers that are automatically generated.
 Attribute:
 Attribute_Label: SHAPE
 Attribute_Definition: Feature geometry.
 Attribute_Definition_Source: ESRI
 Attribute_Domain_Values:
 Unrepresentable_Domain: Coordinates defining the features.
 Attribute:
 Attribute_Label: UNIQUE_ID
 Attribute_Definition: Unique ID that relates scarp to mapped landslide deposit.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Unrepresentable_Domain: Coordinates defining the features.
 Attribute:
 Attribute_Label: TYPE_MOVE
 Attribute_Definition: Type of landslide movement.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Fall
 Enumerated_Domain_Value_Definition: Fall
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute_Domain_Values:
 Enumerated_Domain:

Enumerated_Domain_Value: Slide
 Enumerated_Domain_Value_Definition: Slide
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Spread
 Enumerated_Domain_Value_Definition: Spread
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Flow
 Enumerated_Domain_Value_Definition: Flow
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Complex
 Enumerated_Domain_Value_Definition: Complex
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute:
 Attribute_Label: MOVE_CLASS
 Attribute_Definition: Classification of landslide movement.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Earth Flow
 Enumerated_Domain_Value_Definition: Composition = earth, movement = flow
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Debris Flow
 Enumerated_Domain_Value_Definition: Composition = debris, movement = flow
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Rock Fall
 Enumerated_Domain_Value_Definition: Composition = rock, movement = fall
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Earth Slide - Rotational
 Enumerated_Domain_Value_Definition: Composition = earth, movement =
 slide/rotational
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Earth Slide - Translational

Enumerated_Domain_Value_Definition: Composition = earth, movement = slide/translational

Enumerated_Domain_Value_Definition_Source: SP42

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: Complex

Enumerated_Domain_Value_Definition: Composition = multiple, movement = multiple

Enumerated_Domain_Value_Definition_Source: SP42

Attribute:

Attribute_Label: MOVE_CODE

Attribute_Definition: Abbreviated code for landslide movement type.

Attribute_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: RF

Enumerated_Domain_Value_Definition: Rock Fall

Enumerated_Domain_Value_Definition_Source: SP42

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: EFL

Enumerated_Domain_Value_Definition: Earth Flow

Enumerated_Domain_Value_Definition_Source: SP42

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: DFL

Enumerated_Domain_Value_Definition: Debris Flow

Enumerated_Domain_Value_Definition_Source: SP42

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: ES-R

Enumerated_Domain_Value_Definition: Earth Slide - Rotational

Enumerated_Domain_Value_Definition_Source: SP42

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: ES-T

Enumerated_Domain_Value_Definition: Earth Slide - Translational

Enumerated_Domain_Value_Definition_Source: SP42

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: C

Enumerated_Domain_Value_Definition: Complex

Enumerated_Domain_Value_Definition_Source: SP42

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: C-EFL

Enumerated_Domain_Value_Definition: Complex - Earth Flow

Enumerated_Domain_Value_Definition_Source: SP42

Attribute:

Attribute_Label: GlobalID

Attribute_Definition: ID used in Landslide Inventory geodatabase.

Attribute_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Unrepresentable_Domain: Coordinates defining the features.

Attribute:

Attribute_Label: CONFIDENCE

Attribute_Definition: Mapping confidence of landslide deposit delineation.

Attribute_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: high

Enumerated_Domain_Value_Definition: > 30 points; where: "The point system in this protocol is based on a ranking of four primary landslide features with 0 to 10 points per feature, with zero points for an unidentifiable feature and 10 points for a very clearly identifiable feature. For example, if the head scarp and toe of a landslide were clearly identifiable in the lidar DEM, the mapper would apply 10 points for the head scarp and 10 points for the toe, equaling 20 points, which would be associated with a moderate certainty of identification."

Enumerated_Domain_Value_Definition_Source: SP42

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: moderate

Enumerated_Domain_Value_Definition: 11-29 points

Enumerated_Domain_Value_Definition_Source: SP42

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: low

Enumerated_Domain_Value_Definition: <= 10 points

Enumerated_Domain_Value_Definition_Source: SP42

Attribute:

Attribute_Label: DATE_MOVE

Attribute_Definition: Date of last movement.

Attribute_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Range_Domain:

Range_Domain_Minimum: 2009

Range_Domain_Maximum: 2010

Attribute:

Attribute_Label: NAME

Attribute_Definition: Landslide name.

Attribute_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: Evans Creek Landslide

Enumerated_Domain_Value_Definition: landslide name
 Enumerated_Domain_Value_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Bear Trap Slide
 Enumerated_Domain_Value_Definition: landslide name
 Enumerated_Domain_Value_Definition_Source: U.S. Geological Survey
 Attribute:
 Attribute_Label: GEOL
 Attribute_Definition: Dominate geologic unit where landslide occurred.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Dike, Dike 1, QTg, QT_i, Qal, Qau, Qba, Qgf, Qls, Qt, Qyt, Tad, Tb, Tba, Tbp, Tc, To, Tdg, Tds, Tfc, Thg, Ti, Tib, Tib₁, Tiha, Tipa, Tis, Tlm, Tmd, Tmv, Tn, Tql, Tr, Trd, Tsa₁, Tsa₄, Tu, Tum, Tus
 Enumerated_Domain_Value_Definition: Lithologies
 Enumerated_Domain_Value_Definition_Source: DOGAMI GEO
 Attribute:
 Attribute_Label: SLOPE
 Attribute_Definition: Slope of hillside adjacent to landslide.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 3
 Range_Domain_Maximum: 50
 Attribute:
 Attribute_Label: AGE
 Attribute_Definition: Relative age of deposit.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Historic
 Enumerated_Domain_Value_Definition: Active movement <150 years: "The landslide appears to be currently moving or to have moved within historic time or historic data has identified the landslide as having moved in the last 150 years. Landslide features generally sharp and clear."
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Prehistoric
 Enumerated_Domain_Value_Definition: Ancient movement >150 years: "Landslide features are slightly to strongly eroded or covered with younger deposits. Features may be subdued and indistinct."
 Enumerated_Domain_Value_Definition_Source: SP42
 Attribute:
 Attribute_Label: FAN_HEIGHT

Attribute_Definition: Thickness of debris flow fan.
Attribute_Definition_Source: U.S. Geological Survey
Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 8
 Range_Domain_Maximum: 150
Attribute:
 Attribute_Label: HS_HEIGHT
 Attribute_Definition: Measured head scarp height, in feet.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 8
 Range_Domain_Maximum: 800
Attribute:
 Attribute_Label: FAIL_DEPTH
 Attribute_Definition: Measured depth of landslide, in feet.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 7
 Range_Domain_Maximum: 772
Attribute:
 Attribute_Label: HS_IS1
 Attribute_Definition: Horizontal distance from head scarp to internal scarp 1.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 60
 Range_Domain_Maximum: 800
Attribute:
 Attribute_Label: IS1_IS2
 Attribute_Definition: Horizontal distance from internal scarp 1 to internal scarp 2.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 50
 Range_Domain_Maximum: 800
Attribute:
 Attribute_Label: IS2_IS3
 Attribute_Definition: Horizontal distance from internal scarp 2 to internal scarp 3.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 70
 Range_Domain_Maximum: 2000
Attribute:

Attribute_Label: IS3_IS4
 Attribute_Definition: Horizontal distance from internal scarp 3 to internal scarp 4.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 130
 Range_Domain_Maximum: 360
 Attribute:
 Attribute_Label: HD_AVE
 Attribute_Definition: Average horizontal distance between internal scarps: calculated average horizontal distance between scarps.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 115
 Range_Domain_Maximum: 3000
 Attribute:
 Attribute_Label: DIRECT
 Attribute_Definition: Direction of movement.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 0
 Range_Domain_Maximum: 337.5
 Attribute:
 Attribute_Label: AREA
 Attribute_Definition: Area of landslide deposit (square feet).
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 22349
 Range_Domain_Maximum: 168740368
 Attribute:
 Attribute_Label: VOL
 Attribute_Definition: Volume of landslide deposit (cubic feet).
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Range_Domain:
 Range_Domain_Minimum: 64073
 Range_Domain_Maximum: 59767189504
 Attribute:
 Attribute_Label: DEEP_SHAL
 Attribute_Definition: Relative depth of landslide.
 Attribute_Definition_Source: U.S. Geological Survey
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Shallow

Enumerated_Domain_Value_Definition: Landslide thickness <= 15 feet

Enumerated_Domain_Value_Definition_Source: SP42

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: Deep

Enumerated_Domain_Value_Definition: Landslide thickness > 15 feet

Enumerated_Domain_Value_Definition_Source: SP42

Attribute:

Attribute_Label: QUADNAME

Attribute_Definition: USGS Quadrangle Name.

Attribute_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: Bagby Hot Springs

Enumerated_Domain_Value_Definition: Quad Index

Enumerated_Domain_Value_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: Battle Ax

Enumerated_Domain_Value_Definition: Quad Index

Enumerated_Domain_Value_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: Elkhorn

Enumerated_Domain_Value_Definition: Quad Index

Enumerated_Domain_Value_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: Lyons

Enumerated_Domain_Value_Definition: Quad Index

Enumerated_Domain_Value_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: Mill City North

Enumerated_Domain_Value_Definition: Quad Index

Enumerated_Domain_Value_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: Rooster Rock

Enumerated_Domain_Value_Definition: Quad Index

Enumerated_Domain_Value_Definition_Source: U.S. Geological Survey

Attribute:

Attribute_Label: sqmi

Attribute_Definition: Area of landslide deposit (square miles).

Attribute_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Range_Domain:

Range_Domain_Minimum: 0

Range_Domain_Maximum: 6

Attribute:

Attribute_Label: Acres

Attribute_Definition: Area of landslide deposit (acres).

Attribute_Definition_Source: U.S. Geological Survey

Attribute_Domain_Values:

Range_Domain:

Range_Domain_Minimum: 0.5

Range_Domain_Maximum: 3873.7

Attribute:

Attribute_Label: Shape_Length

Attribute_Definition: Length of feature in internal units (feet).

Attribute_Definition_Source: ESRI

Attribute_Domain_Values:

Unrepresentable_Domain: Positive real numbers that are automatically generated.

Attribute:

Attribute_Label: Shape_Area

Attribute_Definition: Area of feature in internal units squared (square feet).

Attribute_Definition_Source: ESRI

Attribute_Domain_Values:

Unrepresentable_Domain: Positive real numbers that are automatically generated.

Overview_Description:

Entity_and_Attribute_Overview: Lists each UNIQUE_ID and its corresponding landslide.

Entity_and_Attribute_Detail_Citation:

Burns, W.J., and Madin, I.P., 2009, Protocol for inventory mapping of landslide deposits from light detection and ranging (LIDAR) imagery: Oregon Department of Geology and Mineral Industries Special Paper 42, 30 p.

Oregon Department of Geology and Mineral Industries, 2009, Oregon geologic data compilation: digital data set courtesy of Bill Burns, will be available online at <http://ogdc.geos.pdx.edu/> [digital data set]

Distribution_Information:

Distributor:

Contact_Information:

Contact_Organization_Primary:

Contact_Organization: U.S. Geological Survey

Contact_Position: Ask USGS -- Water Webserver Team

Contact_Address:

Address_Type: mailing address

Address: 445 National Center

City: Reston

State_or_Province: VA

Postal_Code: 20192

Country: USA

Contact_Voice_Telephone: 1-888-275-8747 (1-888-ASK-USGS)

Contact_Electronic_Mail_Address: http://water.usgs.gov/user_feedback_form.html

Resource_Description: Downloadable Data

Distribution_Liability: Although these data have been used by the U.S. Geological Survey, U.S. Department of the Interior, no warranty expressed or implied is made by the U.S. Geological Survey as to the accuracy of the data. The act of distribution shall not constitute any such warranty, and no responsibility is assumed by the U.S. Geological Survey in the use of these data, software, or related materials. The use of firm, trade, or brand names in this report is for identification purposes only and does not constitute endorsement by the U.S. Geological Survey. The names mentioned in this document may be trademarks or registered trademarks of their respective trademark owners.

Standard_Order_Process:

Digital_Form:

Digital_Transfer_Information:

Format_Name: ESRI Geodatabase Feature Class

Format_Information_Content: PKZIP compression

File-Decompression_Technique: Winzip

Transfer_Size: 1000

Digital_Transfer_Option:

Online_Option:

Computer_Contact_Information:

Network_Address:

Network_Resource_Name:

http://water.usgs.gov/GIS/dsdl/LNsantiam_LandslideInventory.zip

Fees: None. This dataset is provided by USGS as a public service.

Metadata_Reference_Information:

Metadata_Date: 20100927

Metadata_Contact:

Contact_Information:

Contact_Organization_Primary:

Contact_Organization: U.S. Geological Survey

Contact_Person: REQUIRED: The person responsible for the metadata information.

Contact_Position: Ask USGS -- Water Webserver Team

Contact_Address:

Address_Type: mailing address

Address: 445 National Center

City: Reston

State_or_Province: VA

Postal_Code: 20192

Country: USA

Contact_Voice_Telephone: 1-888-275-8747 (1-888-ASK-USGS)

Contact_Electronic_Mail_Address: http://water.usgs.gov/user_feedback_form.html

Metadata_Standard_Name: FGDC Content Standards for Digital Geospatial Metadata

Metadata_Standard_Version: FGDC-STD-001-1998

Metadata_Time_Convention: local time

Metadata_Extensions:

Online_Linkage: <http://www.esri.com/metadata/esriprof80.html>

Profile_Name: ESRI Metadata Profile

Metadata_Extensions:

Online_Linkage: <http://www.esri.com/metadata/esriprof80.html>

Profile_Name: ESRI Metadata Profile

B.2: Timber Harvest Change (1995-2009)

GIS data set available online:

http://water.usgs.gov/GIS/dsdl/LNsantiam_TimberChange2009.zip

Identification_Information:

Citation:

Citation_Information:

Originator: Steven Sobieszczyk

Publication_Date: 2009

Title: Timber Harvest Change in the Little North Santiam River Basin, Oregon, 1995 to 2009

Geospatial_Data_Presentation_Form: vector digital data

Online_Linkage:

http://water.usgs.gov/lookup/getspatial?lnsantiam_TimberChange2009

Description:

Abstract: Using available aerial photos from approximately a 15-year period, changes in timber harvest were mapped in the Little North Santiam River Basin, Oregon. Timber harvest plots as seen on digital orthophotos from 1995, 2000, 2005, and 2009 were digitized and attributed based on harvest type or purpose: clearcut, thinning, or development.

Purpose: This data set represents four separate periods (1995; 2000; 2005; and 2009) of timber harvest change in the Little North Santiam River Basin, Oregon. Using digital orthophotos from the 4 time periods, each imagery set had observed timber harvest plots digitized and attributed. Classifications were limited to whether the timber harvest area had been clearcut (majority of trees removed), thinned (majority of trees remained), or developed (trees removed and replaced with man-made infrastructure). Land cover change and timber harvest inventory will be used for future watershed analysis in the Little North Santiam Basin.

Supplemental_Information:

This work was completed as part of the Master's thesis "Using Turbidity Monitoring and LiDAR-Derived Imagery to Investigate Sources of Suspended Sediment in the Little North Santiam River Basin, Oregon, Winter 2009–2010" by Steven Sobieszczyk, Portland State University and U.S. Geological Survey.

Image evaluation and feature interpretation occurred at a scale of 1:10,000. Digitization of features occurred at a scale of 1:4,000. Timber loss due to natural features, such as landslide and rock outcrop, were not included in inventory.

Time_Period_of_Content:

Time_Period_Information:

Range_of_Dates/Times:

Beginning_Date: 1995

Ending_Date: 2009

Currentness_Reference: ground condition

Status:

Progress: Complete

Maintenance_and_Update_Frequency: As needed

Spatial_Domain:**Bounding_Coordinates:**

West_Bounding_Coordinate: -122.582591

East_Bounding_Coordinate: -122.174616

North_Bounding_Coordinate: 44.880884

South_Bounding_Coordinate: 44.776300

Keywords:**Theme:**

Theme_Keyword_Thesaurus: None

Theme_Keyword: timber harvest

Theme_Keyword: clearcut

Theme_Keyword: thinning

Theme_Keyword: development

Theme_Keyword: inlandWaters

Place:

Place_Keyword_Thesaurus: None

Place_Keyword: Little North Santiam River

Place_Keyword: Elkhorn

Place_Keyword: Mehama

Place_Keyword: Lyons

Place_Keyword: Oregon

Place_Keyword: Marion County

Temporal:

Temporal_Keyword_Thesaurus: None

Temporal_Keyword: 1995

Temporal_Keyword: 2000

Temporal_Keyword: 2005

Temporal_Keyword: 2009

Access_Constraints: None.

Use_Constraints: The U.S. Geological Survey should be acknowledged as the data source in products derived from these data.

Point_of_Contact:**Contact_Information:****Contact_Organization_Primary:**

Contact_Organization: U.S. Geological Survey

Contact_Person: Steven Sobieszczyk

Contact_Position: Hydrologist

Contact_Address:

Address_Type: mailing and physical address

Address: 2130 SW 5th Ave.

City: Portland

State_or_Province: OR

Postal_Code: 97201

Country: USA

Contact_Voice_Telephone: 503-251-3208

Contact_Facsimile_Telephone: 503-251-3470

Contact_Electronic_Mail_Address: *ssobie@usgs.gov*

Contact_Instructions:

Warning: Although accurate at the time of production, this information may have become obsolete.

See the Metadata_Reference_Information section for a current contact.

Browse_Graphic:

Browse_Graphic_File_Name:

http://water.usgs.gov/GIS/browse/LNsantiam_TimberChange2009.jpeg

Browse_Graphic_File_Description: Illustration of data set

Browse_Graphic_File_Type: JPEG

Native_Data_Set_Environment: Microsoft Windows XP Version 5.1 (Build 2600)
Service Pack 3; ESRI ArcCatalog 9.3.1.3000

Data_Quality_Information:

Attribute_Accuracy:

Attribute_Accuracy_Report: Data mapped at 4:000 scale. Horizontal error was +/- 1 to 24 ft based on either LiDAR or georectified orthophoto accuracy estimates.

Logical_Consistency_Report: Data are topologically correct in ArcGIS.

Completeness_Report: Data are complete.

Lineage:

Source_Information:

Source_Citation:

Citation_Information:

Originator: U.S. Department of Agriculture and U.S. Geological Survey

Publication_Date: 1995

Title: Digital Orthophoto Quadrangles

Geospatial_Data_Presentation_Form: remote-sensing image

Online_Linkage: <http://gis.oregon.gov/DAS/EISPD/GEO/data/doq.shtml>

Type_of_Source_Media: online

Source_Time_Period_of_Content:

Time_Period_Information:

Single_Date/Time:

Calendar_Date: 1995

Source_Currentness_Reference: publication date

Source_Citation_Abbreviation: USGSDOQ1995

Source_Contribution: Used as digitizing basemap or source.

Source_Information:

Source_Citation:

Citation_Information:

Originator: U.S. Department of Agriculture and U.S. Geological Survey

Publication_Date: 2000

Title: Digital Orthophoto Quadrangles

Geospatial_Data_Presentation_Form: remote-sensing image

Online_Linkage: <http://gis.oregon.gov/DAS/EISPD/GEO/data/doq.shtml>

Type_of_Source_Media: online

Source_Time_Period_of_Content:

Time_Period_Information:

Calendar_Date: 2000

Source_Currentness_Reference: publication date
 Source_Citation_Abbreviation: USGSDOQ2000
 Source_Contribution: Used as digitizing basemap or source.
 Source_Information:
 Source_Citation:
 Citation_Information:
 Originator: U.S. Department of Agriculture and U.S. Geological Survey
 Publication_Date: 2005
 Title: Digital Orthophoto Quadrangles
 Geospatial_Data_Presentation_Form: remote-sensing image
 Other_Citation_Details: National Agriculture Imagery Program (NAIP). 2005.
 Oregon colored half-meter Digital Orthophoto Quadrangle. U.S. Department of
 Agriculture and the U.S. Geological Survey.
 Online_Linkage: <http://oregonexplorer.info/imagery/>
 Type_of_Source_Media: online
 Source_Time_Period_of_Content:
 Time_Period_Information:
 Single_Date/Time:
 Calendar_Date: 2005
 Source_Currentness_Reference: publication date
 Source_Citation_Abbreviation: USGSDOQ2005
 Source_Contribution: Used as digitizing basemap or source.
 Source_Information:
 Source_Citation:
 Citation_Information:
 Originator: U.S. Department of Agriculture and U.S. Geological Survey
 Publication_Date: 2009
 Title: Digital Orthophoto Quadrangles
 Geospatial_Data_Presentation_Form: remote-sensing image
 Other_Citation_Details: National Agriculture Imagery Program (NAIP). 2009.
 Oregon colored half-meter Digital Orthophoto Quadrangle. U.S. Department of
 Agriculture and the U.S. Geological Survey.
 Online_Linkage: <http://oregonexplorer.info/imagery/>
 Type_of_Source_Media: online
 Source_Time_Period_of_Content:
 Time_Period_Information:
 Single_Date/Time:
 Calendar_Date: 2009
 Source_Currentness_Reference: publication date
 Source_Citation_Abbreviation: USGSDOQ2009
 Source_Contribution: Used as digitizing basemap or source.
 Source_Information:
 Source_Citation:
 Citation_Information:
 Originator: Oregon LiDAR Consortium
 Publication_Date: 2009
 Title: Willamette Valley LiDAR

Geospatial_Data_Presentation_Form: raster digital data
 Type_of_Source_Media: online
 Source_Time_Period_of_Content:
 Time_Period_Information:
 Single_Date/Time:
 Calendar_Date: 2009
 Source_Currentness_Reference: ground condition
 Source_Citation_Abbreviation: LiDAR
 Source_Contribution: Used as digitizing basemap or source.
 Process_Step:
 Process_Description: Digital Orthophoto Quadrangles (DOQ) for 1995 and 2000 downloaded from Oregon Geospatial Enterprise Office (GEO) at <http://gis.oregon.gov/DAS/EISPD/GEO/data/doq.shtml>. DOQs for 2005 and 2009 downloaded from Oregon Imagery Explorer at <http://oregonexplorer.info/imagery/>.
 Source_Used_Citation_Abbreviation: USGSDOQ2009
 Source_Used_Citation_Abbreviation: USGSDOQ2005
 Source_Used_Citation_Abbreviation: USGSDOQ2000
 Source_Used_Citation_Abbreviation: USGSDOQ1995
 Process_Date: 2009
 Process_Step:
 Process_Description: GIS polygon shapefile created based on DOQ projection (Oregon Lambert Conformal Conic)
 Process_Date: 2009
 Process_Step:
 Process_Description: Using the 1995 DOQs for the Little North Santiam River Basin as a basemap, all recent timber harvest areas were digitized. Polygons were attributed based on harvest type (clearcut or thinning), primary quadrangle location, secondary quadrangle location (if applicable), date of DOQ, and polygon characteristics (perimeter, area, acres, etc.).
 Source_Used_Citation_Abbreviation: USGSDOQ1995
 Process_Date: 2009
 Process_Step:
 Process_Description: Digitizing was repeated for 2000, 2005, 2009 DOQs. One more classification was added for timber harvest type – development – area that was harvested and built upon.
 Source_Used_Citation_Abbreviation: USGSDOQ2009
 Source_Used_Citation_Abbreviation: USGSDOQ2005
 Source_Used_Citation_Abbreviation: USGSDOQ2000
 Process_Date: 2009
 Process_Step:
 Process_Description: 2009 timber harvests were mapped using differential lidar grids (highest hit – bare earth: patches of land where difference was less than 5 feet tall where considered clearcut) and 2009 NAIP aerial photographs.
 Source_Used_Citation_Abbreviation: LiDAR
 Process_Date: 2009
 Spatial_Data_Organization_Information:
 Direct_Spatial_Reference_Method: Vector

Point_and_Vector_Object_Information:
 SDTS_Terms_Description:
 SDTS_Point_and_Vector_Object_Type: G-polygon
 Point_and_Vector_Object_Count: 311
 Spatial_Reference_Information:
 Horizontal_Coordinate_System_Definition:
 Planar:
 Map_Projection:
 Map_Projection_Name: Lambert Conformal Conic
 Lambert_Conformal_Conic:
 Standard_Parallel: 43.000000
 Standard_Parallel: 45.500000
 Longitude_of_Central_Meridian: -120.500000
 Latitude_of_Projection_Origin: 41.750000
 False_Easting: 1312335.958005
 False_Northing: 0.000000
 Planar_Coordinate_Information:
 Planar_Coordinate_Encoding_Method: coordinate pair
 Coordinate_Representation:
 Abscissa_Resolution: 0.000001
 Ordinate_Resolution: 0.000001
 Planar_Distance_Units: international feet
 Geodetic_Model:
 Horizontal_Datum_Name: D_North_American_1983_HARN
 Ellipsoid_Name: Geodetic Reference System 80
 Semi-major_Axis: 6378137.000000
 Denominator_of_Flattening_Ratio: 298.257222
 Vertical_Coordinate_System_Definition:
 Altitude_System_Definition:
 Entity_and_Attribute_Information:
 Detailed_Description:
 Entity_Type:
 Entity_Type_Label: Insantiam_timberchange
 Entity_Type_Definition: timber harvest plots
 Entity_Type_Definition_Source: U.S. Geological Survey
 Attribute:
 Attribute_Label: FID
 Attribute_Definition: Internal feature number.
 Attribute_Definition_Source: ESRI
 Attribute_Domain_Values:
 Unrepresentable_Domain: Sequential unique whole numbers that are automatically generated.
 Attribute:
 Attribute_Definition: Internal feature number.
 Attribute_Definition_Source: ESRI
 Attribute_Domain_Values:

Unrepresentable_Domain: Sequential unique whole numbers that are automatically generated.

Attribute:

Attribute_Label: Shape

Attribute_Definition: Feature geometry.

Attribute_Definition_Source: ESRI

Attribute_Domain_Values:

Unrepresentable_Domain: Coordinates defining the features.

Attribute:

Attribute_Label: dy

Attribute_Definition: Digital Orthophoto Quadrangle (DOQ) year

Attribute_Definition_Source: USDA/USGS DOQ

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: 1995

Enumerated_Domain_Value_Definition: Timber harvest plots shown in 1995

photos

Enumerated_Domain_Value_Definition_Source: USGS

Enumerated_Domain:

Enumerated_Domain_Value: 2000

Enumerated_Domain_Value_Definition: Timber harvests shown in 2000 photos

not seen in 1995 photos

Enumerated_Domain_Value_Definition_Source: USGS

Enumerated_Domain:

Enumerated_Domain_Value: 2005

Enumerated_Domain_Value_Definition: Timber harvests shown in 2005 photos

not seen in 2000 photos

Enumerated_Domain_Value_Definition_Source: USGS

Enumerated_Domain:

Enumerated_Domain_Value: 2009

Enumerated_Domain_Value_Definition: Timber harvests shown in 2009 photos

not seen in 2005 photos

Enumerated_Domain_Value_Definition_Source: USGS

Attribute:

Attribute_Label: FEATURE

Attribute_Definition: Timber removal type

Attribute_Definition_Source: USDA/USGS DOQ

Attribute_Domain_Values:

Enumerated_Domain:

Enumerated_Domain_Value: clearing, timber harvest

Enumerated_Domain_Value_Definition: clearcut stand

Enumerated_Domain_Value_Definition_Source: USGS

Enumerated_Domain:

Enumerated_Domain_Value: thinning, timber harvest

Enumerated_Domain_Value_Definition: 25% or greater trees remain after harvest

Enumerated_Domain_Value_Definition_Source: USGS

Enumerated_Domain:

Enumerated_Domain_Value: clearing, development
 Enumerated_Domain_Value_Definition: clearcut stand replaced with urban development or infrastructure
 Enumerated_Domain_Value_Definition_Source: USGS
 Beginning_Date_of_Attribute_Values: 1992
 Ending_Date_of_Attribute_Values: 2005
 Attribute:
 Attribute_Label: PRIM_QUAD
 Attribute_Definition: Primary quadrangle for timber harvest classification
 Attribute_Definition_Source: USDA/USGS DOQ
 Attribute_Domain_Values:
 Unrepresentable_Domain: 1:24,000 Quadrangle Name/Ohio Code
 Attribute:
 Attribute_Label: SEC_QUAD
 Attribute_Definition: Secondary quadrangle for timber harvest classification
 Attribute_Definition_Source: USDA/USGS DOQ
 Attribute_Domain_Values:
 Unrepresentable_Domain: 1:24,000 Quadrangle Name/Ohio Code
 Attribute:
 Attribute_Label: sqmi
 Attribute_Definition: Area measurement of polygon in square miles
 Attribute_Definition_Source: USGS
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: SQMI
 Enumerated_Domain_Value_Definition: Polygon area
 Enumerated_Domain_Value_Definition_Source: Determined by ESRI software
 (ArcMap calculations)
 Attribute:
 Attribute_Label: Acres
 Attribute_Definition: Area measurement of polygon in acres
 Attribute_Definition_Source: USGS
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: ACRES
 Enumerated_Domain_Value_Definition: Polygon area
 Enumerated_Domain_Value_Definition_Source: Determined by ESRI software
 (ArcMap calculations)
 Distribution_Information:
 Distributor:
 Contact_Information:
 Contact_Organization_Primary:
 Contact_Organization: U.S. Geological Survey
 Contact_Position: Ask USGS – Water Webserver Team
 Contact_Address:
 Address_Type: mailing address
 Address: 445 National Center

City: Reston

State_or_Province: VA

Postal_Code: 20192

Country: USA

Contact_Voice_Telephone: 1-888-275-8747 (1-888-ASK-USGS)

Contact_Electronic_Mail_Address: http://water.usgs.gov/user_feedback_form.html

Resource_Description: Downloadable Data

Distribution_Liability: Although these data have been used by the U.S. Geological Survey, U.S. Department of the Interior, no warranty expressed or implied is made by the U.S. Geological Survey as to the accuracy of the data. The act of distribution shall not constitute any such warranty, and no responsibility is assumed by the U.S. Geological Survey in the use of these data, software, or related materials. The use of firm, trade, or brand names in this report is for identification purposes only and does not constitute endorsement by the U.S. Geological Survey. The names mentioned in this document may be trademarks or registered trademarks of their respective trademark owners.

Standard_Order_Process:

Digital_Form:

Digital_Transfer_Information:

Format_Name: ESRI Geodatabase Feature Class

Format_Information_Content: PKZIP compression

File-Decompression_Technique: Winzip

Transfer_Size: 1000

Digital_Transfer_Option:

Online_Option:

Computer_Contact_Information:

Network_Address:

Network_Resource_Name:

http://water.usgs.gov/GIS/dsdl/LNsantiam_TimberChange2009.zip

Fees: None. This dataset is provided by USGS as a public service.

Metadata_Reference_Information:

Metadata_Date: 20100830

Metadata_Contact:

Contact_Information:

Contact_Organization_Primary:

Contact_Organization: U.S. Geological Survey

Contact_Position: Ask USGS – Water Webserver Team

Contact_Address:

Address_Type: mailing address

Address: 445 National Center

City: Reston

State_or_Province: VA

Postal_Code: 20192

Country: USA

Contact_Voice_Telephone: 1-888-275-8747 (1-888-ASK-USGS)

Contact_Electronic_Mail_Address: http://water.usgs.gov/user_feedback_form.html

Metadata_Standard_Name: FGDC Content Standards for Digital Geospatial Metadata

Metadata_Standard_Version: FGDC-STD-001-1998

Metadata_Time_Convention: local time

Metadata_Extensions:

Online_Linkage: *<http://www.esri.com/metadata/esriprof80.html>*

Profile_Name: ESRI Metadata Profile

B.3: Hydrography

GIS data set available online:

http://water.usgs.gov/GIS/dsdl/LNsantiam_Hydrography.zip

Identification_Information:

Citation:

Citation_Information:

Originator: Steven Sobieszczyk

Publication_Date: 2010

Title: Hydrography for the Little North Santiam River Basin, Oregon

Geospatial_Data_Presentation_Form: vector digital data

Online_Linkage:

http://water.usgs.gov/lookup/getspatial?lnsantiam_Hydrography

Description:

Abstract: LiDAR-derived (hydrography) stream network.

Purpose: This data set represents the river network for the Little North Santiam River Basin, Oregon. Using light detection and ranging (LiDAR) high-resolution imagery, stream centerlines for rivers, streams, and gullies were digitized.

Supplemental_Information:

This work was completed as part of the Master's thesis "Using Turbidity Monitoring and LiDAR-Derived Imagery to Investigate Sources of Suspended Sediment in the Little North Santiam River Basin, Oregon, Winter 2009–2010" by Steven Sobieszczyk, Portland State University and U.S. Geological Survey.

Mapping completed at 1:4,000 scale. Names of rivers and streams based on those from Oregon Atlas and USGS topographic maps. Data set has 3D component based on elevations queried from LiDAR imagery.

Time_Period_of_Content:

Time_Period_Information:

Single_Date/Time:

Calendar_Date: 2009

Currentness_Reference: ground condition

Status:

Progress: Complete

Maintenance_and_Update_Frequency: None planned

Spatial_Domain:

Bounding_Coordinates:

West_Bounding_Coordinate: -122.583134

East_Bounding_Coordinate: -122.133505

North_Bounding_Coordinate: 44.900483

South_Bounding_Coordinate: 44.778859

Keywords:

Theme:

Theme_Keyword_Thesaurus: None

Theme_Keyword: streams

Theme_Keyword: rivers

Theme_Keyword: gullies
 Theme_Keyword: inlandWaters
 Theme_Keyword: hydrography
 Theme_Keyword: LiDAR
 Place:
 Place_Keyword_Thesaurus: None
 Place_Keyword: Little North Santiam River
 Place_Keyword: Elkhorn
 Place_Keyword: Mehama
 Place_Keyword: Lyons
 Place_Keyword: Oregon
 Place_Keyword: Marion County
 Temporal:
 Temporal_Keyword_Thesaurus: None
 Temporal_Keyword: 2009
 Access_Constraints: None.
 Use_Constraints: The U.S. Geological Survey should be acknowledged as the data source in products derived from these data.
 Point_of_Contact:
 Contact_Information:
 Contact_Organization_Primary:
 Contact_Organization: U.S. Geological Survey
 Contact_Person: Steven Sobieszczyk
 Contact_Position: Hydrologist
 Contact_Address:
 Address_Type: mailing and physical address
 Address: 2130 SW 5th Ave.
 City: Portland
 State_or_Province: OR
 Postal_Code: 97201
 Country: USA
 Contact_Voice_Telephone: 503-251-3208
 Contact_Facsimile_Telephone: 503-251-3470
 Contact_Electronic_Mail_Address: ssobie@usgs.gov
 Contact_Instructions:
 Warning: Although accurate at the time of production, this information may have become obsolete.
 See the Metadata_Reference_Information section for a current contact.
 Browse_Graphic:
 Browse_Graphic_File_Name:
http://water.usgs.gov/GIS/browse/LNsantiam_Hydrography.jpeg
 Browse_Graphic_File_Description: Illustration of data set
 Browse_Graphic_File_Type: JPEG

 Data_Quality_Information:
 Attribute_Accuracy:

Attribute_Accuracy_Report: Data mapped at 4:000 scale. Horizontal error was +/- 1 ft based on LiDAR accuracy estimates.

Logical_Consistency_Report:

Snapping tolerance set to nodes and vertices during digitizing to avoid dangling nodes and isolated networks.

Data are topologically correct in ArcGIS.

Completeness_Report: Data are complete.

Lineage:

Source_Information:

Source_Citation:

Citation_Information:

Originator: Oregon LiDAR Consortium

Publication_Date: 2009

Title: Willamette Valley LiDAR

Geospatial_Data_Presentation_Form: remote-sensing image

Type_of_Source_Media: online

Source_Time_Period_of_Content:

Time_Period_Information:

Single_Date/Time:

Calendar_Date: 2009

Source_Currentness_Reference: publication date

Source_Citation_Abbreviation: LIDAR2009

Source_Contribution: Used as digitizing basemap or source.

Process_Step:

Process_Description: LiDAR digital elevation model was converted to a slopeshade model. Linework was manually digitized along river, stream, and gully centerline.

Linework mapped at 1:4000 scale and extended as far as what was visually discernable.

Process_Date: 20100610

Process_Time: 17570200

Process_Step:

Process_Description: Streams were annotated based on referenced stream names from Oregon Atlas, USGS topographic maps, and other digital USGS hydrography networks.

No naming conflicts existed from streams.

Process_Date: 20100615

Process_Time: 17271300

Process_Step:

Process_Description: Elevations applied to linework using 3D Analyst, Convert features to 3D tool. Values embedded into data set.

Source_Used_Citation_Abbreviation: LIDAR2009

Process_Date: 20100615

Process_Time: 17271300

Spatial_Data_Organization_Information:

Direct_Spatial_Reference_Method: Vector

Point_and_Vector_Object_Information:

SDTS_Terms_Description:

SDTS_Point_and_Vector_Object_Type: String

Point_and_Vector_Object_Count: 973

Spatial_Reference_Information:

Horizontal_Coordinate_System_Definition:

Planar:

Map_Projection:

Map_Projection_Name: Lambert Conformal Conic

Lambert_Conformal_Conic:

Standard_Parallel: 43.000000

Standard_Parallel: 45.500000

Longitude_of_Central_Meridian: -120.500000

Latitude_of_Projection_Origin: 41.750000

False_Easting: 1312335.958005

False_Northing: 0.000000

Planar_Coordinate_Information:

Planar_Coordinate_Encoding_Method: coordinate pair

Coordinate_Representation:

Abscissa_Resolution: 0.000001

Ordinate_Resolution: 0.000001

Planar_Distance_Units: international feet

Geodetic_Model:

Horizontal_Datum_Name: D_North_American_1983_HARN

Ellipsoid_Name: Geodetic Reference System 80

Semi-major_Axis: 6378137.000000

Denominator_of_Flattening_Ratio: 298.257222

Vertical_Coordinate_System_Definition:

Altitude_System_Definition:

Altitude_Datum_Name: North American Vertical Datum of 1988

Altitude_Resolution: 0.5

Altitude_Distance_Units: feet

Altitude_Encoding_Method: Explicit elevation coordinate included with horizontal

coordinates

Entity_and_Attribute_Information:

Detailed_Description:

Entity_Type:

Entity_Type_Label: LNsantiam_Hydrography

Entity_Type_Definition: Hydrography

Entity_Type_Definition_Source: U.S. Geological Survey

Attribute:

Attribute_Label: FID

Attribute_Definition: Internal feature number.

Attribute_Domain_Values:

Unrepresentable_Domain: Sequential unique whole numbers that are automatically generated.

Attribute:

Attribute_Label: Shape

Attribute_Definition: Feature geometry.

Attribute_Definition_Source: ESRI

Attribute_Domain_Values:
 Unrepresentable_Domain: Coordinates defining the features.

Attribute:
 Attribute_Label: Name
 Attribute_Definition: Stream name
 Attribute_Definition_Source: USGS
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Name
 Enumerated_Domain_Value_Definition: Stream name
 Enumerated_Domain_Value_Definition_Source: USGS topographic maps, Oregon
 Atlas, USGS hydrography data sets (RF1, NHDplus)

Attribute:
 Attribute_Label: Descript
 Attribute_Definition: Stream type
 Attribute_Definition_Source: USGS
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: River
 Enumerated_Domain_Value_Definition: Defined river segment - only defined
 river was the Little North Santiam River
 Enumerated_Domain_Value_Definition_Source: USGS topographic maps, Oregon
 Atlas, USGS hydrography data sets (RF1, NHDplus)

Enumerated_Domain:
 Enumerated_Domain_Value: Stream
 Enumerated_Domain_Value_Definition: Defined stream segment - included any
 other named stream feature, including creek, brook, stream, etc. as well as unnamed
 perennial streams.
 Enumerated_Domain_Value_Definition_Source: USGS topographic maps, Oregon
 Atlas, USGS hydrography data sets (RF1, NHDplus)

Enumerated_Domain:
 Enumerated_Domain_Value: Gully
 Enumerated_Domain_Value_Definition: Undefined, ephemeral, or minor mapped
 tributaries or channels.
 Enumerated_Domain_Value_Definition_Source: USGS topographic maps, Oregon
 Atlas, USGS hydrography data sets (RF1, NHDplus)

Attribute:
 Attribute_Label: Miles
 Attribute_Definition: Stream length
 Attribute_Definition_Source: USGS
 Attribute_Domain_Values:
 Enumerated_Domain:
 Enumerated_Domain_Value: Miles
 Enumerated_Domain_Value_Definition: Stream length in miles
 Enumerated_Domain_Value_Definition_Source: USGS

Overview_Description:

Entity_and_Attribute_Overview: Little North Santiam River, tributaries, and gullies (ephemeral streams) identified.

Entity_and_Attribute_Detail_Citation: LiDAR-derived hydrography

Distribution_Information:

Distributor:

Contact_Information:

Contact_Organization_Primary:

Contact_Organization: U.S. Geological Survey

Contact_Position: Ask USGS -- Water Webserver Team

Contact_Address:

Address_Type: mailing address

Address: 445 National Center

City: Reston

State_or_Province: VA

Postal_Code: 20192

Country: USA

Contact_Voice_Telephone: 1-888-275-8747 (1-888-ASK-USGS)

Resource_Description: Downloadable Data

Distribution_Liability: Although these data have been used by the U.S. Geological Survey, U.S. Department of the Interior, no warranty expressed or implied is made by the U.S. Geological Survey as to the accuracy of the data. The act of distribution shall not constitute any such warranty, and no responsibility is assumed by the U.S. Geological Survey in the use of these data, software, or related materials. The use of firm, trade, or brand names in this report is for identification purposes only and does not constitute endorsement by the U.S. Geological Survey. The names mentioned in this document may be trademarks or registered trademarks of their respective trademark owners.

Standard_Order_Process:

Digital_Form:

Digital_Transfer_Information:

Format_Name: shapefile

Format_Information_Content: PKZIP compression

File-Decompression_Technique: Winzip

Transfer_Size: 1000

Digital_Transfer_Option:

Online_Option:

Computer_Contact_Information:

Network_Address:

Network_Resource_Name:

http://water.usgs.gov/GIS/dsdl/LNsantiam_Hydrography.zip

Fees: None. This dataset is provided by USGS as a public service.

Metadata_Reference_Information:

Metadata_Date: 20100830

Metadata_Contact:

Contact_Information:

Contact_Organization_Primary:

Contact_Organization: U.S. Geological Survey

Contact_Position: Ask USGS -- Water Webserver Team
Contact_Address:
 Address_Type: mailing address
 Address: 445 National Center
 City: Reston
 State_or_Province: VA
 Postal_Code: 20192
 Country: USA
Contact_Voice_Telephone: 1-888-275-8747 (1-888-ASK-USGS)
Contact_Electronic_Mail_Address: http://water.usgs.gov/user_feedback_form.html
Metadata_Standard_Name: FGDC Content Standards for Digital Geospatial Metadata
Metadata_Standard_Version: FGDC-STD-001-1998
Metadata_Time_Convention: local time
Metadata_Extensions:
 Online_Linkage: <http://www.esri.com/metadata/esriprof80.html>
 Profile_Name: ESRI Metadata Profile